

Report

**Technical Review of Electro Purification LLC Applications for:
1) Authorization to Drill, Operate, and Aggregate Ten New Wells
for Production of Groundwater within the Bluebonnet
Groundwater Conservation District, and
2) Out-of-District Transport of Groundwater for Beneficial Uses
in Fort Bend County**



Prepared for:

Zach Holland

General Manager

Bluebonnet Groundwater Conservation District

P.O. Box 269

Navasota, TX 77868-0269

Prepared by:

William R. Hutchison, Ph.D., P.E., P.G.

Independent Groundwater Consultant

9802 Murmuring Creek Drive

Austin, TX 78736

512-745-0599

billhutch@texasgw.com

January 12, 2014

Professional Engineer and Professional Geoscientist Seals

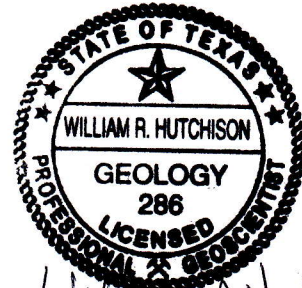
This report was prepared by William R. Hutchison, Ph.D., P.E., P.G., who is licensed in the State of Texas as follows:

- Professional Engineer (Geological and Civil) No. 96287
- Engineering Firm Registration No. 14526
- Professional Geoscientist (Geology) No. 286
- Geoscience Firm Registration No. 50445



William R. Hutchison

1/12/2014



William R. Hutchison

1/12/2014

Table of Contents

1.0	Executive Summary	4
1.1	Applicant’s Identified Project Needs	4
1.2	Groundwater Model Simulations	4
1.3	Potential Subsidence	6
2.0	Review of Proposed Project Needs in Context of Existing Plans	7
2.1	Regional Water Plan	7
2.2	Desired Future Condition and Modeled Available Groundwater Data	7
2.3	Groundwater Reduction Program	11
3.0	Groundwater Model Simulations	14
3.1	Base Scenario	16
3.2	Proposed Project Pumping in Addition to the Modeled Available Groundwater	16
3.3	Proposed Project Pumping with Reductions in Other Pumping	18
3.4	Simulation of Jasper Aquifer Pumping	19
3.5	Simulation of Conversion Schedule	19
3.6	Simulations with Simple Local-Scale MODFLOW Model	20
3.6.1	<i>Background</i>	20
3.6.2	<i>Simple MODFLOW Model Grid, Layering, and Boundary Conditions</i>	21
3.6.3	<i>Model Parameters for the Simple MODFLOW model</i>	22
3.6.4	<i>Simulations with the Simple MODFLOW model</i>	24
4.0	Simulated Effects of Proposed Pumping on Registered and Permitted Wells Using GAM and HAGM	26
4.1	Location of Registered and Permitted Wells	26
4.2	Simulations Results	29
4.2.1	<i>Drawdown Tables</i>	29
4.2.2	<i>Drawdown Maps</i>	30
4.3	Limitations of the Simulation Results	31
5.0	Simulated Effects of Proposed Pumping on Desired Future Conditions	33
5.1	Discussion of Results	34
6.0	Potential Effects of Proposed Pumping on Subsidence	37
6.1	Historic Subsidence in the Region	37
6.2	Clay Thickness	38

6.2	Historic Pumping in Areas with Historic Subsidence.....	39
6.3	Subsidence Results from GAM and HAGM Simulations	45
6.3.1	<i>Subsidence Estimates for Each Scenario</i>	46
6.3.2	<i>Subsidence Estimates for Individual Well Sites</i>	46
6.3.3	<i>Hydrographs of Estimated Subsidence</i>	48
6.3.4	<i>Maps of Subsidence at Individual Well Sites</i>	48
6.4	Discussion of Subsidence Results.....	48
7.0	Results of Simple Local-Scale MODFLOW Model Simulations	50
7.1	Variation of Aquifer Layer Clay Content.....	50
7.2	Variation in Postulated Confining Layer Clay Content.....	51
7.3	Discussion of Results	53
8.0	Discussion and Recommendations.....	54
8.1	Recommended Drilling and Testing Program.....	55
8.2	Recommended Monitoring Program	57
9.0	References.....	58

Appendix A – Review of the GAM and the HAGM in the Context of the Proposed Electro Purification Wells

Appendix B – GMA 14 Resolution Regarding Subsidence Districts

Appendix C – Tables and Maps of Simulated Well Drawdown Estimates

Appendix D – Tables and Hydrographs of County-Model Layer Drawdown Estimates

Appendix E – Tables, Hydrographs, and Maps of Subsidence Estimates

Appendix F – Salt Domes

List of Figures

Figure 1. Proposed Electro Purification Wells in Austin and Waller Counties	16
Figure 2. Applicant’s Postulated Conceptualization of an Upper Evangeline Aquifer and Lower Evangeline Aquifer	20
Figure 3. Model Grid and Boundary Conditions of Simple MODFLOW model.....	22
Figure 4. Registered and Permitted Wells, and Wells from TWDB database within Ten Miles of at least one EP Well - Chicot Aquifer	26
Figure 5. Registered and Permitted Wells, and Wells from the TWDB Database within Ten Miles of at least one EP Well - Evangeline Aquifer	27
Figure 6. Histogram of Distances to Wells - Chicot Aquifer	28
Figure 7. Histogram of Distances to Wells - Evangeline Aquifer	28
Figure 8. Map of Subsidence Measurement Locations	38
Figure 9. Average Clay Thickness in Areas with Historic Subsidence	39
Figure 10. Historic Pumping in Areas with Measured Subsidence Less than one foot	41
Figure 11. Historic Pumping in Areas with Measured Subsidence between one and three feet.....	41
Figure 12. Historic Pumping in Areas with Measured Subsidence between three and five feet	42
Figure 13. Historic Pumping in Areas with Measured Subsidence between five and seven feet	42
Figure 14. Historic Pumping in Areas with Measured Subsidence between seven and nine feet.....	43
Figure 15. Historic Pumping in Areas with Measured Subsidence greater than nine feet	43
Figure 16. Historic Pumping in the Electro Purification Project Area.....	44
Figure 17. Comparison of Actual Subsidence from 1906 to 2000 and Estimated Subsidence from 1891 to 2009 from the GAM and HAGM	45
Figure 18. Drawdown and Subsidence Estimates - Aquifer Unit Clay Content Variation	51
Figure 19. Drawdown and Subsidence Estimates - Confining Unit Clay Content Variation	52

List of Tables

Table 1. TWDB Decadal Population Projections Through 2070	8
Table 2. TWDB Decadal Municipal Water Demand Projections in Acre-Feet Per Year Through 2070	9
Table 3. Summary of Gulf Coast Aquifer Desired Future Condition and Modeled Available Groundwater for Austin, Fort Bend and Waller Counties (data from Oliver, 2010, and Hasan and Wade, 2011)	11
Table 4. Summary of Applicant’s Summary of Richmond and Rosenberg Demands and Required Conversions under the Groundwater Reduction Plan	12
Table 5. Summary of Simulations (EP Wells = Proposed Electro Purification Wells, MAG = Modeled Available Groundwater)	15
Table 6. Summary of Pumping Assignments in Model Grid for Scenarios 1 to 10	17
Table 7. Simulated Electro Purification (EP) Pumping, Other Pumping, and Total Pumping in Austin and Waller Counties for Scenarios 11 to 20	18
Table 8. Summary of Pumping Assignment for Scenarios 31 and 32	19
Table 9. Summary of Pumping in Waller County for Scenarios 31 and 32	20
Table 10. Initial Parameters for Simple MODFLOW Model	23
Table 11. Summary of Layer Clay Percentages Assumptions for Each Simulation with Simple MODFLOW Model	25
Table 12. Summary of Drawdown Estimates (2008 to 2060) for Wells Completed in the Chicot Aquifer – Estimates from Tables C-1 and C-2	30
Table 13. Summary of Drawdown Estimates (2008 to 2060) for Wells Completed in the Evangeline Aquifer - Estimates from Tables C-3 and C-4	30
Table 14. Summary of Baseline Scenario Drawdowns	34
Table 15. Summary of Subsidence Estimates (1891 to 2060) at Well Sites (Wells Completed in the Chicot Aquifer) – Estimates from Tables E-9 and E-10	47
Table 16. Summary of Subsidence Estimates (1891 to 2060) at Well Sites (Wells Completed in the Evangeline Aquifer) - Estimates from Tables E-11 and E-12	47

1.0 Executive Summary

This report summarizes the technical review of the Electro Purification LLC application for Authorization to Drill, Operate, and Aggregate Ten New Wells for Production of Groundwater within the Bluebonnet Groundwater Conservation District, and includes the application for Out-of-District Transport of Groundwater for Beneficial Uses in Fort Bend County.

The technical review covers four basic areas:

- Review the “needs” identified in the permit application in light of the Region H water plan, modeled available groundwater numbers that were developed by TWDB from the GMA 14 joint planning process, and the Fort Bend Subsidence District Groundwater Reduction Plan
- Review the impacts of proposed pumping on existing registered wells and permitted wells in the district
- Evaluate the impacts of the proposed pumping in the context of the adopted desired future conditions for Bluebonnet Groundwater Conservation District
- Evaluate the proposed pumping in the context of subsidence

In addition to these four basic areas of the technical review of the application, and in response to issues raised by several parties in the contested case hearing, Appendix F summarizes an analysis of the “salt-dome” issue.

1.1 Applicant’s Identified Project Needs

Electro Purification proposes ten wells in Austin and Waller counties, producing 20 million gallons per day (MGD), or 22,500 acre-feet per year (AF/yr) of groundwater from the Gulf Coast Aquifer. Water produced from these wells would be transported to Fort Bend County for sale, distribution and beneficial use. The current identified customers for the water identified by the applicant are the Cities of Richmond and Rosenberg. Electro Purification provided a summary of the Groundwater Reduction Plans (GRP) for Richmond and Rosenberg. The proposed new wells and pumping are intended to replace the reduced groundwater pumping in Richmond, Rosenberg and entities partnered with each. However, the number of wells and the requested pumping rate (20 MGD or 22,500 AF/yr) would supply more than twice the required amount to meet the GRP requirements for Richmond and Rosenberg. The application provides no specific customers for the additional proposed pumping.

1.2 Groundwater Model Simulations

Analyses of impacts of the proposed wells in terms of drawdown to existing registered and permitted wells in the Bluebonnet Groundwater Conservation District, the impact of the proposed pumping in the context of the adopted desired future conditions of the Bluebonnet Groundwater Conservation District, and in the context of subsidence were completed with the use of two groundwater models developed by the US Geological Survey that have been used for groundwater planning in the recent past.

One model used was the Northern Gulf Coast Groundwater Availability Model (GAM) that was developed by the US Geological Survey for the Texas Water Development Board (TWDB) in 2004 (Kasmarek and Robinson, 2004). This model is the groundwater model used by the TWDB for calculation of modeled available groundwater, and was used by consultants for Groundwater Management Area 14 during development of desired future conditions for the Gulf Coast Aquifer in 2010.

Simulations were also completed using the Houston Area Groundwater Model (HAGM) that was developed by the US Geological Survey in 2012 (Kasmarek, 2012). This model was an update to the GAM, and was developed in cooperation with the Harris-Galveston Subsidence District, the Fort Bend Subsidence District, and the Lone Star Groundwater Conservation District. The primary area of interest in the development of the model was Fort Bend, Galveston, Harris, and Montgomery Counties. The primary objective of the model was to develop an updated tool to support the subsidence district's efforts to update their regulatory plan.

A more detailed review of these models in the context of the proposed pumping is provided in Appendix A of this report. In summary, neither model is likely reliable with respect to estimates of future drawdown, especially in the case of a proposed substantial increase in pumping. Subsidence estimates may be considered more reliable than the drawdown estimates. Overall, the accuracy of long-term subsidence estimates are within a foot of actual long-term subsidence measurements as documented by the US Geological Survey in areas of the model where subsidence has been measured. However, there is still a considerable degree of uncertainty in predicted subsidence estimates in an area where a large and concentrated increase in pumping is proposed with either model.

Overall, confidence in the results of the GAM and HAGM simulations is relatively low. The GAM and HAGM are regional scale models, and many of the issues are local scale that cannot be adequately simulated by these regional models. In an attempt to highlight and address some of the limitations of the GAM and HAGM with respect to the proposed project, an alternative simple local-scale MODFLOW model was developed. As developed in this report, this local-scale model simulated a postulated condition that the Evangeline Aquifer can be subdivided into an upper and lower aquifer zones that are separated by a confining unit. This postulated subdivision of the Evangeline Aquifer is not simulated with either the GAM or HAGM since these are regional models. However, if this localized condition exists, the simple model can be a useful tool to understand the relationships between pumping in the deeper portions of the Evangeline Aquifer (as proposed by Electro Purification), and

- The drawdown in the overlying upper portions of the Evangeline Aquifer (when vertically separated from the pumping zone by a confining layer by varying degrees)
- The drawdown in the Chicot Aquifer, which overlies the Evangeline and in which several wells are completed in the proposed project area
- The subsidence in the area under varying degrees of confinement within the Evangeline Aquifer

The simulations with the simple local-scale MODFLOW model are not to be construed as accurate or quantitative. They are only instructive to understand the relationship between parameters and the

results (drawdown and subsidence in this case), and the importance of local subsurface data collection and analyses of tests in the project area to obtain accurate parameters from any future testing in the area, if a permit is issued.

1.3 Potential Subsidence

Based on an analysis of measured subsidence data and simulations over a wide range of alternative scenarios, the following findings were developed:

- Historic subsidence in the region has occurred in areas with high pumping and thick clay sequences. Subsidence has been measured in excess of nine feet in some areas of Harris County. Clay thickness in the proposed Electro Purification project area is less than the clay thickness in those portions of Harris County.
- Based on an analysis of mapped clay thickness at the proposed Electro Purification site and an evaluation of historic pumping in areas with measured subsidence in the region, subsidence impacts associated with the proposed project could be as high as three to seven foot range over several decades, depending on the amount of pumping.
- The proposed Electro Purification pumping at the full amount (20 million gallons per day for the project and as much as six million gallons per day in a one-square mile area) represents an intense amount of pumping over a fairly small area. Analysis of historic pumping estimates suggest that this amount of pumping in a small area, while not unprecedented for the area, is certainly not common. Thus, the use of historic analogs and models that are based on historic data cannot be considered highly accurate.
- The models that are available for use in this analysis (GAM and HAGM) were used to simulate a wide range of potential pumping scenarios to better understand the potential for subsidence in the area of the proposed pumping. Based on the calibration of the model, it appears that measureable subsidence will occur by 2060 if pumping exceeds about 6 million gallons per day. Based on the model simulations, this subsidence may not actually be measureable for 10 to 20 years.
- The models results suggest that spreading the pumping over a wide area will mitigate the subsidence impacts as compared to concentrating the pumping over a small area.

2.0 Review of Proposed Project Needs in Context of Existing Plans

Electro Purification proposes ten wells in Austin and Waller counties, producing 20 million gallons per day (MGD), or 22,500 acre-feet per year (AF/yr) of groundwater from the Evangeline Aquifer. Water produced from these wells would be transported to Fort Bend County for sale, distribution and beneficial use. The current identified customers for the water identified by the applicant are the Cities of Richmond and Rosenberg.

2.1 Regional Water Plan

Decadal estimates of future population and municipal water demand through 2070 were recently approved by the Texas Water Development Board. Data for Fort Bend County are presented in Tables 1 and 2 by Water User Group. For municipal use, this includes incorporated census places with a population greater than 500 and retail public utilities providing more than 280 acre-feet per year. Places that do not meet these criteria are grouped together in “County-Other”, which for Fort Bend County is substantial.

From these estimates, it can be seen that the total expected municipal demand for Richmond and Rosenberg is expected to increase to 6,869 acre-feet per year in 2030, and 8,336 acre-feet per year in 2070. However, as outlined in Electro Purification’s response of January 16, 2013, other entities in the area are partnered with Richmond and Rosenberg in the Groundwater Reduction Plan. Many of these entities listed in the January 16, 2013 letter do not appear as separate line items in Tables 1 and 2 due to their size and/or annual production, and are therefore lumped with others in the “County-Other” line. Further discussion of the partnering arrangements are discussed in Section 2.3.

2.2 Desired Future Condition and Modeled Available Groundwater Data

Desired future conditions are established by groundwater conservation districts in a groundwater management area, and are essentially quantified planning goals for a 50-year period. Modeled available groundwater is the amount of pumping, calculated by the Texas Water Development Board, which will achieve the desired future condition.

In 2010, the groundwater conservation districts in Groundwater Management Area 14 adopted desired future conditions for the Gulf Coast Aquifer. The desired future conditions for the Gulf Coast Aquifer were developed based on a simulation using the Northern Gulf Coast Groundwater Availability Model (GAM). Specifically, the desired future conditions were based on Scenario 3 of GAM Run 10-023 (Oliver, 2010). The results of the simulation provided estimates of drawdown for each of the subunits, or layers, of the Gulf Coast Aquifer (Chicot, Evangeline, Burkeville, and Jasper in increasing depth).

Table 1. TWDB Decadal Population Projections Through 2070

Water User Group	2020	2030	2040	2050	2060	2070
ARCOLA	1,874	2,848	3,748	4,605	5,302	5,999
BEASLEY	666	727	847	1,013	1,240	1,551
COUNTY-OTHER	184,306	235,839	269,995	340,568	440,233	568,474
FAIRCHILDS	783	915	1,026	1,186	1,422	1,778
FORT BEND COUNTY MUD #116	2,505	2,843	3,340	3,729	4,118	4,506
FORT BEND COUNTY MUD #121	3,188	3,461	4,094	4,741	5,389	6,037
FORT BEND COUNTY MUD #129	2,680	3,848	4,933	5,838	6,471	6,475
FORT BEND COUNTY MUD #23	11,693	12,464	12,884	13,305	13,725	14,145
FORT BEND COUNTY MUD #25	9,412	9,502	9,649	9,822	10,000	10,181
FULSHEAR	12,106	13,755	14,932	15,925	16,784	17,543
GREATWOOD	12,140	12,601	12,669	12,736	12,803	12,870
HOUSTON	41,589	44,084	46,095	47,876	49,329	50,432
KATY	6,908	16,048	16,136	16,205	16,259	16,302
MEADOWS PLACE	4,669	4,761	4,856	4,953	5,052	5,153
MISSOURI CITY	75,849	93,347	110,720	125,923	135,484	141,294
NEEDVILLE	2,836	2,874	2,922	2,995	3,104	3,267
NORTH FORT BEND WATER AUTHORITY	279,197	386,813	471,003	519,828	545,853	559,135
PEARLAND	3,495	3,766	4,691	5,615	6,543	7,621
PECAN GROVE MUD #1	11,510	11,535	11,581	11,620	11,653	11,683
PLANTATION MUD	3,948	3,948	3,948	3,948	3,948	3,948
PLEAK	1,350	1,580	1,691	1,797	1,907	2,034
RICHMOND	12,400	12,890	13,510	14,375	15,236	16,093
ROSENBERG	40,384	42,560	44,928	47,378	50,227	53,654
SIENNA PLANTATION	18,447	23,593	32,113	40,633	49,154	57,016
SIMONTON	884	1,047	1,369	1,623	1,826	1,992
STAFFORD	17,761	18,241	18,845	19,518	20,271	21,115
SUGAR LAND	105,510	114,908	122,172	129,275	135,224	139,312
WESTON LAKES	2,621	2,791	3,019	3,247	3,475	3,704
WHCRWA	11,255	11,534	11,591	11,656	11,750	11,850

Table 2. TWDB Decadal Municipal Water Demand Projections in Acre-Feet Per Year Through 2070

Water User Group	2020	2030	2040	2050	2060	2070
BEASLEY	78	82	93	109	133	166
COUNTY-OTHER	25,842	32,512	36,976	46,469	59,999	77,413
FAIRCHILDS	94	106	116	132	157	196
FORT BEND COUNTY MUD #116	580	654	767	854	942	1,031
FORT BEND COUNTY MUD #121	394	423	498	575	652	730
FORT BEND COUNTY MUD #129	664	947	1,211	1,432	1,586	1,587
FORT BEND COUNTY MUD #23	1,318	1,387	1,428	1,469	1,511	1,556
FORT BEND COUNTY MUD #25	1,212	1,199	1,200	1,210	1,228	1,250
FULSHEAR	1,378	1,549	1,679	1,788	1,884	1,967
GREATWOOD	1,469	1,491	1,477	1,471	1,475	1,482
HOUSTON	8,426	8,739	8,994	9,266	9,530	9,739
KATY	1,664	3,798	3,796	3,800	3,810	3,819
MEADOWS PLACE	773	765	761	767	780	796
MISSOURI CITY	11,858	14,199	16,577	18,715	20,104	20,959
NEEDVILLE	300	292	287	289	298	313
NORTH FORT BEND WATER AUTHORITY	62,302	85,549	103,873	114,477	120,129	123,021
PEARLAND	502	533	658	784	911	1,061
PECAN GROVE MUD #1	2,016	1,963	1,922	1,922	1,923	1,928
PLANTATION MUD	417	399	385	377	376	376
PLEAK	158	179	187	197	208	222
RICHMOND	2,023	2,046	2,098	2,207	2,333	2,463
ROSENBERG	4,707	4,823	4,989	5,205	5,503	5,873
SIENNA PLANTATION	4,395	5,584	7,581	9,578	11,576	13,423
SIMONTON	105	119	151	176	198	216
STAFFORD	4,238	4,290	4,383	4,512	4,678	4,872
SUGAR LAND	28,173	30,347	32,045	33,780	35,292	36,352
WESTON LAKES	1,657	1,758	1,899	2,039	2,181	2,325
WHCRWA	1,441	1,449	1,438	1,436	1,445	1,457

The desired future conditions adopted by the groundwater conservation districts of Groundwater Management Area 14 adopted the simulated drawdown in groundwater elevations averaged by county and model layer for all counties not included in a subsidence district (Fort Bend, Galveston, and Harris). As part of the adoption of the desired future conditions, Groundwater Management Area 14 adopted a resolution (included in this report as Appendix B) explaining the unique role that the subsidence districts played in the development of the desired future conditions, and the unique circumstances associated with the subsidence districts in this planning process.

In summary, the Fort Bend Subsidence District (FBSD) and the Harris-Galveston Subsidence District (HGSD), which operate in Fort Bend, Galveston, and Harris counties, do not specifically regulate on the basis of groundwater drawdowns, nor do they regulate on the basis of specific pumping limitations. Rather, as explained in the resolution, the regulations in these three counties are based on limitations of groundwater pumping as a percentage of total water demand, and the percentage of groundwater pumping to total water demand is decreased over time, as total water demand increases. The resolution acknowledges that there is no “easily defined relationship” between groundwater elevation drawdown and subsidence. However, the resolution notes that high pumping can result in groundwater elevation drawdown that, in turn, can cause clay layers within the aquifer to compact. This compaction of clay layers within the aquifer results in subsidence. The resolution clearly stated that the desired future condition for Fort Bend, Galveston, and Harris counties is that future land subsidence be avoided.

The resolution provided a qualitative expression of a desired future condition for Fort Bend, Galveston, and Harris counties. The adopted desired future condition includes quantitative estimates of drawdown from 2009 to 2060 (52 years) based on Scenario 3 of GAM Run 10-023 for all other counties in Groundwater Management Area 14. The desired future conditions were then used by the Texas Water Development Board to develop modeled available groundwater estimates (the amount of pumping to achieve the desired future condition) for each county-model layer unit. The results of this effort are documented in GAM Run 10-038MAG (Hasan and Wade, 2011). Table 3 summarizes the pertinent drawdown estimates for Austin and Waller counties, as well as the model results for Fort Bend County from Oliver (2010), and the modeled available groundwater estimates from Hasan and Wade for all three counties of interest.

Table 3. Summary of Gulf Coast Aquifer Desired Future Condition and Modeled Available Groundwater for Austin, Fort Bend and Waller Counties (data from Oliver, 2010, and Hasan and Wade, 2011)

County	Aquifer	Desired Future Condition (ft of drawdown from 2009 to 2060) ¹	Modeled Available Groundwater (AF/yr)					
			2010	2020	2030	2040	2050	2060
Austin	Chicot	17	1,300	1,300	1,300	1,300	1,300	1,300
Fort Bend	Chicot	19	83,006	75,916	61,657	61,004	60,061	60,177
Waller	Chicot	7	300	300	300	300	300	300
Austin	Evangeline	10	20,013	20,013	20,013	20,013	20,013	20,013
Fort Bend	Evangeline	24	30,923	32,789	30,420	31,166	32,251	32,313
Waller	Evangeline	8	41,027	41,027	41,027	41,027	41,027	41,027
Austin	Burkeville	11	0	0	0	0	0	0
Fort Bend	Burkeville	20	0	0	0	0	0	0
Waller	Burkeville	9	0	0	0	0	0	0
Austin	Jasper	20	1,001	1,001	1,001	1,001	1,001	1,001
Fort Bend	Jasper	40	0	0	0	0	0	0
Waller	Jasper	25	300	300	300	300	300	300

¹Note that the drawdowns presented for Fort Bend County are not the adopted desired future condition (see text and Appendix B for explanation), but are the estimated drawdowns from Scenario 3 of GAM Run 10-034 (Oliver, 2010) in Fort Bend County that are consistent with the adopted desired future conditions in Groundwater Management Area 14.

2.3 Groundwater Reduction Program

Electro Purification provided a summary of the Groundwater Reduction Programs (GRP) for Richmond and Rosenberg in their response letter of January 16, 2013. The proposed new wells and pumping are intended to replace the reduced groundwater pumping in Richmond, Rosenberg and other entities partnered with each.

According to the applicant, the following entities are currently served by the City of Richmond water system, and are partnered with the City of Richmond in the Groundwater Reduction Program:

- Fort Bend County MUD No. 19 – Riverwood
- Fort Bend County MUD No. 121 – RiverPark West
- Fort Bend County MUD No. 140 – River’s Edge
- Fort Bend County MUD No. 145 – Rio Vista
- Fort Bend County MUD No. 187 – Del Webb

According to the applicant, the following entities are partnered with the City of Richmond in the Groundwater Reduction Program, but are not currently served by the City of Richmond water system

- Fort Bend County MUD No. 116 – Canyon Gate
- Fort Bend County WCID No. 3 – Texana
- Fort Bend County WCID No. 8 – Westcreek
- Lamar Consolidated ISD
- RiverPark West HOA
- Texana HOA
- Fort Bend Country Club

According to the application, the following entities are partnered with the City of Rosenberg in the Groundwater Reduction Program:

- Quadvest, L.P. (Bridlewood Estates)
- Fort Bend County MUD No. 5
- Fort Bend County MUD No. 155 (amenity well)
- Fort Bend County MUD No. 162
- Fort Bend County Fresh Water Supply District No. 2

Based on the analysis presented by the applicant in their January 16, 2013 letter, the applicant provided the data presented in Table 4 for total demands for Richmond, Rosenberg and their GRP partners, and required reductions expressed in terms of a percentage of total demand, and in terms of pumping in million gallons per day and acre-feet per year. Based on the information submitted, there are only identified customers for the proposed project for up to about 11,097 acre-feet per year of groundwater.

Table 4. Summary of Applicant’s Summary of Richmond and Rosenberg Demands and Required Conversions under the Groundwater Reduction Plan

Year	Total Demand (mgd)	Total Demand (AF/yr)	Required Conversion (%)	Required Conversion (mgd)	Required Conversion (AF/yr)
2010	8.358	9,362	0	0	0
2015	11.294	12,651	30	3.388	3,795
2025	15.123	16,940	60	9.074	10,164
2030	16.511	18,494	60	9.907	11,097

Please recall from Table 2 that, based on Texas Water Development Board projections, the total demand in 2030 for Richmond and Rosenberg is 6,869 acre-feet per year (2,046 acre-feet per year for Richmond and 4,823 acre-feet per year for Rosenberg). A 60 percent reduction in this projected demand is 4,121 acre-feet per year, and would represent the conversion requirement of the cities of

Richmond and Rosenberg. These are the projected demand and conversion requirement for the cities themselves, and do not include their GRP partners. However, the applicant stated that 11,097 AF/yr is needed to meet reduction requirements of Richmond, Rosenberg, and their GRP partners in 2030.

Assuming that the TWDB water demand projections in Table 2 are consistent with those demand estimates that were basis for the Groundwater Reduction Program, the amount of water needed to meet the GRP partners in 2030 is 6,976 acre-feet per year (the difference between 11,097 acre-feet per year stated by the applicant and the 4,121 acre-feet per year conversion requirement for the cities of Richmond and Rosenberg calculated above).

In terms of million gallons per day, the total conversion requirement in 2030 stated by the applicant is 9.907 mgd, the conversion requirement for Richmond and Rosenberg in 2030 is 3.679 mgd, and the calculated conversion requirement of the GRP partners is 6.228 mgd.

Based on these calculations, the applicant appears to be stating that Richmond and Rosenberg account for 37 percent of the conversion requirement, and the GRP partners account for 63 percent of the conversion requirement in 2030. In addition, the remaining amount requested (11,403 acre-feet per year) has no identified customer.

In conclusion, the number of wells and the requested pumping rate (20 MGD or 22,500 AF/yr) would supply more than twice the required amount to meet the GRP requirements for Richmond and Rosenberg, and their reported GRP partners. The application provides no specific customers for the additional proposed pumping.

3.0 Groundwater Model Simulations

Analyses of impacts of the proposed wells in terms of drawdown to existing registered and permitted wells in the Bluebonnet Groundwater Conservation District, the impact of the proposed pumping in the context of the adopted desired future conditions of the Bluebonnet Groundwater Conservation District, and in the context of subsidence were completed with the use of two groundwater models developed by the US Geological Survey that have been used for groundwater planning in the recent past.

The first was the Northern Gulf Coast Groundwater Availability Model (GAM) that was developed by the US Geological Survey for the Texas Water Development Board (TWDB) in 2004 (Kasmarek and Robinson, 2004). This model is the currently approved groundwater model by the TWDB, and was used by consultants for Groundwater Management Area 14 during development of desired future conditions for the Gulf Coast Aquifer in 2010.

Simulations were also completed using the Houston Area Groundwater Model (HAGM) that was developed by the US Geological Survey in 2012 (Kasmarek, 2012). This model was an update to the GAM, and was developed in cooperation with the Harris-Galveston Subsidence District, the Fort Bend Subsidence District, and the Lone Star Groundwater Conservation District. The primary area of interest in the development of the model was Fort Bend, Galveston, Harris, and Montgomery Counties. The primary objective of the model was to develop an updated tool to support the subsidence district's efforts to update their regulatory plan.

A more detailed review of these models in the context of the proposed pumping is provided in Appendix A of this report. In summary, neither model is likely reliable with respect to estimates of future drawdown, especially in the case of a proposed substantial increase in pumping. Subsidence estimates may be considered more reliable than the drawdown estimates. Overall, the accuracy of long-term subsidence estimates are within a foot of actual long-term subsidence measurements as documented by the US Geological Survey in other areas of the model where subsidence has been measured. There is still a considerable degree of uncertainty in the subsidence estimates in an area where a large and concentrated increase in pumping is proposed.

A total of 33 scenarios were developed as part of this review, and 66 simulations were completed as part of this technical review: 33 scenarios simulated with the GAM, and 33 scenarios simulated with the HAGM. The scenarios simulated different numbers of wells, simulated alternate conditions where other pumping in Austin and Waller counties remained the same (representing an increase in modeled available groundwater), or were reduced to maintain the same modeled available groundwater for those counties, and simulated the effects of pumping from the underlying Jasper Aquifer rather than the Evangeline Aquifer at the same locations as proposed by the applicant. The 32 scenarios are summarized in Table 5.

Table 5. Summary of Simulations (EP Wells = Proposed Electro Purification Wells, MAG = Modeled Available Groundwater)

Scenario Number	Description
Base	Desired Future Condition/Modeled Available Groundwater Conditions
1	1 EP Well + MAG
2	2 EP Wells + MAG
3	3 EP Wells + MAG
4	4 EP Wells + MAG
5	5 EP Wells + MAG
6	6 EP Wells + MAG
7	7 EP Wells + MAG
8	8 EP Wells + MAG
9	9 EP Wells + MAG
10	10 EP Wells + MAG
11	1 EP Well, Reduce other pumping
12	2 EP Wells, Reduce other pumping
13	3 EP Wells, Reduce other pumping
14	4 EP Wells, Reduce other pumping
15	5 EP Wells, Reduce other pumping
16	6 EP Wells, Reduce other pumping
17	7 EP Wells, Reduce other pumping
18	8 EP Wells, Reduce other pumping
19	9 EP Wells, Reduce other pumping
20	10 EP Wells, Reduce other pumping
21	9 Evangeline, 1 Jasper + MAG
22	8 Evangeline, 2 Jasper + MAG
23	7 Evangeline, 3 Jasper + MAG
24	6 Evangeline, 4 Jasper + MAG
25	5 Evangeline, 5 Jasper + MAG
26	4 Evangeline, 6 Jasper + MAG
27	3 Evangeline, 7 Jasper + MAG
28	2 Evangeline, 8 Jasper + MAG
29	1 Evangeline, 9 Jasper + MAG
30	0 Evangeline, 10 Jasper + MAG
31	Conversion schedule + MAG
32	Conversion schedule, reduce other pumping

3.1 Base Scenario

The Base Scenario using the GAM was completed by simply running the model using the files used in Scenario 3 of GAM Run 10-023 (Oliver, 2010). This scenario included a simulation of 129 stress periods that covered the years 1891 to 2060. The Base Scenario using the HAGM was completed by using pumping file for the HAGM (1891 to 2009), and adding the pumping from Scenario 3 of GAM Run 10-023 for pumping from 2010 to 2060.

3.2 Proposed Project Pumping in Addition to the Modeled Available Groundwater

Scenarios 1 to 10 were completed by adding wells as noted in Table 5 (one in Scenario 1, two in Scenario 2, etc.) to the pumping file for the GAM or the HAGM as appropriate for the years 2014 to 2060. The simulation period was selected to be consistent with the applicant's analysis presented in the applicant's hydrogeological report. Locations of the wells are shown in Figure 1. Note that these simulations assumed that other pumping in Austin and Waller counties would not be reduced as a result of the proposed Electro Purification Project.

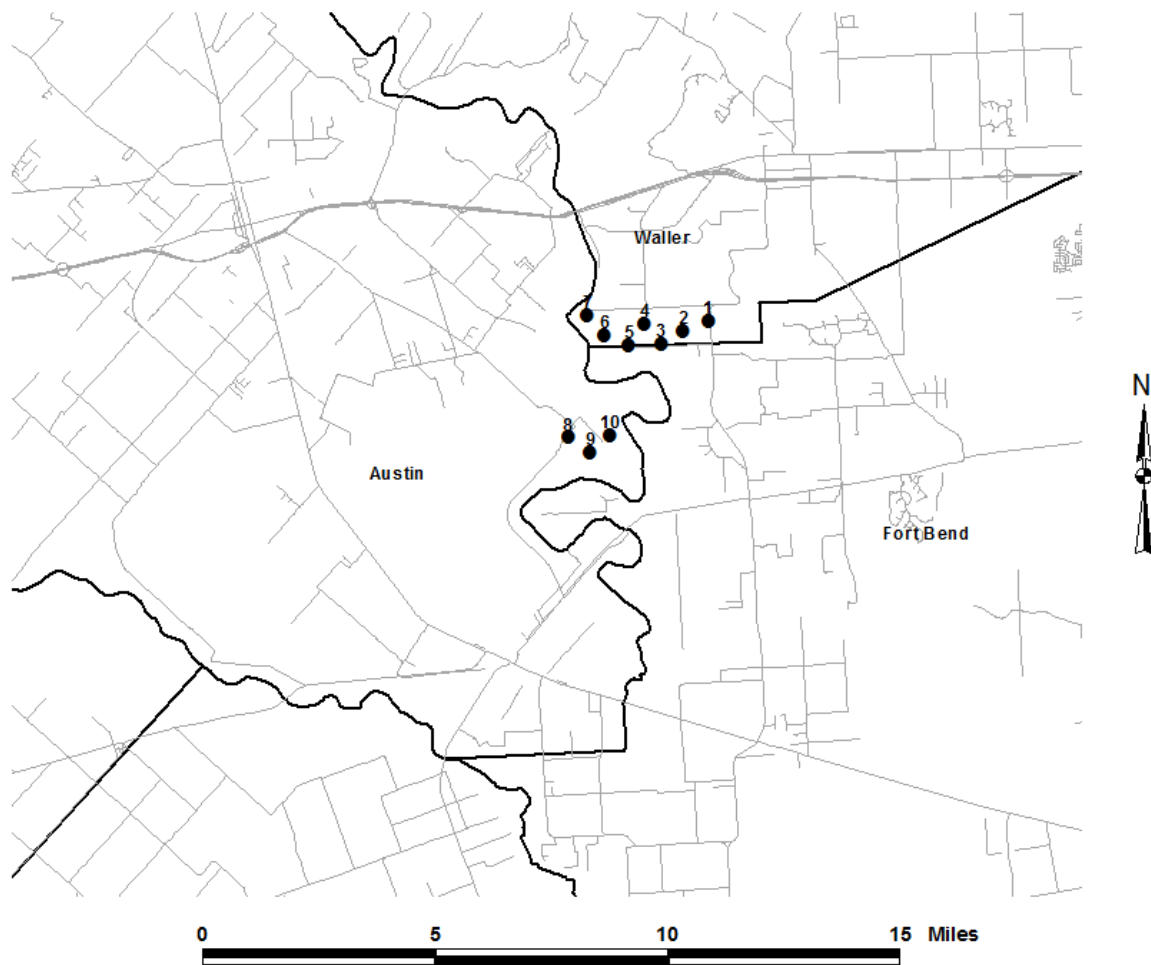


Figure 1. Proposed Electro Purification Wells in Austin and Waller Counties

As noted in the hydrogeologic report that was part of the application, the ten wells are located within five model cells. However, three wells are located in Model Row 53, Model Column 68 according to the applicant’s hydrogeologic report.

The TWDB designated each model cell with a county code. These county codes are used to calculate average drawdown and pumping for each county of model layer. Because a model grid cell may cover more than one county, the TWDB assigned a county code to the cell based on the location of the center point of the cell. In this case, Model Row 53, Column 68 is designated as a Fort Bend County cell, even though part of the cell is in Waller County. Thus, in order to complete comparisons with the Base Case as described above and compare drawdown and pumping of proposed Electro Purification pumping with the base case in the context of previous planning efforts, the wells were moved to the adjacent Waller County Cell (Row 52, Column 68) to maintain consistency with the TWDB files that were used in the desired future condition development process and calculation of the modeled available groundwater for Groundwater Management Area 14.

Table 6 summarizes the model row and column assignments for the proposed Electro Purification wells for each of the scenarios.

Table 6. Summary of Pumping Assignments in Model Grid for Scenarios 1 to 10

Scenario	Waller County Wells			Austin County Wells		Total Scenario Pumping (mgd)
	Pumping in Row 52, Column 68 (mgd)	Pumping in Row 52, Column 67 (mgd)	Pumping in Row 53, Column 69 (mgd)	Pumping in Row 54, Column 66 (mgd)	Pumping in Row 53, Column 65 (mgd)	
1	2	0	0	0	0	2
2	2	2	0	0	0	4
3	2	2	2	0	0	6
4	4	2	2	0	0	8
5	4	4	2	0	0	10
6	4	4	4	0	0	12
7	6	4	4	0	0	14
8	6	4	4	2	0	16
9	6	4	4	2	2	18
10	6	4	4	4	2	20

3.3 Proposed Project Pumping with Reductions in Other Pumping

The objective of Scenarios 11 to 20 was to simulate proposed project pumping while honoring the modeled available groundwater totals for each county. Thus, as proposed project pumping increased, other planned pumping in the simulation was decreased such that total pumping in each county equaled the modeled available groundwater.

Scenarios 11 to 20 were completed by adding pumping identical to those in Scenarios 1 to 10 (Table 6 presented shown above) to the pumping file for the GAM or the HAGM as appropriate for the years 2014 to 2060. The simulation period was selected to be consistent with the applicant’s analysis presented in their hydrogeological report. These simulations, however, assumed that other Evangeline Aquifer pumping in Austin and Waller counties would be reduced as a result of the proposed Electro Purification Project in order to maintain the modeled available groundwater values shown in Table 3. Thus, these scenarios represent changing the location of pumping as compared to Scenario 3 of GAM Run 10-023 (the basis for the desired future condition), but not the total pumping.

Table 7 summarizes the reduction in other Evangeline Aquifer pumping for each scenario. Recall that the Modeled Available Groundwater for the Evangeline Aquifer in Waller County is 41,027 acre-feet per year, and is 20,013 acre-feet per year in Austin County.

Table 7. Simulated Electro Purification (EP) Pumping, Other Pumping, and Total Pumping in Austin and Waller Counties for Scenarios 11 to 20

Scenario	Austin County			Waller County		
	EP Pumping (AF/yr)	Other Pumping (AF/yr)	Total Pumping (AF/yr)	EP Pumping (AF/yr)	Other Pumping (AF/yr)	Total Pumping (AF/yr)
11	0	20,013	20,013	2,240	38,787	41,027
12	0	20,013	20,013	4,481	36,546	41,027
13	0	20,013	20,013	6,721	34,306	41,027
14	0	20,013	20,013	8,961	32,066	41,027
15	0	20,013	20,013	11,201	29,826	41,027
16	0	20,013	20,013	13,442	27,585	41,027
17	0	20,013	20,013	15,682	25,345	41,027
18	2,240	17,773	20,013	15,682	25,345	41,027
19	4,481	15,532	20,000	15,682	25,345	41,027
20	6,721	13,292	20,000	15,682	25,345	41,027

3.4 Simulation of Jasper Aquifer Pumping

Scenarios 21 to 30 investigated the effect of completing the proposed Electro Purification Project wells into the deeper Jasper Aquifer, which is deeper than the Evangeline Aquifer and is separated from the Evangeline Aquifer by the Burkeville Confining Layer. In these scenarios, all ten proposed wells were assumed to be operational, but the number of Evangeline wells and the number of Jasper wells were varied. Recall from Scenario 10 that all ten proposed Electro Purification wells were assumed completed in the Evangeline Aquifer, and there is no reduction in other pumping in Austin and Waller counties. Using Scenario 10 as a starting point, Scenario 21 assumed that one well was completed in the Jasper and the other nine were completed in the Evangeline. Scenario 22 assumed two Jasper wells and eight Evangeline wells. Finally Scenario 30 assumed 10 Jasper wells and no Evangeline wells. For each scenario, pumping was added for each cell for the years 2014 to 2060 in addition to the pumping from Scenario 3 of GAM Run 10-023. The simulation period was selected to be consistent with the applicant’s analysis presented in their hydrogeological report.

3.5 Simulation of Conversion Schedule

As discussed in Section 2.3 of this report, and summarized previously in Table 4 of this report, the applicant has outlined the conversion schedule for the cities of Richmond and Rosenberg, and their Groundwater Reduction Plan partners. In summary, the applicant stated that pumping will begin in 2015 (3.388 mgd, or 3,795 AF/yr), increase in 2025 to 9.074 mgd (or 10,164 AF/yr), and increase again in 2030 to 9.907 mgd (or 11,097 AF/yr).

This conversion schedule was simulated by locating wells in three cells that contain proposed project wells in Waller County and distributing the pumping amongst the cells evenly for each of the three periods as shown in Table 8. Austin County well locations were not included for these scenarios in order to avoid the need to construct a pipeline under the Brazos River.

In Scenario 31, the pumping was added to the pumping file for the GAM or the HAGM as appropriate for the years 2015 to 2060 as shown in Table 8. Thus, Scenario 31 represents pumping in addition to the modeled available groundwater similar to Scenarios 1 to 10.

Table 8. Summary of Pumping Assignment for Scenarios 31 and 32

Period	Pumping in Row 52, Col 68 (mgd)	Pumping in Row 52, Col 67 (mgd)	Pumping in Row 53, Col 69 (mgd)	Total EP Pumping (mgd)
2015 to 2024	1.70	1.70	0.00	3.40
2025 to 2029	3.02	3.02	3.02	9.06
2030 to 2060	3.30	3.30	3.30	9.90

In Scenario 32, other pumping in Waller County was reduced in order to simulate the effects of changing the location of pumping as compared to Scenario 3 of GAM Run 10-023 (the basis for the desired future condition), but maintaining total pumping equal to the modeled available groundwater similar to Scenarios 11 to 20. A summary of simulated Electro Purification pumping, other Waller County pumping, and total pumping for Scenarios 31 and 32 is presented in Table 9.

Table 9. Summary of Pumping in Waller County for Scenarios 31 and 32

Scenario	Time Period	Waller County		
		EP Pumping (AF/yr)	Other Pumping (AF/yr)	Total Pumping (AF/yr)
31	2015 to 2024	3,795	41,027	44,822
31	2024 to 2029	10,164	41,027	51,191
31	2030 to 2060	11,097	41,027	52,124
32	2015 to 2024	3,795	37,232	41,027
32	2024 to 2029	10,164	30,863	41,027
32	2030 to 2060	11,097	29,930	41,027

3.6 Simulations with Simple Local-Scale MODFLOW Model

3.6.1 Background

In an attempt to highlight and address one of the limitations of the GAM and HAGM with respect to the proposed project, an alternative simple local-scale model using MODFLOW was developed. This local-scale model simulated a postulated condition that the Evangeline Aquifer can be subdivided into an upper and lower aquifer zones that are separated by a confining unit as shown in Figure 2.

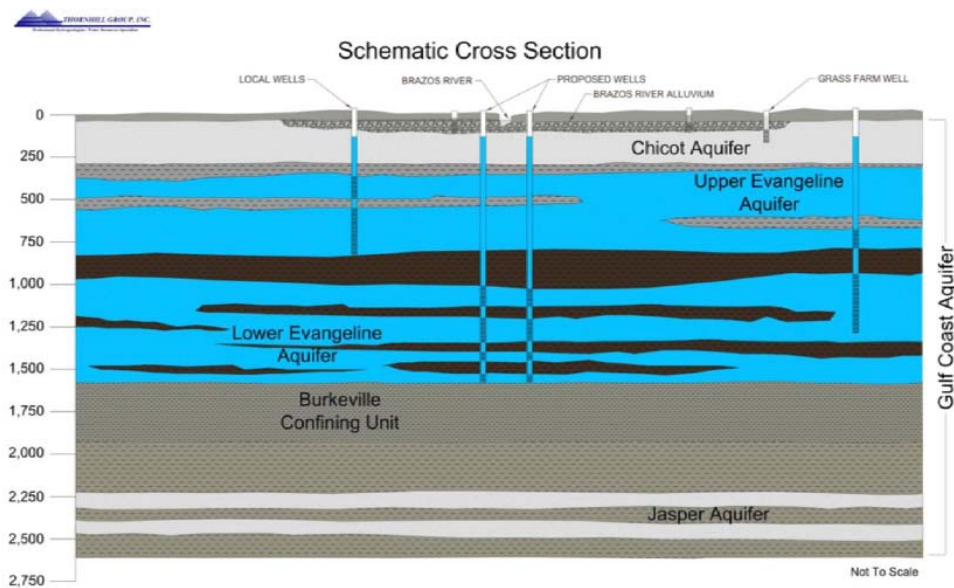


Figure 2. Applicant’s Postulated Conceptualization of an Upper Evangeline Aquifer and Lower Evangeline Aquifer

This schematic cross-section was provided by the applicant's hydrogeology consultant. In essence, the applicant has stated that, if a confining unit exists between the Upper Evangeline Aquifer and the Lower Evangeline Aquifer, it is likely that pumping in the Lower Evangeline Aquifer will have less drawdown impact on wells completed in the Upper Evangeline Aquifer as compared to a situation where no such intermediate and extensive confining unit were present. However, it must be noted that if an extensive and continuous intermediate confining unit were present, the drawdown of groundwater elevations associated with the proposed project may result in additional subsidence as compared to a situation without extensive clay layers in the Evangeline Aquifer.

This postulated subdivision of the Evangeline Aquifer is not part of the hydrogeologic framework of the GAM or HAGM since these are regional models. However, if this localized condition exists at the proposed project site, the simple model can be a useful tool to understand the relationships between pumping in the deeper portions of the Evangeline Aquifer (as proposed by Electro Purification). Furthermore, the assumed sand and clay ratios in the immediate area of the proposed Electro Purification wells is not well known. The simple MODFLOW model was used to understand the relative effect of alternative sand and clay ratios in the aquifer units on drawdown and subsidence, and the effect of the postulated intermediate confining layer immediately above the proposed production unit of the Electro Purification wells.

As developed more fully below, if this project proceeds to a testing and drilling phase, it is recommended that the subsequent evaluation of the test data include expanding this type of numerical analysis. Specifically, hydrogeologic framework data collected during the drilling should be used to construct a numerical model that conforms better to local hydrogeologic conditions, and data from any aquifer test be evaluated with local numerical model to assess and update estimated impacts of the proposed pumping.

3.6.2 Simple MODFLOW Model Grid, Layering, and Boundary Conditions

The simple MODFLOW model simulated an idealized flow system of about 50 miles by 50 miles. The flow system is discretized into a grid of cells defined by 100 rows by 100 columns, with each cell 3,000 ft by 3,000 ft, which corresponds to the proposed well spacing of the Electro Purification wells. Thus, there is only one well in each cell of this model.

The model contains four layers:

- Layer 1 represents the Chicot Aquifer, and is 200 feet thick
- Layer 2 represents the "upper" Evangeline Aquifer, and is 500 feet thick
- Layer 3 represents the confining unit between the "upper" and "lower" Evangeline Aquifer, and is 200 feet thick
- Layer 4 represents the "lower" Evangeline, is 700 feet thick.

Proposed Electro Purification wells were simulated to pump water from Layer 4, the "lower" Evangeline.

The model grid and boundary conditions are shown in Figure 3. The regional flow in the system is from top to bottom of Figure 3, with a constant head boundary difference of 30 feet between north

and south boundaries (blue lines on Figure 3). In addition, recharge was assumed to be 0.05 inches per year. The red cells on Figure 3 represent the locations of the proposed Electro Purification wells (one per cell), and pumping was set to 20 million gallons per day for all simulations for 50 years.

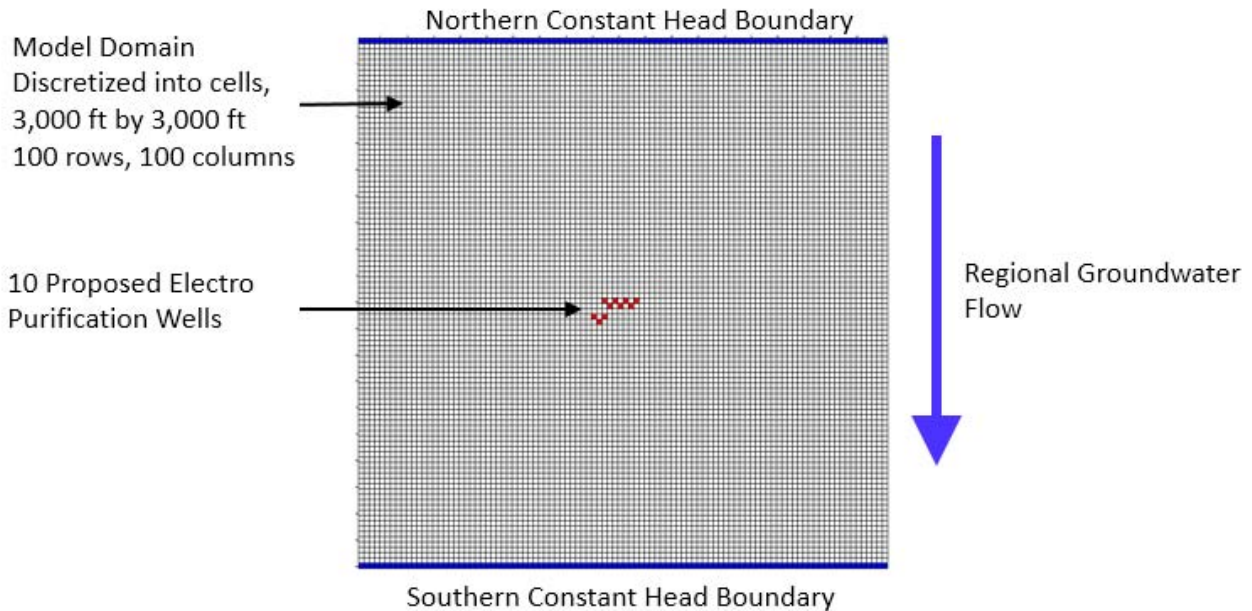


Figure 3. Model Grid and Boundary Conditions of Simple MODFLOW model

3.6.3 Model Parameters for the Simple MODFLOW model

For the purposes of this evaluation, basic input parameters included horizontal hydraulic conductivity (sand and clay), specific storativity, and inelastic specific storativity. These basic input parameters were then used with model layer thickness and clay percentage assumptions to develop appropriate model input parameters.

Parameters from the GAM and HAGM were evaluated, as were parameters identified in the hydrogeology report associated with Electro Purification's application. Based on this review, Table 10 summarizes the starting parameters that were used in this analysis. The objectives of this analysis were to investigate the general relationship between the effects of clay content in the aquifer layers and the postulated intermediate confining layer within the Evangeline Aquifer on a local scale on drawdown and subsidence. As developed in the next section, these initial parameters were varied in a series of simulations as part of this analysis.

Table 10. Initial Parameters for Simple MODFLOW Model

Model Layer	1	2	3	4
Unit Designation	Chicot	Upper Evangeline	Evangeline Confining Unit	Lower Evangeline
Layer Thickness (ft)	200	500	200	700
Horizontal Sand Hydraulic Conductivity (ft/day)	20	18	16	14
Horizontal Clay Hydraulic Conductivity (ft/day)	0.01	0.01	0.01	0.01
Assumed Clay Percentage	40	60	85	60
Assumed Clay Thickness (ft)	80	300	170	420
Assumed Sand Thickness (ft)	120	200	30	280
Equivalent Layer Hydraulic Conductivity (ft/day)	12.004	7.206	2.409	5.606
Equivalent Layer Vertical Hydraulic Conductivity (ft/day)	0.0250	0.0167	0.0118	0.0167
Layer Transmissivity (ft²/day)	2,401	3,603	482	3,924
Layer Transmissivity (gpd/ft)	17,958	26,950	3,603	29,353
Specific Storage (ft⁻¹)	5.00E-06	6.00E-08	1.50E-08	4.30E-08
Storativity (dimensionless)	1.00E-03	3.00E-05	3.00E-06	3.01E-05
Inelastic Specific Storativity (ft⁻¹)	8.70E-05	1.50E-05	2.50E-05	2.00E-05
Inelastic Storativity (dimensionless)	6.96E-03	4.50E-03	4.25E-03	8.40E-03
Elastic Storativity (dimensionless)	6.96E-05	4.50E-05	4.25E-05	8.40E-05

The parameters presented above were based on the following:

- Layer thickness was assigned based on the model framework as suggested by the project applicant's hydrogeology report.
- Horizontal sand hydraulic conductivity was assumed to be 20 ft/day in the upper layer, and decreased 2 ft/day with each layer to simulate deeper burial and compaction of the sand units.
- Horizontal clay hydraulic conductivity was assumed to be 0.01 ft/day for all layers.
- Assumed clay percentage in layers 1, 2 and 4 were assumed after reviewing average clay content data used in the GAM and HAGM in the area of the proposed Electro Purification wells. Assumed clay content in layer 3 was assumed to represent a confining unit (low sand content)
- Assumed clay thickness was calculated using the clay percentage and total layer thickness.
- Assumed sand thickness was calculated as total layer thickness minus layer clay thickness.

- The equivalent layer horizontal conductivity was calculated using the layer-thickness weighted mean of the sand and clay horizontal hydraulic conductivity following a method documented by Fitts (2002, pg. 52).
- The equivalent layer vertical hydraulic conductivity was calculated using the layer-thickness weighted harmonic mean of the sand and clay horizontal hydraulic conductivity following a method documented by Fitts (2002, pg. 52).
- Layer transmissivity (expressed in ft²/day and gpd/ft) is the product of the equivalent layer horizontal hydraulic conductivity and layer thickness.
- Specific storage was assumed based on a review of GAM and HAGM parameters.
- Storativity is the product of specific storage and model layer thickness
- Inelastic specific storage was assumed based on a review of GAM and HAGM documentation.
- Inelastic storativity is the product of inelastic specific storage and model clay layer thickness
- Elastic storativity is assumed to be equal to inelastic storativity divided by 100, as was assumed in the GAM and HAGM.

3.6.4 Simulations with the Simple MODFLOW model

Two sets of 50-year simulations were completed:

- Simulations 1 to 11 varied the clay content of model layers 1, 2, and 4 between 25 and 75 percent, in 5 percent increments
- Simulations 12 to 20 varied the clay content of model layer 3 (the postulated intermediate confining layer) between 50 and 90 percent, in 5 percent increments

Details of assumed clay content in each layer are summarized in Table 11. All basic parameter values remained unchanged from the values in Table 10.

Table 11. Summary of Layer Clay Percentages Assumptions for Each Simulation with Simple MODFLOW Model

Simulation	Percent Clay in Layer			
	Layer 1	Layer 2	Layer 3	Layer 4
1	25	25	85	25
2	30	30	85	30
3	35	35	85	35
4	40	40	85	40
5	45	45	85	45
6	50	50	85	50
7	55	55	85	55
8	60	60	85	60
9	65	65	85	65
10	70	70	85	70
11	75	75	85	75
12	40	60	90	60
13	40	60	85	60
14	40	60	80	60
15	40	60	75	60
16	40	60	70	60
17	40	60	65	60
18	40	60	60	60
19	40	60	55	60
20	40	60	50	60

4.0 Simulated Effects of Proposed Pumping on Registered and Permitted Wells Using GAM and HAGM

4.1 Location of Registered and Permitted Wells

Figure 4 presents the locations of 379 wells completed in the Chicot Aquifer that are less than 10 miles from at least one proposed Electro Purification well. These wells include registered and permitted wells from the Bluebonnet GCD database in Austin and Waller counties (as of July 31, 2013), and wells in the TWDB database in Austin, Fort Bend and Waller counties. Figure 5 presents the locations of 115 wells from the same sources that are completed in the Evangeline Aquifer.

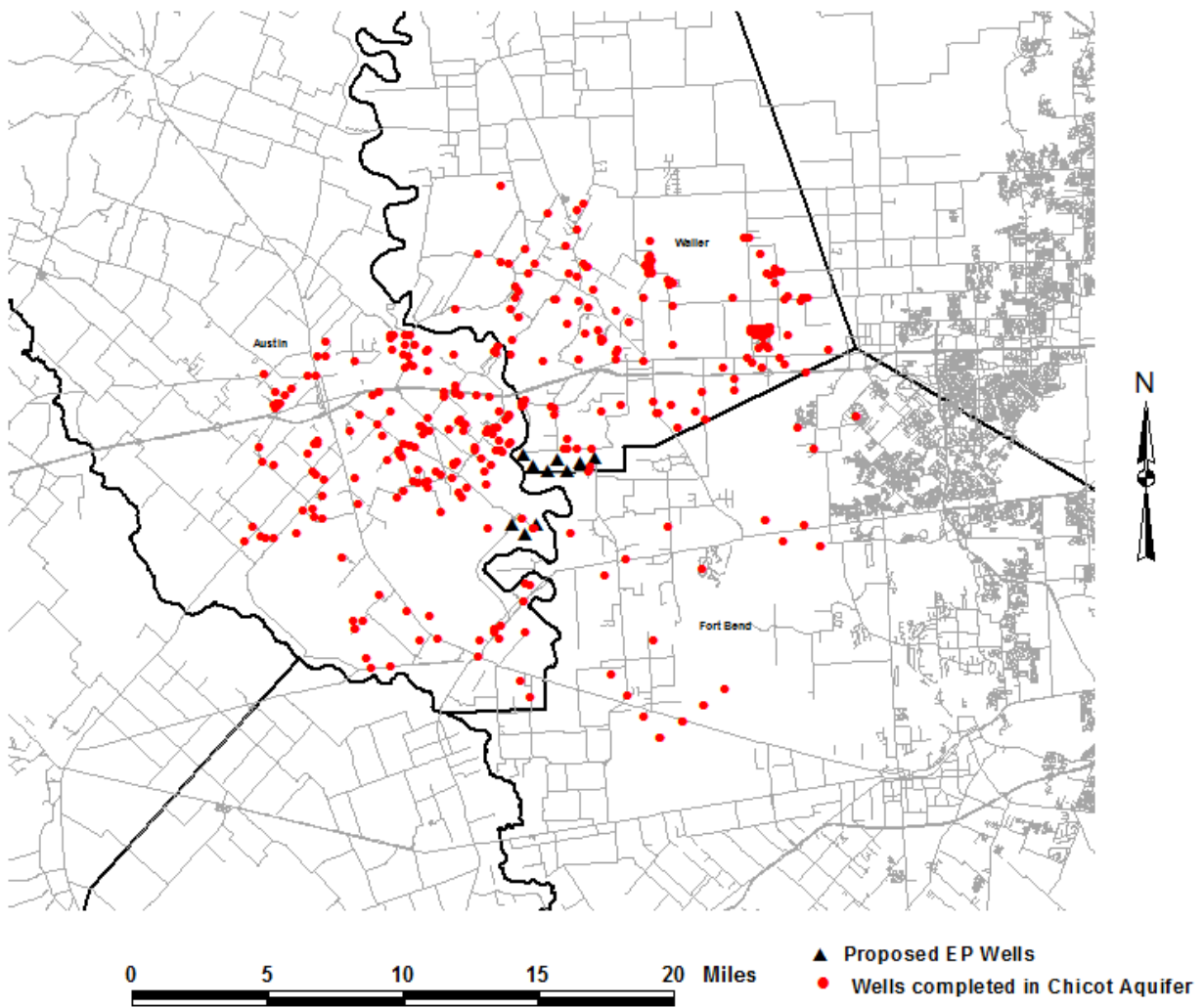


Figure 4. Registered and Permitted Wells, and Wells from TWDB database within Ten Miles of at least one EP Well - Chicot Aquifer

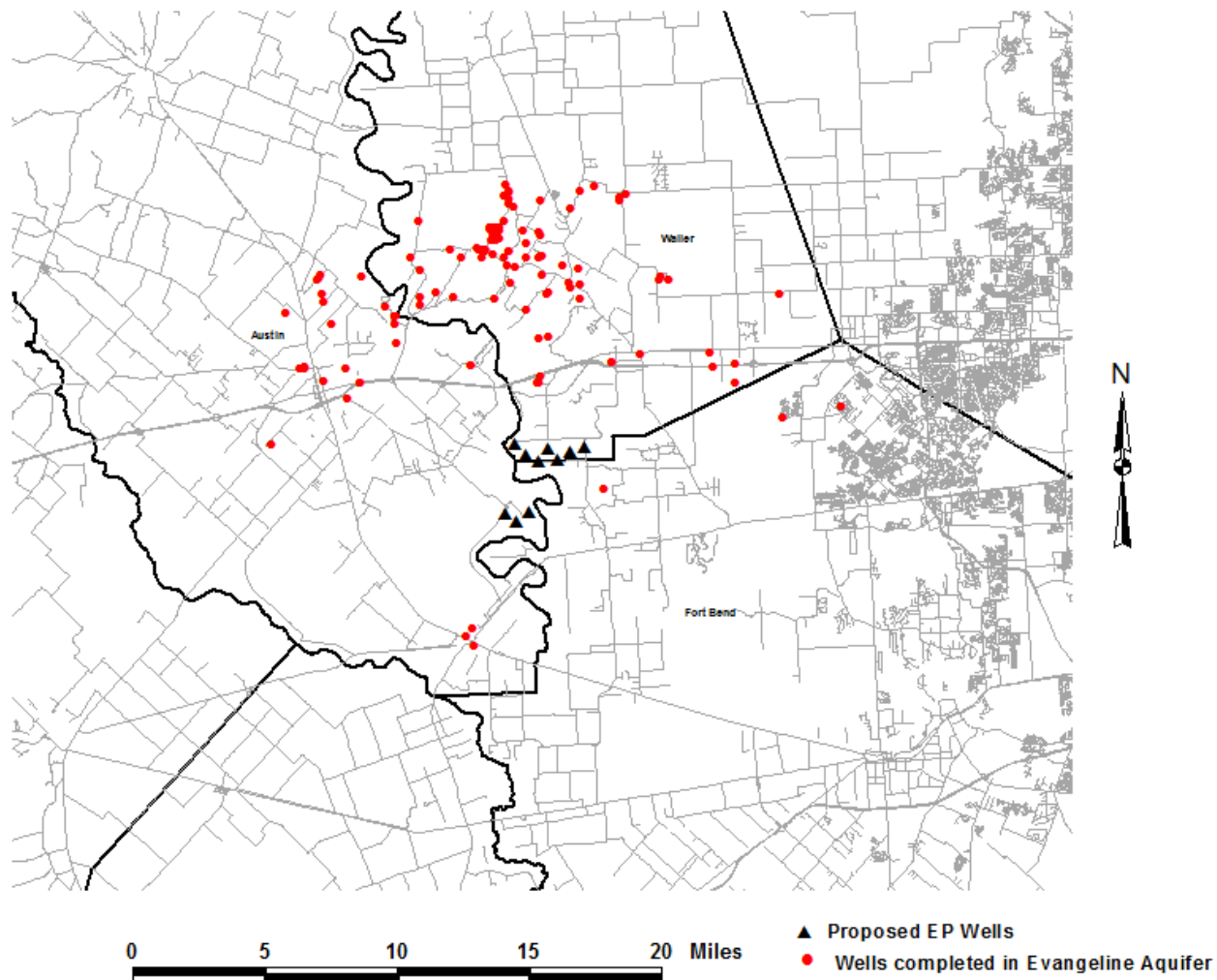


Figure 5. Registered and Permitted Wells, and Wells from the TWDB Database within Ten Miles of at least one EP Well - Evangeline Aquifer

Figure 6 presents a histogram of well distance to the closest Electro Purification well for wells completed in the Chicot Aquifer. Figure 7 presents a histogram of well distance to the closest Electro Purification well for wells completed in the Evangeline Aquifer.

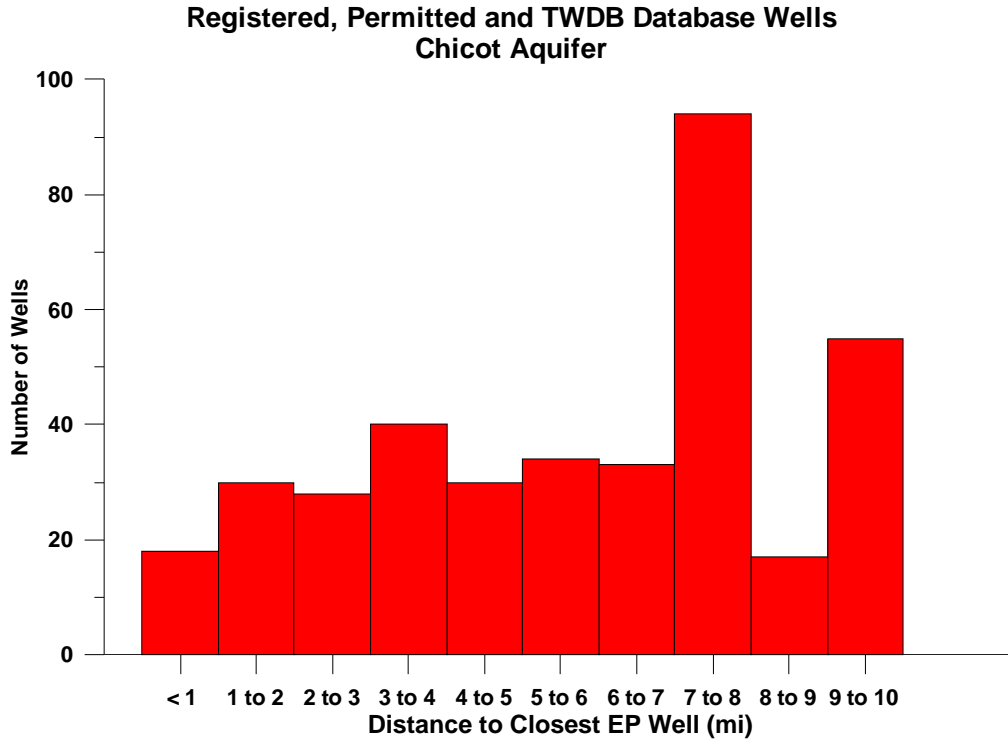


Figure 6. Histogram of Distances to Wells - Chicot Aquifer

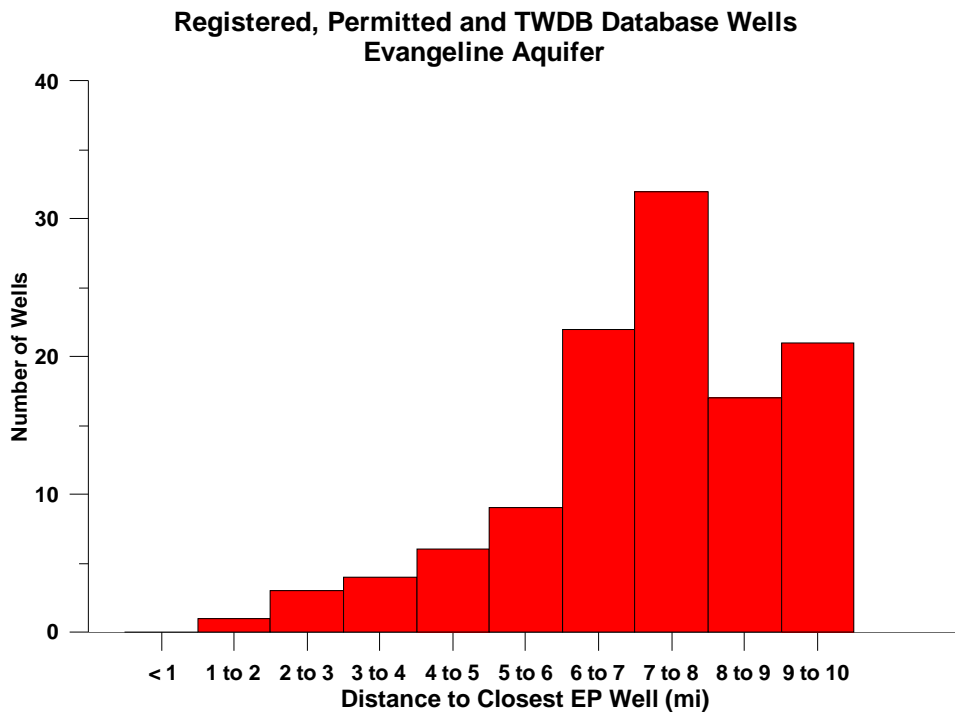


Figure 7. Histogram of Distances to Wells - Evangeline Aquifer

4.2 Simulations Results

Simulation results for each well location are presented in the form of tables and maps in Appendix C. Tables and maps include well-by-well estimates of drawdown from 2008 to 2060 for each well (379 Chicot Aquifer wells and 115 Evangeline Aquifer wells).

- The baseline scenario (DFC/MAG simulation)
- Scenario 3 (Electro Purification pumping = 6 million gallons per day or mgd)
- Scenario 10 (Electro Purification pumping = 20 mgd)
- Scenario 31 (Electro Purification pumping = 9.9 mgd)

4.2.1 Drawdown Tables

Four tables are included as follows:

- Table C-1 (Chicot Aquifer – Estimated Drawdown from the GAM)
- Table C-2 (Chicot Aquifer – Estimated Drawdown from the HAGM)
- Table C-3 (Evangeline Aquifer – Estimated Drawdown from the GAM)
- Table C-4 (Evangeline Aquifer – Estimated Drawdown from the HAGM)

Wells are designated by the well number used by Bluebonnet GCD. Wells that use the State Well Number were obtained from the TWDB database.

Drawdown is calculated as the difference between estimated groundwater elevation in 2008 and the estimated groundwater elevation in 2060. This was the drawdown calculation time period used by Groundwater Management Area 14 in establishing the desired future conditions for the various components of the Gulf Coast Aquifer (Chicot, Evangeline, Burkeville, and Jasper).

The total estimated drawdown is included as well as the estimated drawdown that can be attributed to the proposed Electro Purification pumping for a specific scenario. For example, if the baseline scenario yields a drawdown estimate at a specific point of 5 feet, and the drawdown for a particular scenario of Electro Purification pumping at that same point is 12 feet, then the drawdown attributed to the Electro Purification pumping is 12 feet minus 5 feet, or 7 feet.

Table 12 summarizes the results of Tables C-1 and C-2 for the wells completed in model layer 1 (Chicot Aquifer). Note that ranges of drawdown are presented for three distance groups. The closest Chicot Aquifer well used in this analysis is 0.15 miles from a proposed Electro Purification well.

Table 13 summarizes the results of Tables C-3 and C-4 for the wells completed in model layer 2 (Evangeline Aquifer). Note that ranges of drawdown are presented for three distance groups. The closest Evangeline Aquifer well used in this analysis is 1.7 miles from a proposed Electro Purification well.

Table 12. Summary of Drawdown Estimates (2008 to 2060) for Wells Completed in the Chicot Aquifer – Estimates from Tables C-1 and C-2

Distance to EP Wells	Scenario	Simulated Drawdown (ft)		Drawdown Attributable to EP (ft)	
		GAM	HAGM	GAM	HAGM
0.15 to 0.5 mile	Base	26 to 32	38 to 43	0	0
	Scenario 3 (6 mgd)	38 to 44	48 to 53	12 to 15	9 to 13
	Scenario 10 (20 mgd)	66 to 79	69 to 80	41 to 48	32 to 39
	Scenario 31 (9.9 mgd)	46 to 52	54 to 59	19 to 25	15 to 20
0.5 to 1 mile	Base	26 to 28	39 to 44	0	0
	Scenario 3 (6 mgd)	41 to 44	51 to 53	12 to 16	10 to 13
	Scenario 10 (20 mgd)	74 to 78	75 to 81	43 to 50	35 to 41
	Scenario 31 (9.9 mgd)	51 to 53	57 to 60	18 to 25	15 to 20
1 to 2 miles	Base	23 to 36	37 to 47	0	0
	Scenario 3 (6 mgd)	34 to 45	48 to 54	8 to 15	6 to 13
	Scenario 10 (20 mgd)	57 to 80	67 to 81	31 to 49	23 to 40
	Scenario 31 (9.9 mgd)	41 to 53	53 to 60	12 to 23	10 to 20

Table 13. Summary of Drawdown Estimates (2008 to 2060) for Wells Completed in the Evangeline Aquifer - Estimates from Tables C-3 and C-4

Distance to EP Wells	Scenario	Simulated Drawdown (ft)		Drawdown Attributable to EP (ft)	
		GAM	HAGM	GAM	HAGM
1.7 to 3 miles	Base	25 to 28	41 to 51	0	0
	Scenario 3 (6 mgd)	50 to 57	66 to 79	25 to 32	25 to 31
	Scenario 10 (20 mgd)	96 to 116	112 to 136	72 to 90	71 to 89
	Scenario 31 (9.9 mgd)	65 to 76	81 to 96	40 to 51	40 to 51
3 to 5 miles	Base	23 to 43	38 to 71	0	0
	Scenario 3 (6 mgd)	38 to 50	56 to 78	7 to 18	7 to 18
	Scenario 10 (20 mgd)	63 to 78	86 to 106	30 to 54	28 to 54
	Scenario 31 (9.9 mgd)	46 to 54	66 to 85	10 to 29	10 to 29
5 to 7 miles	Base	15 to 26	31 to 88	0	0
	Scenario 3 (6 mgd)	21 to 34	39 to 95	6 to 13	6 to 13
	Scenario 10 (20 mgd)	33 to 58	54 to 110	18 to 36	19 to 37
	Scenario 31 (9.9 mgd)	24 to 42	43 to 93	9 to 20	9 to 20

4.2.2 Drawdown Maps

Figures C-1 to C-16 are maps of estimated total drawdown for:

- The baseline scenario (DFC/MAG simulation)
- Scenario 3 (Electro Purification pumping = 6 mgd)
- Scenario 10 (Electro Purification pumping = 20 mgd)
- Scenario 31 (Electro Purification pumping = 9.9 mgd)

Each of these groups has four maps. Each map pairs a particular aquifer (Chicot and Evangeline) and a particular model (GAM and HAGM).

Figures C-17 to C-28 are maps of estimated drawdown attributed to a specific Electro Purification pumping scenario:

- Scenario 3 (Electro Purification pumping = 6 mgd)
- Scenario 10 (Electro Purification pumping = 20 mgd)
- Scenario 31 (Electro Purification pumping = 9.9 mgd)

As in Tables C-1 to C-4, these maps present the difference in drawdown (base case to the particular scenario) at each well location.

4.3 Limitations of the Simulation Results

As previously described above and more fully developed in Appendix A, estimates of drawdown using the GAM and HAGM are likely not reliable, especially for simulations with large increases in future pumping, such as the project proposed by Electro Purification. This limitation is directly related to the use of the General Head Boundary (GHB) package in MODFLOW to simulate the recharge and groundwater-surface water interactions in the outcrops of the model layers. As stated in Kasmarek and Robinson (2004, pg. 43) and Kasmarek (2012, pg. 15), the GHB package allows the simulated water table of an aquifer system to function as a head-dependent flux boundary. The rate of flow between the water table and the adjacent deeper zone of the system is controlled by the difference between that water table (a specified head) and the head in the adjacent deeper zone (which changes with model simulation time) and by the vertical hydraulic conductance between the water table and the immediately deeper zone.

As described in Appendix A, the net effect of using the GHB package in this manner is that GHB flows into the aquifer system represent a combined inflow of recharge from precipitation and inflow from streams in the outcrop areas of the model. There is a significant increase in inflow from the GHB boundary through time into the aquifer that essentially means that there is an increase in the sum of recharge from precipitation plus recharge from streamflow. This is coincident with increased pumping in the area. For example: in Austin County, simulated GHB inflows rise from less than 6,000 AF/yr in 1891 to slightly over 16,000 AF/yr by 2009, and then are simulated to increase to almost 24,000 AF/yr by 2060 under the DFC condition. In Waller County, HAGM simulated inflows are less than GHB inflows simulated by the GAM. In the GAM simulation, inflows are simulated to be slightly over 5,000 AF/yr in 1891 and increase to about 30,000 AF/yr in 2009, and then are simulated to increase to about 45,000 AF/yr in 2060.

The model was approved for publication by the US Geological Survey, and used by the Texas Water Development Board for calculation of the modeled available groundwater values that are associated with the desired future conditions. The calibration of the model was considered reasonable for a regional model. This would suggest that the impact of increasing GHB flows into the groundwater flow system is somehow integrated in other model parameters in order to achieve a reasonable calibration (matching simulated groundwater elevations and actual measured groundwater elevations). Historic pumping was one such estimate.

Generally, the pumping estimates from 1891 to 1997 are the same between the GAM and the HAGM. Although both models have the same estimates of pumping in Austin and Waller Counties from 1891 to 1997, neither model seemed to have fully incorporated previous estimates of pumping in Austin and Waller Counties from 1930 to 1965 (Wilson, 1967, pg. 39).

Wilson (1967) estimated the peak of pumping from 1945 to 1965 to be much higher than either the GAM or HAGM estimates. Wilson estimated that Austin County irrigation pumping peaked in about 1954 (about 11,000 AF/yr) while the USGS models estimated a peak in about 1960 of about 8,000 AF/yr (Figure 24). Wilson estimated that Waller County irrigation pumping peaked in about 1954 (about 51,000 AF/yr) while the USGS models estimated a peak in about 1960 of about 25,000 AF/yr (Figure 39). Although Wilson (1967) is listed as a reference by Kasmarek and Robinson (2004), there does not appear to be a specific citation where the information from that effort was used in Kasmarek and Robinson (2004). This observation has limited effect on the four counties of interest to the HAGM (Fort Bend, Galveston, Harris, and Montgomery). However, there are implications when evaluating the potential limitations of the models use in the Bluebonnet GCD area, and for the development of desired future conditions, especially in the instance where future pumping approaches and/or exceeds the estimates of historic pumping of Wilson (1967), as in the case of the proposed Electro Purification project. If the model had accurately incorporated these historic pumping estimates into the model, there would be the ability to compare the impacts of historic high pumping with estimates of proposed pumping by Electro Purification.

It is also possible that calibration of hydraulic conductivity was impacted by the use of GHBs to simulate recharge and groundwater-surface water interaction. If the resulting hydraulic conductivity values are too low as a result, drawdown estimates under a scenario of large increases in pumping as compared to the historic pumping may result in an overestimation of drawdown.

As a result, future pumping increases are likely to result in less confidence in drawdown calculations since it is possible that an unreasonable amount of inflow is induced into the aquifer system, or the hydraulic conductivity values are unreasonably low to account for the unusual approach of using GHBs to simulate recharge and groundwater-surface water interaction. This would likely have an impact on drawdown estimates (i.e. underestimate drawdown if the increases in inflow are unreasonable or an overestimate if the hydraulic conductivities are too low).

In conclusion, the estimates presented in Appendix C, and discussed in Section 4.2 demonstrate the potential drawdown impacts on individual wells as estimated by the GAM and HAGM. However, these results are considered unreliable, and may likely represent over-estimates of drawdown. Local scale testing and developing a local scale model based on those results are recommended to overcome these limitations.

5.0 Simulated Effects of Proposed Pumping on Desired Future Conditions

As discussed earlier, the Northern Gulf Coast GAM was used by the groundwater conservation districts in Groundwater Management Area 14 in the development of desired future conditions for the Gulf Coast Aquifer in 2010. The Texas Water Development Board used the Northern Gulf Coast GAM to develop the modeled available groundwater values for the groundwater conservation districts and the regional planning groups. As part of the review of Electro Purification's application, the simulation results were processed to evaluate the effect of the proposed pumping on the desired future condition.

Subsequent to the establishment of desired future conditions, the USGS, in cooperation with the Harris-Galveston Subsidence District, the Fort Bend Subsidence District, and the Lone Star Groundwater Conservation District, developed the Houston Area Groundwater Model (HAGM). The primary area of interest in the development of the HAGM was Fort Bend, Galveston, Harris, and Montgomery Counties. The primary objective of the model was to develop an updated tool to support the subsidence district's efforts to update their regulatory plan. Since its release, the groundwater conservation districts in Groundwater Management Area 14 have expressed an interest to possibly using the HAGM to update the desired future conditions, which must be re-adopted by May 2016.

As described earlier, both models were used in this analysis. Appendix D contains tables and graphs of the results of the simulations in the context of potential impacts to desired future conditions.

Tables D-1 to D-3 present the estimated average drawdown by county and model layer for Austin County (Table D-1), Fort Bend County (Table D-2), and Waller County (Table D-3). Drawdowns are calculated from the period 2008 to 2060, as was done for the desired future condition calculation. Please note that estimates from the GAM and HAGM are included.

Tables D-4 to D-6 are in a format similar to Tables D-1 to D-3, but present the estimated average drawdown by county and model layer that is attributable to the proposed Electro Purification project. Table D-4 presents the results for Austin County, Table D-5 presents the results for Fort Bend County, and Table D-6 presents the results for Waller County. These drawdowns were calculated by subtracting the scenario-specific estimate from the baseline scenario estimate. For example, if the county estimate for drawdown in a specific layer for a specific Electro Purification scenario is 40 feet, and the estimated drawdown for that model layer in that county from the base case is 30 feet, the drawdown that is "attributable" to the Electro Purification pumping is 10 feet.

Tables D-4 to D-6 provide a means to quickly view the impact of the proposed pumping on the desired future conditions. Positive numbers mean that the scenario drawdown is more than the baseline scenario (the desired future condition scenario). Negative numbers mean that the scenario drawdown is less than the baseline scenario (the desired future condition scenario). Scenarios 1 to 10, and 31 all involved adding the proposed Electro Purification pumping to the pumping assumed in the baseline scenario. Thus, it is not surprising that the drawdown increases in these scenarios as compared to the baseline scenario. Scenarios 11 to 20, and 32 all involved reducing other pumping in each county such that the proposed Electro Purification pumping plus the other pumping equaled

the modeled available groundwater (the pumping in the baseline scenario). In Austin County, scenario drawdown estimates attributable to the proposed Electro Purification pumping for Scenarios 11 to 20, and 32 are positive, meaning that the drawdown is more than the baseline drawdown despite the same amount of total pumping. This is due to the redistribution of the pumping, and highlights the importance of spatial distribution of pumping on the estimated average drawdown on a county-model layer scale. In contrast, in Waller County, scenario drawdown estimates attributable to the proposed Electro Purification pumping for Scenarios 11 to 20, and 32 are negative, meaning that the drawdown is less than the estimated baseline drawdown despite the same amount of pumping.

These tables provide a snapshot of the final drawdown in 2060 for all scenarios and for all relevant county-model layer groups. Figures D-1 to D-72 present the time-plots of drawdown from 2008 to 2060 for each county-model layer group, for each scenario, and for each model. The cover sheet summarizes the organization of the graphs.

5.1 Discussion of Results

As described previously, the limitations of the model suggest that the confidence in these drawdown estimates could be considered low. However, the GAM was used by the groundwater conservation districts in Groundwater Management Area 14 as part of the process to develop desired future conditions, and by the Texas Water Development Board to develop modeled available groundwater estimates. In addition, the HAGM was developed as a tool for the subsidence districts regulatory program, and is being considered for use in the next round of joint groundwater planning (desired future conditions and modeled available groundwater).

The value in this analysis is to understand differences in the results of the two models as they relate to scenario comparison. For example, it can be seen that the same pumping yields different results in the GAM and HAGM on a county-model layer scale. Table 14 summarizes the drawdown estimates of the GAM and HAGM for each of the three counties of interest (Austin, Fort Bend and Waller).

Table 14. Summary of Baseline Scenario Drawdowns

Aquifer	Model	Austin County Drawdown in 2060 (ft)	Fort Bend County Drawdown in 2060 (ft)	Waller County Drawdown in 2060 (ft)
Chicot	GAM	17.13	20.00	7.48
Chicot	HAGM	29.00	27.35	26.20
Evangelina	GAM	9.94	24.18	7.97
Evangelina	HAGM	18.51	15.37	32.10

Note that in Austin and Waller counties, HAGM estimates of drawdown in 2060 are higher than the estimates from the GAM for the same amount of pumping for both the Chicot and Evangelina. However, in Fort Bend County, while the HAGM estimates of drawdown is higher than the GAM for the Chicot, the estimated drawdown from the HAGM is lower than the GAM for the Evangelina.

The differences between the results of the two models suggests that there is considerable uncertainty in the model estimates of drawdown.

In general, the Electro Purification scenarios that involve increases in pumping cause increases in drawdown that may not be consistent with the desired future condition. However, the amount of the increased drawdown in many cases is relatively small given the uncertainty of the model results, the geographic scale of the averaging (county-wide), and the time period considered (2008 to 2060).

Please recall that the desired future condition was based on a specific spatial distribution of pumping. Several of the simulations completed for this analysis included maintaining the same amount of pumping as the modeled available groundwater by adding the proposed Electro Purification and reducing other pumping. Specifically these simulations include Scenarios 11 to 20 and 32. Table D-4 (Austin County) and Table D-5 (Fort Bend County) results suggest that this redistribution of pumping will still result in a small amount of additional drawdown on a county-model layer scale. However, Table D-6 (Waller County) results suggest that the redistribution will result in lower drawdowns for Waller County in the Chicot and Evangeline aquifers, apparently due to the recovery associated with reduced pumping in the Katy area. This recovery is greater than the drawdown associated with the Electro Purification pumping, and the net result is an overall average of less drawdown.

As described earlier, the model estimates of drawdown have a degree of uncertainty that makes specific findings or recommendations difficult. The GAM has gained acceptance as a tool to use for the development of desired future conditions and the development of modeled available groundwater estimates. The HAGM has gained acceptance as a tool for the regulatory programs of the subsidence districts, and is being considered for use in the next round of joint groundwater planning.

For purposes of this evaluation, the drawdown estimates are not particularly helpful in distinguishing between scenarios except in a general sense (increased pumping results in increased drawdown). Also, the analysis has demonstrated that the spatial distribution of pumping associated with a particular simulation is important, and provides some degree of understanding of the sensitivity of the resulting average drawdown estimates on a county-model layer scale.

Except for the scenarios that involved Jasper pumping (Scenarios 21 to 30), the drawdowns attributed to proposed Electro Purification pumping appears to be relatively minor on a county-model layer scale (generally within 20 feet) given the uncertainty of the models and the geographic and time scales.

The accuracy of the models, the imprecision of the estimates due to potential variations in spatial distribution of pumping, and the iterative nature of the joint planning process (updates every five years) suggests that slight differences in average drawdowns over a county-model layer scale are not necessarily significant with regard to assessing impacts to desired future conditions. In general, given the limitations of the models, most of the scenarios (especially those that incorporate the proposed Electro Purification pumping into the modeled available groundwater) are basically consistent with the desired future conditions.

If Electro Purification is issued a permit to pump groundwater, the locations and amounts would have to be incorporated into the joint groundwater planning process. There is a current and ongoing discussion as to which model to use as part of that process (GAM or HAGM). This analysis provides some insight as to what the model results would be under a wide range of conditions (i.e. different amounts of Electro Purification pumping) using either model. The results also provide insight as to what adjustments would need to be made to the desired future conditions, if the desired future conditions is expressed in a manner similar to the ones adopted in 2010.

6.0 Potential Effects of Proposed Pumping on Subsidence

When groundwater is pumped from an aquifer, stored water in confined aquifers enters the well due to expansion of water, the compression of the aquifer material, and the compression of clayey beds that are within and adjacent to the aquifer. The resulting compression is considered elastic (i.e. reversible) if there is no permanent rearrangement of the skeletal structure of the sediments. Conversely, the resulting compression is considered inelastic (irreversible) if the reduction in pressure caused by the removal of the water causes rearrangement of the skeletal structure of the sediments. Compaction of these sediments results in a loss of storage capacity of the aquifer, and also can result in land subsidence.

Unlike the previously described evaluations of drawdown on a well-by-well basis or in terms of impacts to the desired future condition, the analysis of subsidence has yielded results which are useful in distinguishing various scenarios. Please recall that the review of the GAM and HAGM presented in Appendix A yielded the conclusion that drawdown estimates contain considerable uncertainty, but that long-term subsidence estimates contain less uncertainty.

Data are also available, independent of model simulations, which are useful in the assessment of potential subsidence associated with the proposed project. These data include historic subsidence measurements, data and maps of clay thickness, and estimates of historic groundwater pumping.

6.1 Historic Subsidence in the Region

Figure 8 presents a map of actual subsidence measurements at 474 points used by the USGS to calibrate the GAM and HAGM. Note that subsidence greater than three feet has occurred in Harris, Fort Bend, and Galveston County, and has exceeded 9 feet in some areas. As described above and in Appendix A, subsidence is a function of clay thickness and pumping. Areas with high pumping and thin clays will not experience as much subsidence as areas with high pumping and thick clays. Also, areas with low pumping and thick clays will have less subsidence than areas with high pumping and thick clays.

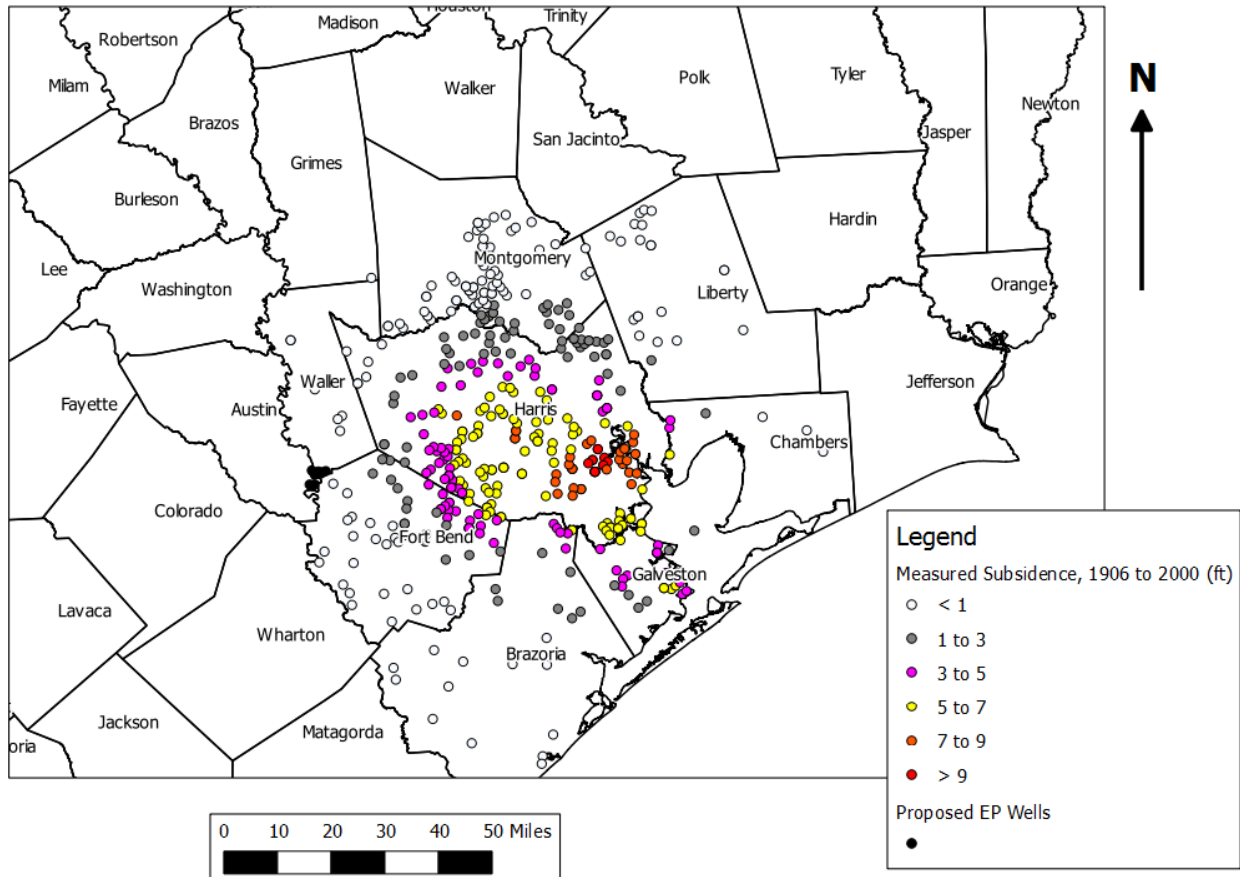


Figure 8. Map of Subsidence Measurement Locations

6.2 Clay Thickness

In order to evaluate the *potential* for subsidence in the Electro Purification project area (an area that has not experienced high levels of pumping in the past), comparisons of clay thickness in the area of interest with clay thickness in areas that have experienced high groundwater pumping was completed as part of this review.

The USGS provided mapped clay thickness data on a model cell basis that were used in the development of the GAM and HAGM (email from Mark Kasmarek of November 13, 2013). These clay thickness data were used as parameters in the initial assignment of elastic and inelastic storativity values in the GAM and HAGM. Maps of these data were presented in the GAM Report (Kasmarek and Robinson, 2004), and are not repeated here.

The clay thickness data and the actual subsidence data presented previously in Figure 8 were used in an analysis of comparing clay thickness in the areas that have experienced subsidence with clay thickness in the proposed Electro Purification project area. This comparison is presented in Figure 9. The plot includes the average clay thickness at points where subsidence measurements were reported. Thus, the two bars labeled “Sub >9” are the average clay thickness for the Chicot Aquifer

and Evangeline Aquifer for all points where measured subsidence is greater than nine feet. The other groups of bars represent areas where measured subsidence is between seven and nine feet (Sub = 7 to 9), measured subsidence is between five and seven feet (Sub = 5 to 7), measured subsidence is between three and five feet (Sub = 3 to 5), measured subsidence is between one and three feet (Sub = 1 to 3), and measured subsidence is less than one foot (Sub < 1). The two bars on the right-hand side of the plot represents the average clay thickness in a 40 square mile area that surrounds the proposed Electro Purification wells.

From this plot it can be seen that the areas with the highest measured subsidence are in areas with the thickest clay. Given the thickness of the clay in the proposed Electro Purification project area, it would appear that subsidence greater than seven feet is unlikely. The next step in this analysis considers historic pumping in these areas, and comparing that pumping to the proposed pumping by Electro Purification.

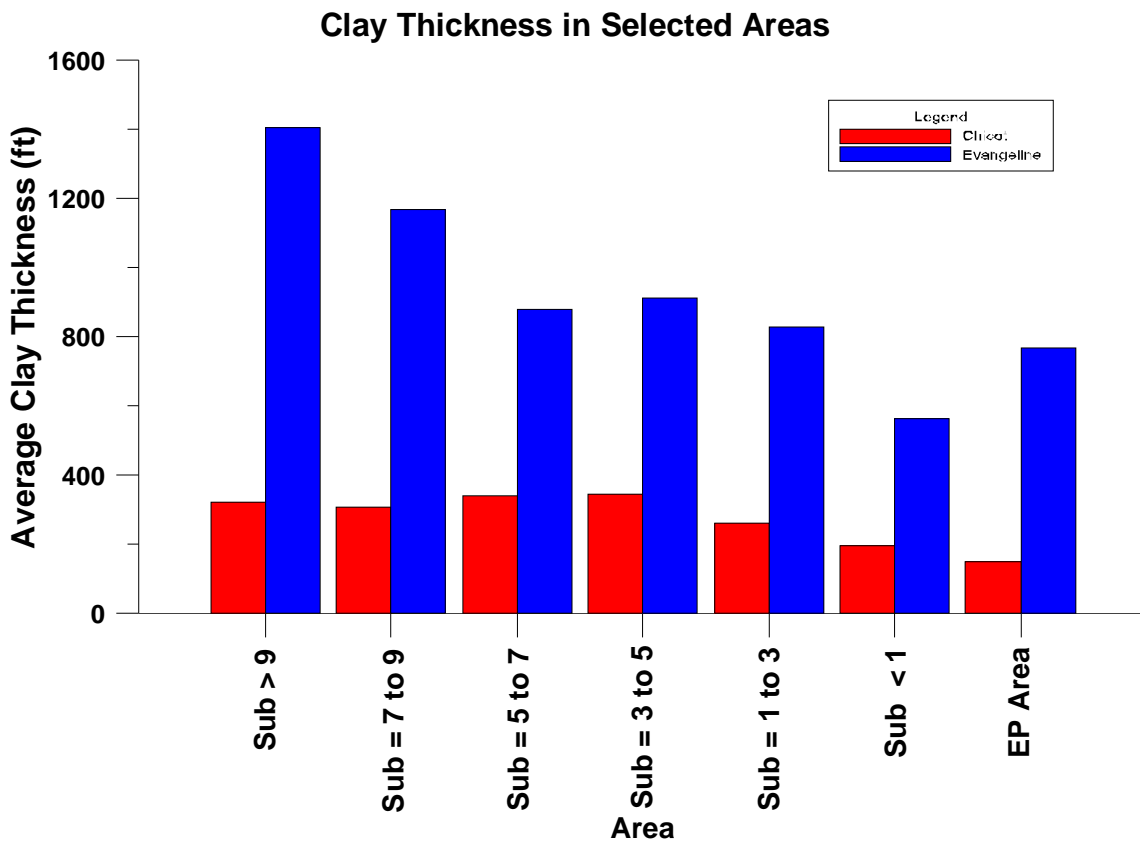


Figure 9. Average Clay Thickness in Areas with Historic Subsidence

6.2 Historic Pumping in Areas with Historic Subsidence

Subsidence is a function of clay thickness and pumping. The previous section included a comparative analysis of clay thickness in areas where subsidence has been measured and the proposed area of the Electro Purification wells. The proposed Electro Purification project contemplates pumping 20 million gallons per day in a relatively small area. Up to six million gallons

of groundwater per day would be pumped within a one square mile area under the Electro Purification proposal.

This portion of the analysis presents estimates of historic pumping at the points where subsidence has been measured to evaluate the intensity of the pumping relative to the measured subsidence. For this analysis, the historic pumping estimates from the GAM and HAGM were used. Points with measured subsidence were identified with model row and column coordinates since these were used in model calibration by the USGS. Historic pumping from that same row and column were extracted from the model files. For this analysis, HAGM estimates of pumping from 1890 to 2009 were used. The pumping estimates were then categorized into pumping rates (in million gallons per day, or mgd) as follows:

- Pumping in a cell less than 0.1 million gallons per day, or mgd
- Pumping in a cell between 0.1 and 0.5 mgd
- Pumping in a cell between 0.5 and 1 mgd
- Pumping in a cell between 1 and 2 mgd
- Pumping in a cell between 2 and 4 mgd
- Pumping in a cell between 4 and 6 mgd
- Pumping in a cell between 6 and 8 mgd

Pumping amounts were extracted for each stress period and categorized as shown above. The results were then converted into frequency of occurrence (i.e. percentage of the wells in a particular subsidence area pumped between 1 and 2 mgd). The results are presented in Figures 10 to 16 as follows:

- Figure 10 presents the analysis for areas with measured subsidence less than one foot
- Figure 11 presents the analysis for areas with measured subsidence between 1 and 3 feet
- Figure 12 presents the analysis for areas with measured subsidence between 3 and 5 feet
- Figure 13 presents the analysis for areas with measured subsidence between 5 and 7 feet
- Figure 14 presents the analysis for areas with measured subsidence between 7 and 9 feet
- Figure 15 presents the analysis for areas with measured subsidence greater than 9 feet
- Figure 16 presents the analysis for the Electro Purification project area

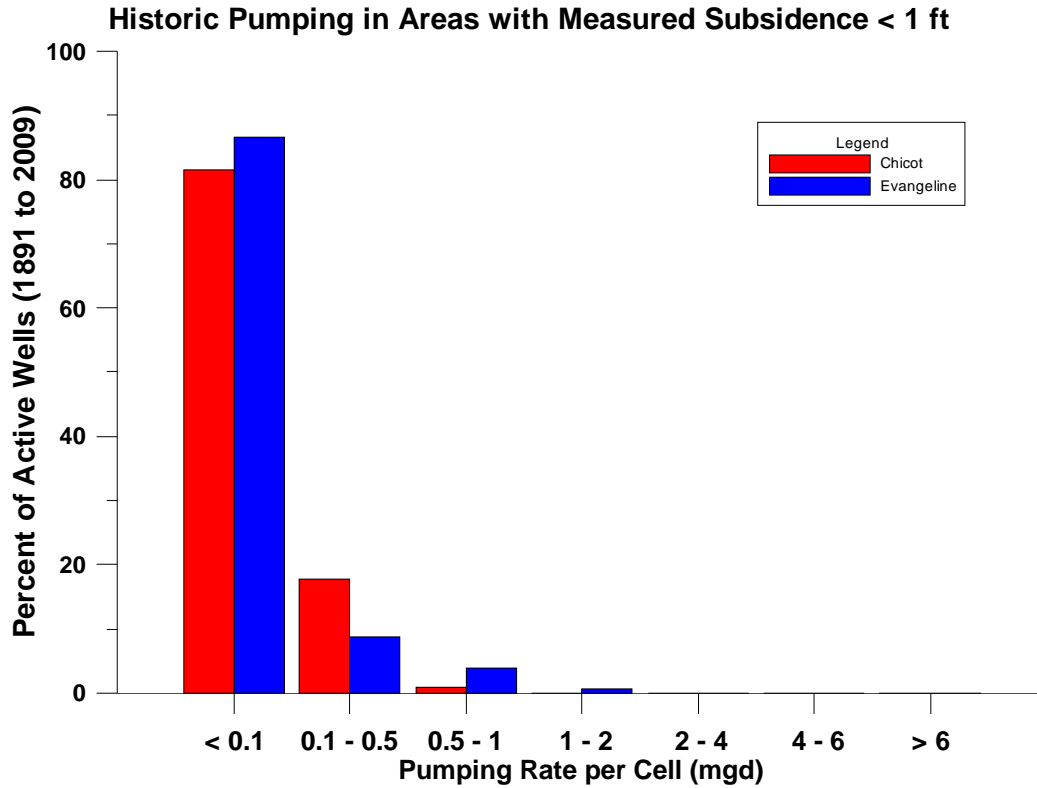


Figure 10. Historic Pumping in Areas with Measured Subsidence Less than one foot

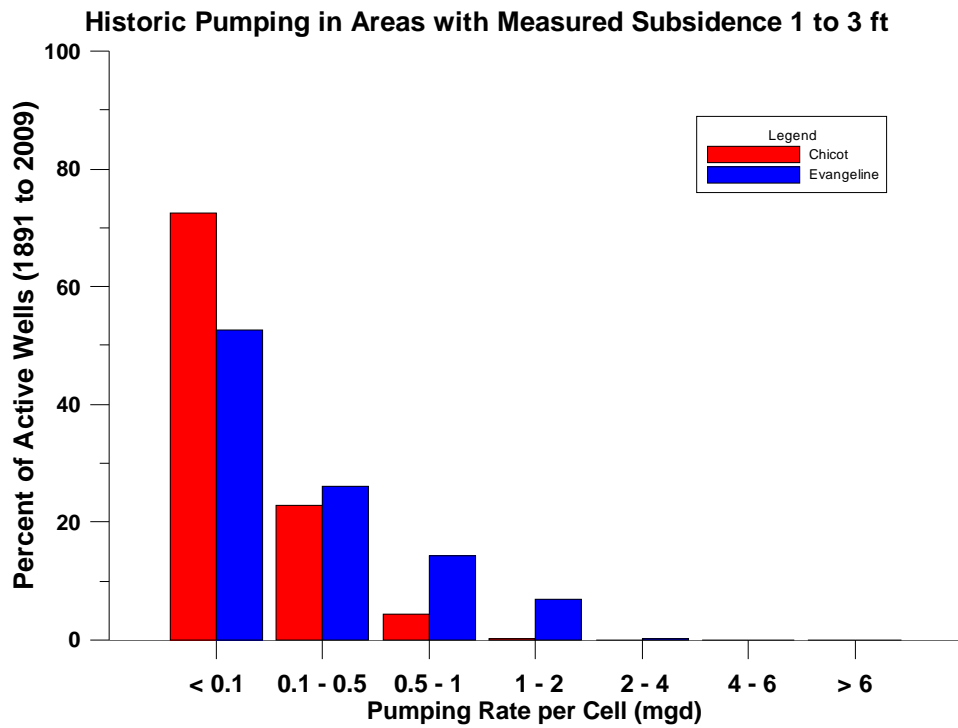


Figure 11. Historic Pumping in Areas with Measured Subsidence between one and three feet

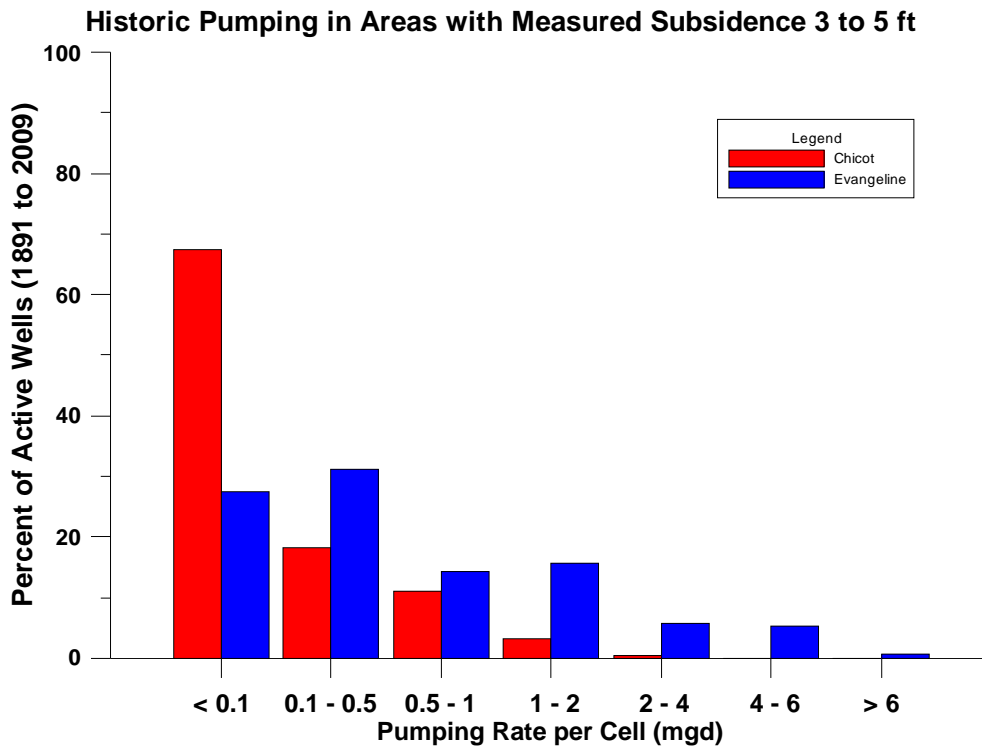


Figure 12. Historic Pumping in Areas with Measured Subsidence between three and five feet

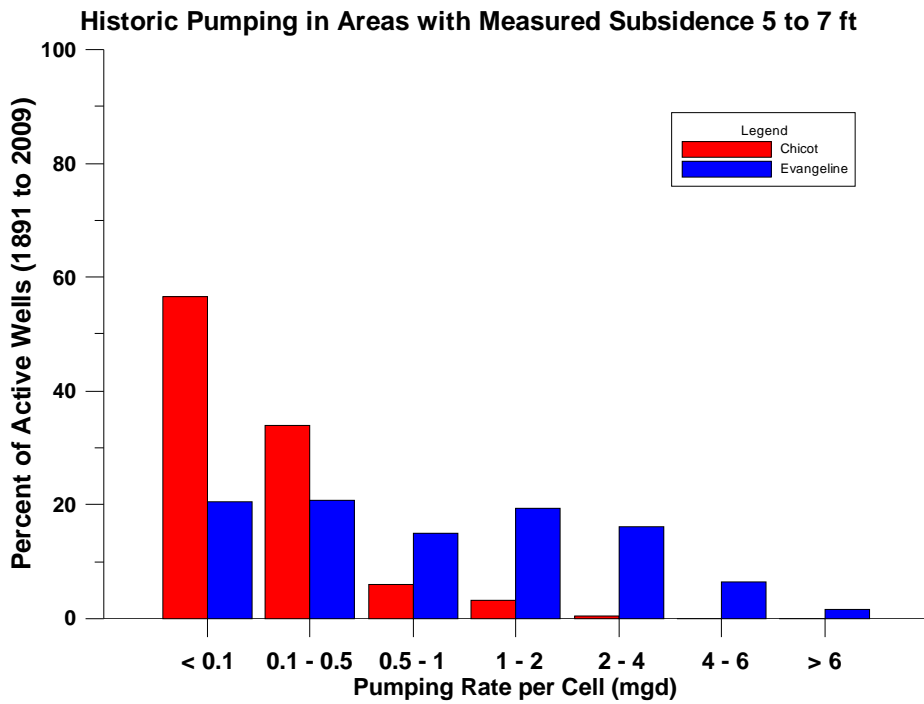


Figure 13. Historic Pumping in Areas with Measured Subsidence between five and seven feet

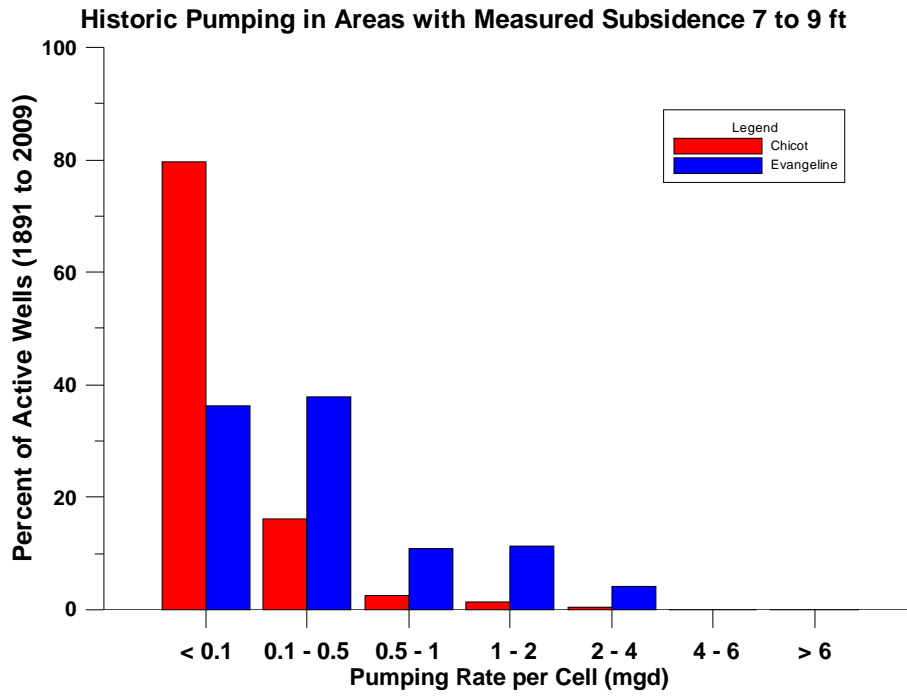


Figure 14. Historic Pumping in Areas with Measured Subsidence between seven and nine feet

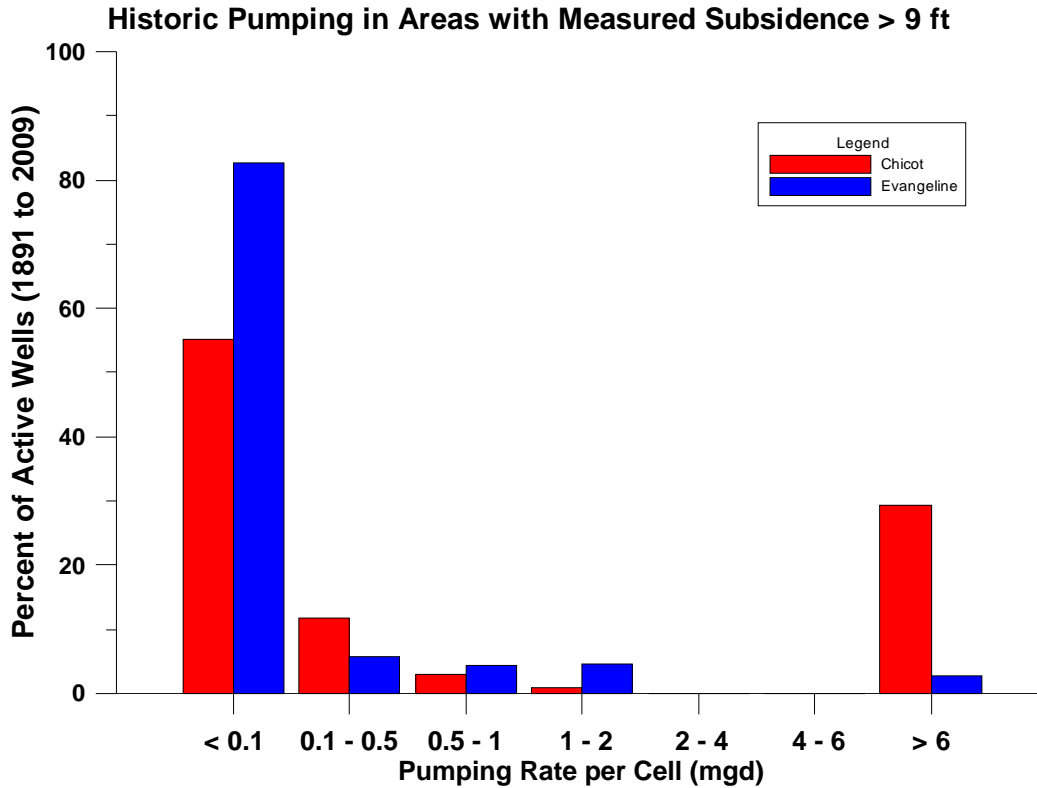


Figure 15. Historic Pumping in Areas with Measured Subsidence greater than nine feet

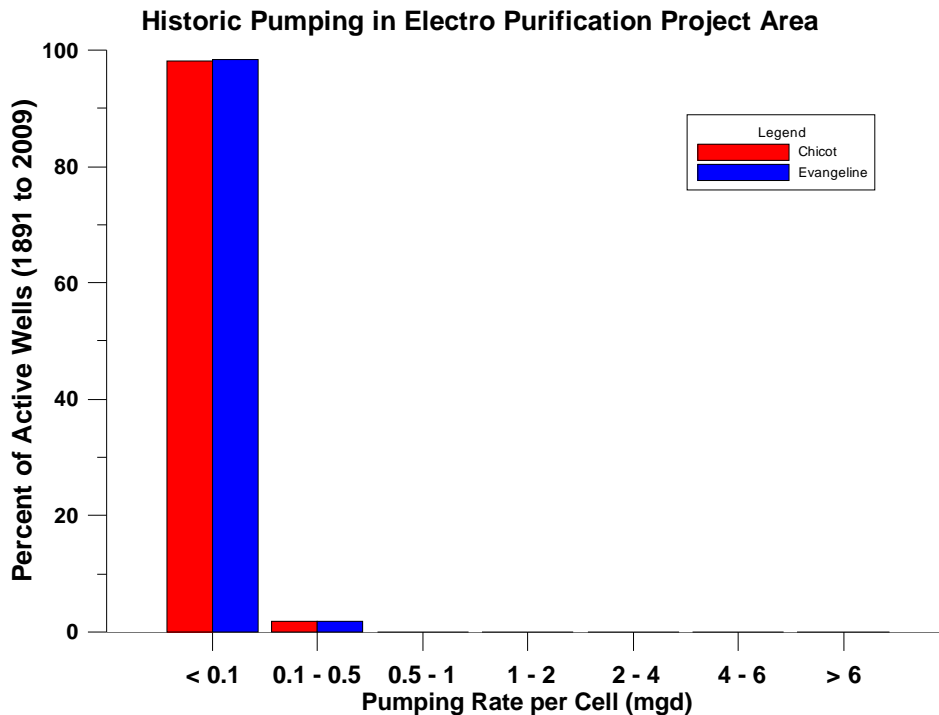


Figure 16. Historic Pumping in the Electro Purification Project Area

From these plots, the following can be concluded:

- Historic pumping in the proposed Electro Purification project area is essentially all less than 0.1 million gallons per day
- About 30 percent of the historic pumping from the Chicot Aquifer in areas where measured subsidence has exceeded nine feet has been from cells that pump more than six million gallons per day.
- Historic pumping from the Evangeline Aquifer in areas where measured subsidence is between three and seven feet from cells that pump more than 500,000 gallons per day is fairly common (generally greater than 30 percent of all Evangeline aquifer pumping). However, there are few cells that have historically pumped six million gallons per day, although they do exist.

Overall, this analysis and the clay thickness analysis suggests that potential subsidence associated with the proposed Electro Purification project at 20 million gallons per day over 7 feet is unlikely due to clay thickness differences between the Electro Purification site and the areas where this much subsidence has been measured, and due to the fact that most of the historic pumping in these high subsidence areas is from the Chicot Aquifer. Subsidence between three and seven feet, however, is possible given that the clay thickness in the Electro Purification area is somewhat similar to those areas that have subsidence measured between three and seven feet, and because the proposed pumping intensity (up to six million gallons per day in a one-square mile area) is at the upper end of historic pumping in areas that have subsidence measured between three and seven feet.

6.3 Subsidence Results from GAM and HAGM Simulations

Among the outputs from the simulations completed with the GAM and HAGM are estimates of subsidence. As noted in Appendix A, the calibration of the GAM and HAGM included comparing measured subsidence with model-estimated subsidence. Figure 17 presents a comparison of the measured subsidence measurements with estimates from the GAM and HAGM. Details of the data and the comparison is discussed in Section A-9.1 of Appendix A.

From this comparison, it can be seen that long-term subsidence measurements are accurate to about a foot, and that the HAGM appears to have fewer outliers than the GAM. Thus, model estimated subsidence of one foot could mean that there is no subsidence or that the subsidence is actually about two feet. In evaluating the results of the simulations completed in this analysis, this one foot threshold was used to distinguish between model “noise” and “measureable” subsidence.

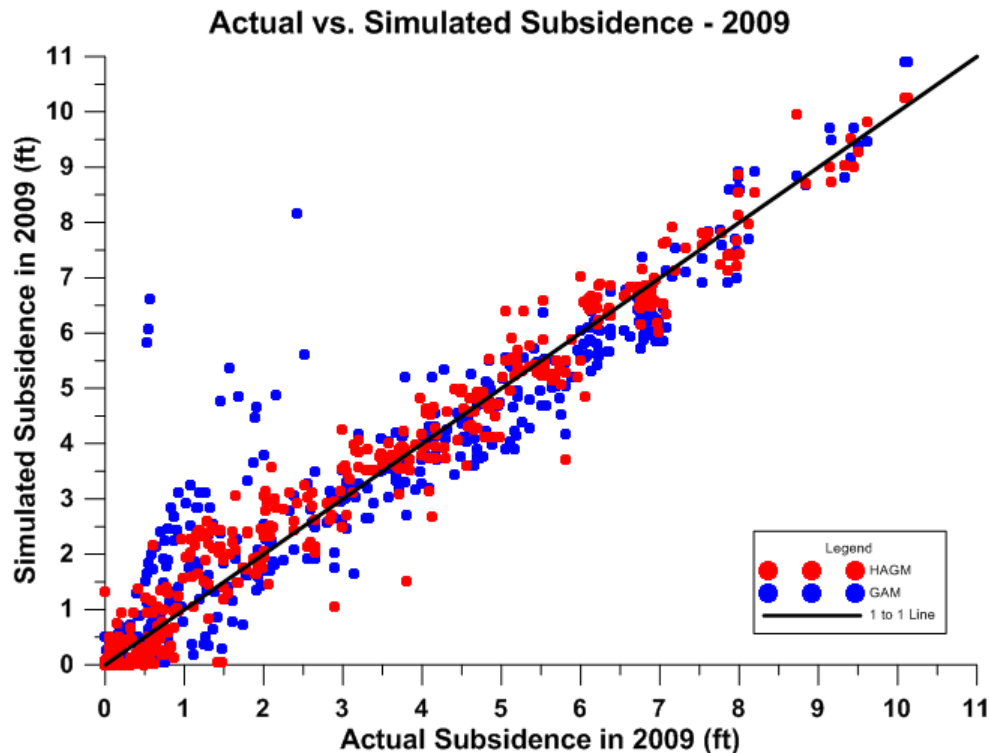


Figure 17. Comparison of Actual Subsidence from 1906 to 2000 and Estimated Subsidence from 1891 to 2009 from the GAM and HAGM

Appendix E contains summary tables, graphs, and maps of the subsidence estimates from all the simulations using the GAM and HAGM. Similar to the drawdown tables and graphs in Appendix D, the results are organized by county and include estimates of subsidence associated with the particular simulation and estimates of subsidence associated with the proposed Electro Purification

project on a simulation-by-simulation basis. Also included are tables of well site by well site subsidence estimates similar drawdown tables presented in Appendix C.

6.3.1 Subsidence Estimates for Each Scenario

Tables E-1 to E-3 present the estimated subsidence for each of the simulations (33 with GAM and 33 with HAGM), including the baseline scenario (DFC/MAG simulation), at the end of the simulation period (2060) for Austin County (Table E-1), Fort Bend County (Table E-2), and Waller County (Table E-3). Average subsidence across the county and maximum subsidence in the county are presented for each model. Table E-4 is the same format as Tables E-1 to E-3, but show the results from a 40 square mile area designated as the “project area” in Austin, Fort Bend and Waller counties. Estimated values greater than one foot are presented in red to designate these as measureable values based on the comparison shown in Figure 17 presented above.

Tables E-5 to E-8 present the simulated subsidence for each simulation that is attributable to the Electro Purification project for each scenario. These estimates were developed by subtracting the subsidence from the baseline scenario from the area of interest. These calculations were made on both the average and maximum subsidence. For example, if the maximum subsidence for the baseline scenario was 1 foot, and the maximum subsidence for the scenario of interest was 3 feet, then the subsidence attributed to the Electro Purification project is 2 feet. Table E-5 presents the results for Austin County, Table E-6 presents the results for Fort Bend County, Table E-7 presents the results for Waller County, and Table E-8 presents the results for the 40-square mile project area. Estimated values greater than one foot are presented in red to designate these as measureable values based on the comparison shown in Figure 17 presented above.

6.3.2 Subsidence Estimates for Individual Well Sites

Tables E-9 to E-12 present simulated subsidence for the same set of well sites previously presented in Section 4.2 (379 Chicot Aquifer wells and 115 Evangeline Aquifer wells). There are two tables for the wells sites where wells are completed in the Chicot Aquifer to present the results of the GAM and HAGM, and two tables for the well sites where the wells are completed in the Evangeline Aquifer to present the results of the GAM and the HAGM.

Estimates of subsidence at these sites are presented for the baseline scenario (DFC/MAG simulation), Scenario 3 (proposed Electro Purification pumping = 6 million gallons per day), Scenario 10 (proposed Electro Purification pumping = 20 million gallons per day), and Scenario 31 (proposed Electro Purification pumping according to the conversion schedule up to 9.9 million gallons per day) are presented in terms of estimated subsidence for the scenario and in terms of subsidence attributable to Electro Purification pumping.

Subsidence estimates are the sum of individual model layer clay compaction estimates. The resulting subsidence estimates. The tables are organized by model layer based on well depth and completion for convenience and consistency with the drawdown tables in Appendix C. The fact that a well is completed in the Chicot Aquifer (layer 1) or Evangeline Aquifer (layer 2) has no bearing on the subsidence estimate, the well site was used as a location for the estimate.

Table 15 summarizes the results of Tables E-9 and E-10 for sites where wells are completed in model layer 1 (Chicot Aquifer). Note that ranges of subsidence are presented for three distance groups. The closest site where a well is completed in the Chicot Aquifer in this analysis is 0.15 miles from a proposed Electro Purification well.

Table 15. Summary of Subsidence Estimates (1891 to 2060) at Well Sites (Wells Completed in the Chicot Aquifer) – Estimates from Tables E-9 and E-10

Distance to EP Wells	Scenario	Simulated Subsidence (ft)		Subsidence Attributable to EP (ft)	
		GAM	HAGM	GAM	HAGM
0.15 to 0.5 mile	Base	0.02 to 0.24	0.40 to 1.15	0	0
	Scenario 3 (6 mgd)	0.31 to 1.16	1.07 to 2.08	0.28 to 1.14	0.58 to 1.34
	Scenario 10 (20 mgd)	2.28 to 3.31	3.20 to 4.21	2.14 to 3.28	2.15 to 3.47
	Scenario 31 (9.9 mgd)	0.59 to 1.91	1.42 to 2.92	0.57 to 1.88	0.93 to 2.17
0.5 to 1 mile	Base	0.02	0.35 to 0.74	0	0
	Scenario 3 (6 mgd)	0.22 to 1.16	0.88 to 2.08	0.19 to 1.14	0.53 to 1.34
	Scenario 10 (20 mgd)	2.18 to 3.31	2.95 to 4.21	2.16 to 3.28	2.60 to 3.47
	Scenario 31 (9.9 mgd)	0.47 to 1.91	1.20 to 2.92	0.45 to 1.88	0.85 to 2.17
1 to 2 miles	Base	0.02 to 0.38	0.39 to 1.31	0	0
	Scenario 3 (6 mgd)	0.18 to 0.83	0.93 to 1.83	0.16 to 0.63	0.32 to 0.86
	Scenario 10 (20 mgd)	1.23 to 2.56	1.93 to 3.30	1.22 to 2.54	1.35 to 2.84
	Scenario 31 (9.9 mgd)	0.36 to 1.14	1.21 to 2.14	0.33 to 1.06	0.50 to 1.39

Table 16 summarizes the results of Tables E-11 and E-12 for sites where wells are completed in model layer 2 (Evangeline Aquifer). Note that ranges of subsidence are presented for three distance groups. The closest site where a well is completed in the Evangeline Aquifer used in this analysis is 1.7 miles from a proposed Electro Purification well.

Table 16. Summary of Subsidence Estimates (1891 to 2060) at Well Sites (Wells Completed in the Evangeline Aquifer) - Estimates from Tables E-11 and E-12

Distance to EP Wells	Scenario	Simulated Subsidence (ft)		Subsidence Attributable to EP (ft)	
		GAM	HAGM	GAM	HAGM
1.7 to 3 miles	Base	0.02 to 0.21	0.39 to 1.14	0	0
	Scenario 3 (6 mgd)	0.30 to 0.64	0.93 to 1.69	0.28 to 0.43	0.45 to 0.55
	Scenario 10 (20 mgd)	1.03 to 1.89	1.82 to 2.84	1.01 to 1.68	1.29 to 1.70
	Scenario 31 (9.9 mgd)	0.51 to 0.98	1.24 to 2.02	0.50 to 0.77	0.72 to 0.88
3 to 5 miles	Base	0.01 to 1.00	0.11 to 1.97	0	0
	Scenario 3 (6 mgd)	0.02 to 1.27	0.36 to 2.23	0 to 0.31	0.15 to 0.31
	Scenario 10 (20 mgd)	0.41 to 1.75	0.94 to 2.72	0.40 to 0.88	0.62 to 0.87
	Scenario 31 (9.9 mgd)	0.10 to 1.41	0.53 to 2.38	0.08 to 0.49	0.23 to 0.48
5 to 7 miles	Base	0.01 to 4.22	0.01 to 1.85	0	0
	Scenario 3 (6 mgd)	0.01 to 4.67	0.01 to 1.96	0 to 0.45	0 to 0.22
	Scenario 10 (20 mgd)	0.01 to 5.52	0.08 to 2.18	0 to 1.30	0.07 to 0.64
	Scenario 31 (9.9 mgd)	0.01 to 4.87	0.01 to 2.02	0 to 0.65	0 to 0.34

6.3.3 Hydrographs of Estimated Subsidence

Figures E-1 to E-64 present time-series graphs of subsidence for Austin County, Fort Bend County, Waller County, and the 40-square mile project area for each simulation and each model (GAM and HAGM). A cover sheet in front of the figures describes each figure and its page number. The tables of subsidence results are useful to quickly compare the end result of the simulations. These graphs are useful to put the estimated subsidence into perspective with regard to the baseline scenario and with time.

6.3.4 Maps of Subsidence at Individual Well Sites

Figures E-65 to E-78 present maps of subsidence at specific well locations, and present the well sites from Tables E-9 to E-12 (Bluebonnet Groundwater Conservation District registered and permitted wells and wells in the Texas Water Development Board database). The well sites are color coded to show the estimated subsidence.

The baseline scenario (DFC/MAG simulation), Scenario 3 (proposed Electro Purification pumping = 6 million gallons per day), Scenario 10 (proposed Electro Purification pumping = 20 million gallons per day), and Scenario 31 (proposed Electro Purification pumping according to the conversion schedule up to 9.9 million gallons per day) are presented in terms of estimated subsidence for the scenario and in terms of subsidence attributable to Electro Purification pumping.

6.4 Discussion of Subsidence Results

This evaluation has focused on evaluating measured subsidence data in the region, evaluating historic pumping in areas with measured subsidence, and estimating subsidence with the GAM and HAGM under a wide range of possible scenarios. Based on this analysis, the following can be concluded:

- Historic subsidence in the region has occurred in areas with high pumping and thick clay sequences. Subsidence has been measured in excess of nine feet in some areas of Harris County. Clay thickness in the proposed Electro Purification project area is less than the clay thickness in those portions of Harris County. Based on an analysis of mapped clay thickness at the proposed Electro Purification site and an evaluation of historic pumping in areas with measured subsidence in the region, subsidence impacts associated with the proposed project could be as high as three to seven foot range over several decades, depending on the amount of pumping.
- The proposed Electro Purification pumping at the full amount (20 million gallons per day for the project and as much as six million gallons per day in a one-square mile area) represents an intense amount of pumping over a fairly small area. Analysis of historic pumping estimates suggest that this amount of pumping in a small area, while not unprecedented for the area, is certainly not common. Thus, the use of historic analogs and models that are based on historic data cannot be considered highly accurate.
- The models that are available for use in this analysis (GAM and HAGM) were used to simulate a wide range of potential pumping scenarios to better understand the potential for subsidence in the area of the proposed pumping. Based on the calibration of the model, it

appears that measureable subsidence will occur by 2060 if pumping exceeds about 6 million gallons per day. Based on the model simulations, this subsidence may not actually be measureable for 10 to 20 years (Figures E-39 and E-40).

- The models results suggest that spreading the pumping over a wide area will mitigate the subsidence impacts as compared to concentrating the pumping over a small area.

7.0 Results of Simple Local-Scale MODFLOW Model Simulations

Simulations with the simple local-scale MODFLOW model that was described previously in Section 3.6 of this report were completed in an attempt to highlight and address limitations of the GAM and HAGM with respect to the proposed project. Specifically, applicant's hydrogeology consultant has stated that a confining unit may exist between the Upper Evangeline Aquifer and the Lower Evangeline Aquifer in the vicinity of the proposed wells. Because of the regional nature of the GAM and HAGM, it is not possible to simulate the effect of this postulated subdivision of the Evangeline Aquifer. Moreover, clay content data has been developed on a regional basis, and demonstrates a high degree of variation. Specific knowledge of clay content in the area of the proposed wells would improve the drawdown and subsidence estimates of the proposed project.

As developed more fully below, if this project proceeds to a testing and drilling phase, it is recommended that the subsequent evaluation of the test data include expanding this type of numerical analysis. Specifically, hydrogeologic framework data collected during the drilling should be used to construct a numerical model that conforms better to local hydrogeologic conditions, and data from any aquifer test be evaluated with local numerical model to assess and update estimated impacts of the proposed pumping.

The simulations included a set that varied the clay content in the aquifer units (layers 1, 2 and 4), and a set that varied the clay content of the postulated confining unit (layer 3). The parameters used for these simulations and the variation was previously presented in Section 3.6.3 and 3.6.4 of this report.

7.1 Variation of Aquifer Layer Clay Content

Based on a review of clay content data used in the GAM and HAGM, clay content in the area of the proposed Electro Purification wells ranges between about 32 percent to about 50 percent in the Chicot Aquifer, and between about 50 percent and 68 percent in the Evangeline Aquifer. For purposes of this preliminary level analysis, and in order to demonstrate the importance of obtaining accurate data, clay content for these aquifer units (layers 1, 2 and 4) were varied between 25 and 75 percent, in 5 percent increments. Layer 3 clay content was assumed to be 85 percent for these simulations.

Figure 18 summarizes the results. Please note plot shows the relationship between changes in clay content of layers 1, 2, and 4 (x-axis), the change in maximum drawdown after 50 years (y-axis on the left side of the graph), and the change in maximum subsidence after 50 years (y-axis on the right side of the graph). Estimated drawdown is shown for layer 1 (blue line), layer 2 (pink line), and layer 4 (green line). Estimated subsidence is shown as a red line.

**Drawdown and Subsidence
Variation in Clay Percentage in Layers 1, 2 and 4
Layer 3 Clay Percentage = 85**

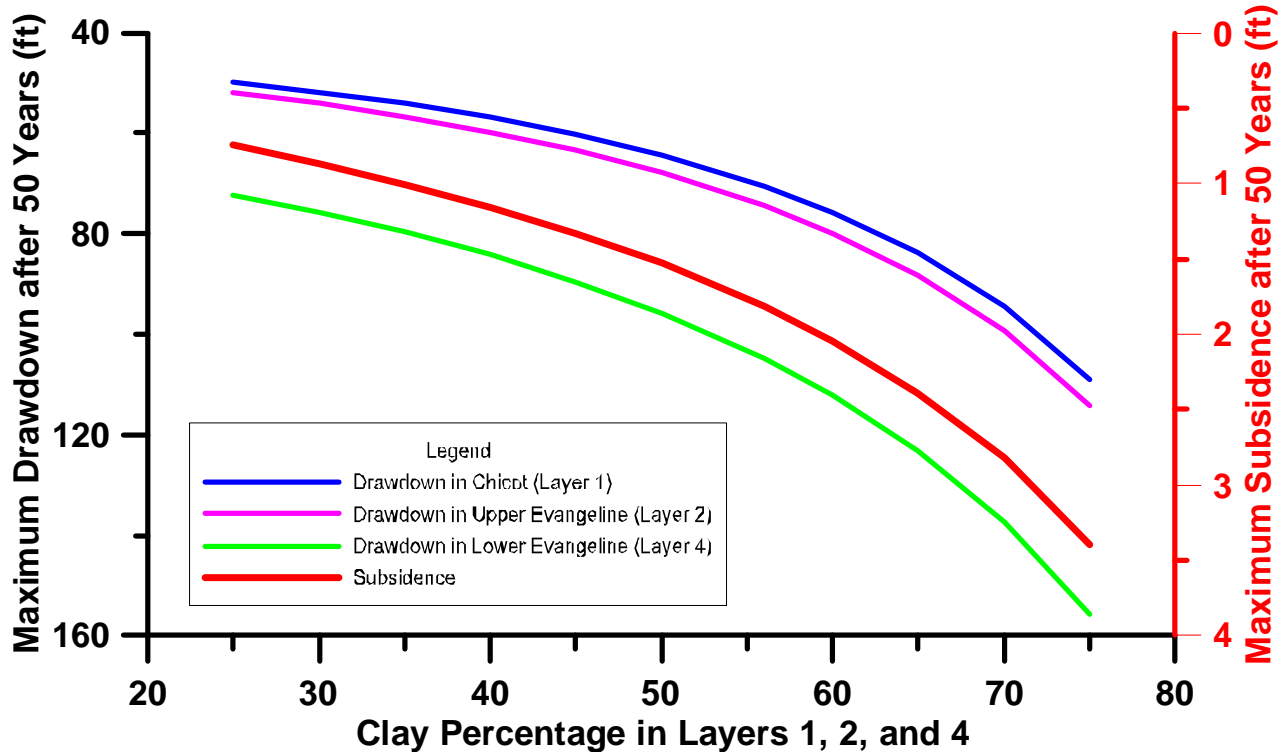


Figure 18. Drawdown and Subsidence Estimates - Aquifer Unit Clay Content Variation

Please note that as clay content in the aquifer layers increase, both drawdown and subsidence increase. Please recall that as clay content increases, equivalent layer hydraulic conductivity decreases. Lower equivalent hydraulic conductivity results in increased drawdown. In turn, increased drawdown results in increased subsidence. As drawdown in layer 4 increases, the vertical gradient across the confining unit (layer 3) increases, and results in drawdown in layers 1 and 2.

This plot cannot be used to accurately estimate drawdown or subsidence of the proposed project due to the simple nature of the model and the approach. Rather, it is offered to demonstrate the importance of accurately collecting clay content data in the area of the proposed Electro Purification wells.

7.2 Variation in Postulated Confining Layer Clay Content

The simulations discussed in Section 7.1 focused on varying the clay content of the aquifer units (layers 1, 2, and 4). The second set of simulations only varied the clay content of the postulated confining unit. For purposes of this preliminary level analysis, and in order to demonstrate the importance of obtaining accurate data, clay content for the postulated confining unit (layer 3) was varied between 50 and 90 percent. In the aquifer units (layers 1, 2 and 4) clay content was held

constant at 40 percent for layer 1 and 60 percent in layers 2 and 4 to approximate the amounts of clay used in the GAM and HAGM for the proposed project area for these simulations.

Figure 19 summarizes the results. Please note plot shows the relationship between changes in clay content of layers 1, 2, and 4 (x-axis), the change in maximum drawdown after 50 years (y-axis on the left side of the graph), and the change in maximum subsidence after 50 years (y-axis on the right side of the graph). Estimated drawdown is shown for layer 1 (blue line), layer 2 (pink line), and layer 4 (green line). Estimated subsidence is shown as a red line.

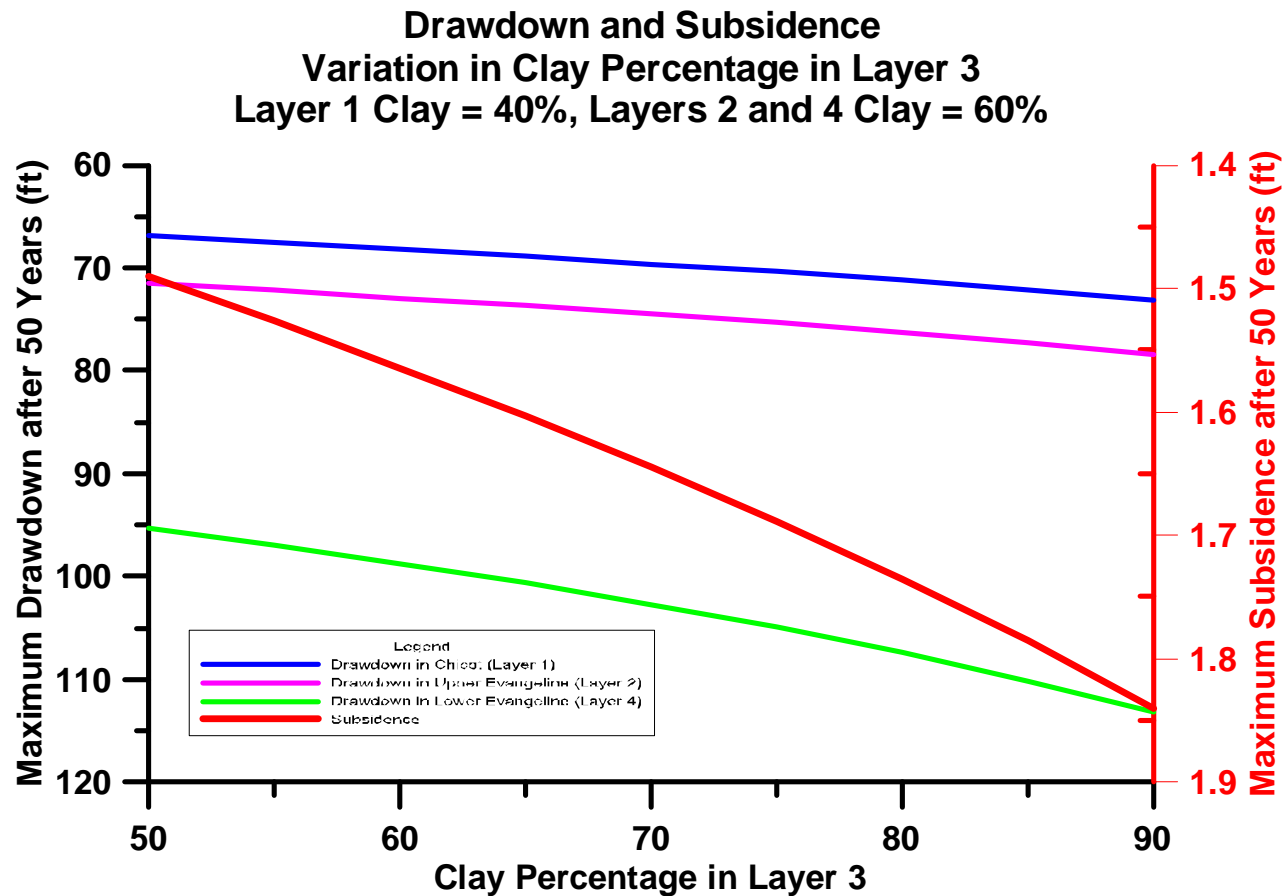


Figure 19. Drawdown and Subsidence Estimates - Confining Unit Clay Content Variation

Please note that as clay content in the confining unit (layer 3) increases, the degree of isolation between the upper and lower Evangeline aquifers increases. Where the clay percentage is about 50 or 60 percent, the “confining unit” has about the same hydraulic conductivity as the aquifer units. This simulates the condition that the confining unit is not truly present. As the degree of isolation increases (i.e. clay content in layer 3 increases), the drawdown in layer 4 increases more rapidly than the drawdown in layers 1 and 2. This is the result of low vertical hydraulic conductivity through the confining unit and the isolation of the production unit (layer 4). Less water can move vertically downward as the isolation increases. Please note that subsidence increases slightly as the clay

content in layer 3 increases, but the change in subsidence is less dramatic than in the previous set of simulations where clay content in the aquifer units was varied

This plot cannot be used to accurately estimate drawdown or subsidence of the proposed project due to the simple nature of the model and the approach. Rather, it is offered to demonstrate the importance of accurately collecting clay content data in the area of the proposed Electro Purification wells.

7.3 Discussion of Results

These simulations with the simple local-scale MODFLOW model are not to be construed as accurate or quantitative. They are only instructive to understand the relationship between parameters and the results (drawdown and subsidence in this case), and the importance of local subsurface data collection and analyses of tests in the project area to obtain accurate parameters from any future testing in the area, if a permit is issued.

To a certain extent, the existing regional models in the area are useful to evaluate long-term subsidence. However, the identified issues with the drawdown estimates from those models suggest that the model parameters used in those models were adjusted in such a fashion to achieve a match with the measured subsidence in the area without much regard for independent knowledge of individual parameters. Moreover, the method used in the GAM and HAGM to simulate recharge and groundwater-surface water interactions suggests that model parameters in the GAM and HAGM should be used in other applications with caution.

The simulations demonstrated that accurate knowledge of the clay content in the aquifer units is important to the estimates of long term drawdown and subsidence. Further, if the lower Evangeline is isolated from the upper Evangeline and Chicot, drawdown in the overlying units could still be observed

Because subsidence would not be measurable for several years, any reasonable test of even several months would not be useful evaluate subsidence directly. Proper analysis of tests coupled with incorporation of subsurface data collected during drilling at the site would provide a means to improve on the simple local scale MODFLOW model to develop more accurate conclusions.

8.0 Discussion and Recommendations

As developed in this report, the overall conclusions of the technical review in the four topic areas are as follows:

Review the “needs” identified in the permit application in light of the Region H water plan, modeled available groundwater numbers that were developed by TWDB from the GMA 14 joint planning process, and the Ft Bend Subsidence District Groundwater Reduction Plan

- Electro Purification has identified customers for about 10 MGD of the 20 GMD of proposed pumping.
- Based on an analysis of TWDB demand projections, Richmond and Rosenberg would use about 37 percent of the water, and their Groundwater Reduction Program partners would use about 63 percent of the water.
- There is no identified customer for the remaining 10 MGD.

Review the impacts of proposed pumping on existing registered wells and permitted wells in the district

- Drawdown estimates for individual wells from the GAM and HAGM were developed as part of this review, but are unreliable.
- The estimates presented in Appendix C, and discussed in Section 4.2 demonstrate the potential drawdown impacts on individual wells as estimated by the GAM and HAGM. However, these results are considered unreliable, and may likely represent over-estimates of drawdown.
- Local scale testing and developing a local scale model based on those results are recommended to overcome these limitations.

Evaluate the impacts of the proposed pumping in the context of the adopted desired future conditions for Bluebonnet Groundwater Conservation District

- Drawdown estimates on a county scale for each of the aquifer units or model layers using the GAM and the HAGM were developed as part of this review in the context of evaluating the effects of the proposed project on the desired future condition that was adopted in 2010 by the groundwater conservation districts in Groundwater Management Area 14.
- In general, the Electro Purification scenarios that involve increases in pumping cause increases in drawdown that may not be consistent with the desired future condition. However, the amount of the increased drawdown in many cases is relatively small given the uncertainty of the model results, the geographic scale of the averaging (county-wide), and the time period considered (2008 to 2060).
- Except for the scenarios that involved Jasper pumping (Scenarios 21 to 30), the drawdowns attributed to proposed Electro Purification pumping appears to be relatively minor on a county-model layer scale (generally within 20 feet) given the uncertainty of the models and the geographic and time scales.

- If Electro Purification is issued a permit to pump groundwater, the locations and amounts would have to be incorporated into the joint groundwater planning process.
- There is a current and ongoing discussion as to which model to use as part of that process (GAM or HAGM). This analysis provides some insight as to what the model results would be under a wide range of conditions (i.e. different amounts of Electro Purification pumping) using either model.
- The results also provide insight as to what modifications would need to be made to the desired future conditions, if the desired future conditions is expressed in a manner similar to the ones adopted in 2010.

Evaluate the proposed pumping in the context of subsidence

- Historic subsidence in the region has occurred in areas with high pumping and thick clay sequences. Subsidence has been measured in excess of nine feet in some areas of Harris County. Clay thickness in the proposed Electro Purification project area is less than the clay thickness in those portions of Harris County.
- Based on an analysis of mapped clay thickness at the proposed Electro Purification site and an evaluation of historic pumping in areas with measured subsidence in the region, subsidence impacts associated with the proposed project could be as high as three to seven foot range over several decades, depending on the amount of pumping.
- The proposed Electro Purification pumping at the full amount (20 million gallons per day for the project and as much as six million gallons per day in a one-square mile area) represents an intense amount of pumping over a fairly small area. Analysis of historic pumping estimates suggest that this amount of pumping in a small area, while not unprecedented for the area, is certainly not common. Thus, the use of historic analogs and models that are based on historic data cannot be considered highly accurate.
- The models that are available for use in this analysis (GAM and HAGM) were used to simulate a wide range of potential pumping scenarios to better understand the potential for subsidence in the area of the proposed pumping. Based on the calibration of the model, it appears that measureable subsidence will occur by 2060 if pumping exceeds about 6 million gallons per day. Based on the model simulations, this subsidence may not actually be measureable for 10 to 20 years (Figures E-39 and E-40).
- The models results suggest that spreading the pumping over a wide area will mitigate the subsidence impacts as compared to concentrating the pumping over a small area.

8.1 Recommended Drilling and Testing Program

If a permit were to be issued, it is recommended that the following drilling and testing program be incorporated into the permit conditions:

- Drill three deep test holes (to the top of the Burkeville, about 1,500 feet deep). The test holes should be no less than 3,000 feet from each other, and should not be in a line. If space permits, the wells should form the vertices of an equilateral triangle.
- Run geophysical logs in each hole consisting of, at a minimum, spontaneous potential, single point resistivity, short and long normal resistivity (16, 32, and 64), and natural gamma.

- If the sites are suitable for well construction based on the test hole drilling and analysis of the geophysical logs, construct a shallow monitoring well (in the Chicot Aquifer, an intermediate monitoring well (in the upper Evangeline, if its existence is confirmed), and a production well at each site (total of three wells at each site).
- Once the wells are completed and fully developed, run three separate aquifer tests (one in each production well), each lasting 30 days, with 30 days of rest time between tests.
- During the test of each production well, the six monitoring wells and two non-operating production wells will be equipped with pressure transducers to record groundwater levels during the test. Data collection frequency will follow standard aquifer test guidelines.
- The well discharge piping and valves should include a means to accurately measure the discharge rate of the well and maintain a constant flow rate during the test. Actual pumping rate will be approved by Bluebonnet Groundwater Conservation District after review of well development data.
- Analysis of the data with analytical techniques can be completed, but needs to be supplemented with numerical analysis similar to the simple local-scale MODFLOW model discussed in this review. Hydrostratigraphy and model layers will be based on the data collected from the test hole drilling program. Analysis will include calibrating the model to all monitoring well data.

The testing and analyses recommendations are an extension of the BGCD guidelines for a Phase II report. The guideline document focuses on developing hydrogeologic parameters of the aquifer at the location of the test. These guidelines work well for a single well permit. Because the proposed Electro Purification project involves multiple wells and relatively high pumping rates, it is necessary to extend the recommended testing analysis as outlined above. Specifics of the enhancements to the guidelines include:

- The guidelines specifically require aquifer transmissivity, hydraulic conductivity, and storativity. The analyses of these tests should also include clay thickness, sand thickness, geologic interpretation of layering used in the numerical model, horizontal hydraulic conductivity of sand and clay units, equivalent horizontal and vertical hydraulic conductivity of identified layers of the formation, inelastic specific storage, inelastic storativity, and elastic storativity.
- The guidelines are somewhat vague on the analytical method to use. Historically, BGCD has approved Phase II reports using Theis analyses for single well tests. Given the limitations of the Theis method coupled with the scope of the proposed project, numerical analyses of the tests is recommended.
- The guidelines require a 24-hour test, which would be inadequate for evaluation of this project, and 30 day tests have been recommended.
- The guidelines state that existing private wells within ¼ mile may be used as monitoring wells. If any such wells exist and are available for monitoring during the test, they can be added. The recommended testing program includes new monitoring wells that should be adequate to characterize the aquifer in the area.
- The guideline provision for use of a published assumptive storativity value is not applicable to this proposed project.

Guideline requirements for the following report items should be followed and supplemented as appropriate:

- Table of water-level drawdown and recovery data for each test and for each well monitored
- Figures of water-level recovery for each test
- Narrative description of testing methods
- Discussion of conduct of the tests, including details of significant events of the test, any equipment failures and any contingency measures that may have been employed.
- Discussion of conclusions drawn for the analyses of the tests (aquifer parameters and the effects of boundary conditions)
- Maps of the production and monitoring wells giving the location and elevation of the wells and all surrounding wells that exist within a ½ mile radius of the wells. The map shall include streets, roads, and the bounds of the land tracts sufficient to determine the location of the wells within the tract of land on which they are located.

Data from the testing program will be used to update and refine the estimates of impacts of the proposed project. These data and results of the analyses will also be used to establish threshold or trigger groundwater elevations in the production wells and monitoring wells that would result in the reduction or cessation of pumping.

8.2 Recommended Monitoring Program

The recommended monitoring program (assuming that a permit is issued based on the results of the drilling and testing program) is as follows:

- Each production well should be equipped with a totalizing flow meter and a pressure transducer and a data logger.
- Each monitoring well should be equipped with a pressure transducer and data logger.
- Production data for each production well should be recorded and reported monthly.
- Groundwater elevation data for each production well and monitoring well should be collected hourly. These data should be downloaded from the data loggers monthly and reported monthly.
- Groundwater quality samples should be taken from each production well quarterly. Laboratory analyses of the samples should include general mineral (for cation/anion balance), total dissolved solids, and metals. Reports should be submitted annually.
- An extensometer should be installed near the production wells. Daily data should be recorded, and reported annually.

9.0 References

Fitts, C. R., 2002, Groundwater Science. Academic Press, 450 p.

Hasan, M. and Wade, S., 2011, GAM Run 10-038MAG, Texas Water Development Board, GAM Run Report, 19 p.

Kasmarek, M.C., and Robinson, J.L., 2004, Hydrogeology and Simulation of Groundwater Flow and Land-Surface Subsidence in the Northern Part of the Gulf Coast Aquifer System, Texas: United States Geological Survey Scientific investigations Report 2004-5102, 111 p.

Kasmarek, M.C., 2012, Hydrogeology and Simulation of Groundwater Flow and Land-Surface Subsidence in the Northern Part of the Gulf Coast Aquifer System, Texas, 1891-2009: United States Geological Survey Scientific investigations Report 2012-5154, 55 p.

Oliver, W., 2010, GAM Run 10-023, Texas Water Development Board, GAM Run Report, 32 p.

Wilson, C., 1967, Ground-Water Resources of Austin and Waller Counties, Texas, Texas Water Development Board Report Number 68, 201 p.

**Appendix A – Review of the GAM and the HAGM in the Context of the
Proposed Electro Purification Wells**

Appendix A – Review of the GAM and the HAGM in the Context of the Proposed Electro Purification Wells

Table of Contents

A-1	Introduction.....	2
A-2	Purpose.....	3
A-3	Aquifer Parameters	4
A-3.1	Hydraulic Conductivity	4
A-3.2	Storativity	5
A-3.3	Vertical Leakance	5
A-3.4	Elastic and Inelastic Storativity	6
A-4	Pumping	6
A-5	Model Layer Elevation versus General Head Boundary.....	8
A-6	Changes to General Head Boundary Flows with Time	9
A-7	Pumping versus GHB Flows	11
A-8	Groundwater Elevations.....	12
A-8.1	Comparisons in Area of Proposed Electro Purification Wells.....	12
A-8.2	Discussion of Use of Groundwater Elevation Data in Model Calibration	14
A-9	Subsidence	16
A-9.1	Comparison of Measured Subsidence and Model Estimated Subsidence	16
A-9.2	Compaction Parameters versus Estimated Subsidence.....	18
A-10	Discussion of Results.....	19
A-11	References.....	20

Figures A1 to A76 a presented at the end of the Appendix

A-1 Introduction

In 2004, the US Geological Survey (USGS) published the groundwater flow model that is known as the Northern Gulf Coast Groundwater Availability Model (GAM). This model is documented in Kasmarek and Robinson (2004), and was implemented with the MODFLOW-96 code developed by the US Geological Survey. The model calibration period was 1891 to 2000.

This model was used by consultants for Groundwater Management Area 14 during development of desired future conditions for the Gulf Coast Aquifer in 2010. During review of these simulations, the Texas Water Development Board found that some trends in water levels between the end of the historical-calibration period (1997) of the model and the beginning of the predictive simulation (2008) did not adequately match water-level trends (Hasan and Wade, 2010). This was a significant issue because the groundwater conservation districts in Groundwater Management Area 14 sought to use the year 2008 as the basis of drawdown calculations in the desired future condition statement, and estimating reasonably accurate 2008 conditions was considered important. More details of this comparison and the adjustments to pumping during the period 1997 to 2008 were presented by Oliver (2010) in response to a request by Groundwater Management Area 14.

Scenario 3 GAM Run 10-023 (Oliver, 2010) was then used as the basis for the Desired Future Condition (DFC) adopted by Groundwater Management Area 14. The Modeled Available Groundwater for the Gulf Coast Aquifer in Groundwater Management Area 14 is documented in Hasan and Wade (2011), and used pumping values from Scenario 3 of GAM Run 10-023 (Oliver, 2010).

In 2012, Thornhill Group, Inc. used the GAM to simulate the impacts associated with the permit applications submitted to the Bluebonnet Groundwater Conservation District for an aggregate well system to produce 20 million gallons per day (22,500 acre-feet per year) from Austin and Waller counties (Thornhill Group, 2012). This simulation consisted of pumping 20 million gallons per day from 2014 to 2060 in addition to the pumping simulated in Scenario 3 of GAM Run 10-023 (Oliver, 2010). The key findings of Thornhill Group (2012) were as follows:

- The distribution of pumping in the model files used to define aquifer desired future conditions (DFCs) does not include the proposed Electro Purification wells
- The model results suggest that drawdown from the proposed Electro Purification wells will be focused around the well field, and the primary effects of production will be on the proposed wells with limited declines on other groundwater users
- Based on the model results, the cone of depression will extend out approximately 10 miles from the proposed well field in all directions

Thornhill Group (2012, pg. 26) stated that the GAM “does not consider the many sand layers in the Evangeline and water level declines associated with the proposed production will likely be limited to the deeper sand layers where the wells will be completed”. Furthermore, Thornhill (2012) stated that the “GAM was designed to meet the purpose of estimating ground-water availability on a regional scale”, and concluded that the proposed production “can be sustained through the end of the planning period”.

Also in 2012, the USGS published an update to the groundwater flow model for the area, and is known as the Houston Area Groundwater Model (HAGM). The HAGM is documented in Kasmarek (2012), and used the MODFLOW-2000 code developed by the US Geological Survey. The calibration period for the model was 1891 to 2009. The framework of the HAGM (i.e. horizontal and vertical discretization) and basic modeling approach were the same as the earlier GAM. The significant updates include an extended period of calibration (to 2009), updated groundwater pumping estimates, and the ability to simulate clay compaction in the Burkeville and Jasper units (layers 3 and 4 of the model).

A-2 Purpose

The purpose of this Appendix to the technical review report is to detail issues with the GAM and the HAGM relative to their use in the simulation of proposed pumping by Electro Purification. The proposed Electro Purification project represents a large increase in pumping in the area of the proposed wells, and many of the potential impacts will be local in nature. Both the GAM and the HAGM are regional models, and their results will have limited use in quantifying local impacts.

As described in the main review report, both models were used in the review of the permit application to develop conclusions on a regional basis for potential impacts of the proposed project. However, several technical issues and limitations of the models are present for this particular application. In order to provide the necessary detail to those issues and limitations, this Appendix provides more details than are contained in the main technical review report.

This information includes the following for Austin, Fort Bend, and Waller counties:

- Comparisons of aquifer parameters between the GAM and the HAGM (hydraulic conductivity, storativity, vertical conductance, elastic storativity, and inelastic storativity)
- Pumping estimates that were used in the GAM from 1891 to 1996 and the pumping estimates that were used in GAM Run 10-023 (Oliver, 2010) from 1997 to 2060 that formed the basis for desired future conditions and modeled available groundwater are compared with pumping estimates that were used in the HAGM from 1891 to 2009
- Comparisons of General Head Boundary head inputs in the GAM and HAGM with model estimates of land elevations
- Time-series graphs of General Head Boundary flows in the GAM and HAGM
- Comparisons of General Head Boundary flows and pumping
- Comparisons of actual historic groundwater elevation at selected wells and model estimated groundwater elevations at those points for both historic conditions (calibration period) and predicted conditions
- Comparisons of actual subsidence with measured subsidence

Repeating maps, figures and tables that were contained in Kasmarek and Robinson (2004) and Kasmarek (2012) in this Appendix was avoided. The information contained in this Appendix was derived from the model files of the GAM and HAGM, and from the groundwater database of the Texas Water Development Board.

A-3 Aquifer Parameters

Kasmarek and Robinson (2004) documented the trial and error process used in calibrating the GAM for the period 1891 to 2000. Kasmarek (2012) documented the trial and error process used in calibrating the HAGM for the period 1891 to 2009. The processes for both models included adjustments to various aquifer parameters.

A comparison of aquifer parameters used in the GAM and HAGM are presented in Figures A1 to A19 (presented at the end of this appendix), and include hydraulic conductivity (Figures A1 to A4), storativity (Figures A5 to A8), vertical conductance (Figures A9 to A11), elastic storativity (Figures A12 to A15), and inelastic storativity (Figures A16 to A19) with one plot representing one parameter in one layer. On all plots, each of the three counties of interest to this review are designated by a different color. For each plot, the comparison consists of plotting the parameter value for each model cell from the GAM on the x-axis, and the parameter value for each model cell from the HAGM on the y-axis. For convenient reference, a one-to-one line is included on each plot. If the parameter values from each model are the same, the parameter values will plot on the one-to-one line.

A-3.1 Hydraulic Conductivity

Hydraulic conductivity describes how easily groundwater moves through the aquifer system. While permeability describes the property of the aquifer material itself, hydraulic conductivity describes the rate of movement given the aquifer system and the fluid (in this case water). The definition of hydraulic conductivity is the rate of flow under a unit hydraulic gradient through a unit cross-sectional area of the aquifer, and in these models has units of feet per day.

Hydraulic conductivity values were estimated and used as inputs to both the GAM and the HAGM, but the use of this parameter in the two models is different. In the GAM, the hydraulic conductivity estimates for each cell were multiplied by the aquifer thickness at each stress period to calculate the aquifer transmissivity. This method, specified with LAYCON=3 specification in the BCF package, allows the variation in transmissivity based on the saturated thickness. In the HAGM, the transmissivity is calculated from the saturated thickness at the beginning of the simulation and held constant for the entire simulation, as specified with LAYCON=0.

Figures A1 to A4 present the comparisons of hydraulic conductivity estimates from the GAM and the HAGM by layer. Each of the three counties is color coded. It can be seen that, in general, changes were made to Fort Bend County in layers 1 and 2 more so than in Austin and in Waller counties. In some areas, hydraulic conductivity values in Fort Bend County in the more recent HAGM were nearly doubled as compared to the GAM, and in some areas they were reduced by as much as one-half in layer 1. In layer 2, in some areas of Fort Bend County, the hydraulic conductivity is 5 to 6 times higher in the HAGM as compared to the GAM, and in other areas of Fort Bend County, the hydraulic conductivity was reduced by one-half. Note also, that in layer 2, estimates of hydraulic conductivity in Austin and Waller counties are significantly lower, and did not change between the GAM and the HAGM. Layer 3 estimates did not change in any of the three counties. Layer 4 estimates in Waller County were increased significantly, and increased somewhat in Fort Bend County.

A-3.2 Storativity

Storativity is used to define the amount of water an aquifer yields to a wells due to the compression of the aquifer in a confined aquifer, or due to reduction in head in an unconfined aquifer. In confined aquifers, groundwater fills the aquifer and the aquifer is under pressure. When a well is pumped, pressure in the aquifer is reduced, and the aquifer compresses. In an unconfined aquifer, when a well is pumping, head is reduced and the aquifer begins to dewater. The specific storage of an aquifer is defined as the volume of water that a unit volume of aquifer releases from storage under a unit decline in head (either through pressure reduction or dewatering). Storativity is the specific storage multiplied by the aquifer thickness, and is dimensionless. In general, unconfined storativity (often referred to as specific yield) is several times higher than confined storativity.

Storativity values were estimated and used as inputs to both the GAM and the HAGM, but the use of this parameter in the two models is different. In the GAM, the storativity estimates can shift between the confined or unconfined storativity values depending on where the head is relative to the top elevation in the cell. In outcrop areas of the four layers, unconfined conditions always exist during the simulation period. However, as one moves downdip from these outcrop areas, the aquifer condition is confined since the head in the aquifer is above the top of the aquifer. If pumping causes the head to drop to below the top of the aquifer, through the specification of LAYCON as 3, the GAM provides for the conversion of the storativity value to an unconfined value that is specified. However, in the HAGM, LAYCON is specified as 0, and the ability to convert from confined storativity values to unconfined storativity values as heads decline is not available in the HAGM.

Figures A4 to A8 present the comparisons of storativity estimates from the GAM and the HAGM by layer. Each of the three counties is color coded. It can be seen that there were no changes in layers 1, 2 and 3 in the HAGM as compared to the GAM. In layer 4, there appears to be a consistent and small reduction in estimated storativity in the HAGM as compared to the GAM.

A-3.3 Vertical Leakance

The GAM and the HAGM both use MODFLOW's BCF (Block Centered Flow) package, which requires the specification of a parameter known as Vcont, or vertical leakance to describe the ability of groundwater to move vertically between model layers. The parameter of vertical leakance is essentially vertical hydraulic conductivity divided by the thickness (or vertical distance between the midpoints of the two layers), and in these models has units of day^{-1} .

Figures A9 to A11 present the comparisons of vertical leakance estimates from the GAM and the HAGM. Each of the three counties is color coded. Because vertical leakance is a parameter related to the flow between layers, only three sets of parameters are required, and only three graphs are presented for the four layer model (i.e. vertical leakance between layers 1 and 2, vertical leakance between layers 2 and 3, and vertical leakance between layers 3 and 4). Note that vertical leakance between layers 1 and 2 and between layers 2 and 3 are the same in the HAGM and the GAM. However, in part of Waller County and in all of Austin and Fort Bend counties, vertical leakance in the HAGM is one order of magnitude lower than in the GAM.

A-3.4 Elastic and Inelastic Storativity

When groundwater is pumped from an aquifer, stored water in confined aquifers enters the well due to expansion of water, the compression of the aquifer material, and the compression of clayey beds that are within and adjacent to the aquifer. The resulting compression is considered elastic (i.e. reversible) if there is no permanent rearrangement of the skeletal structure of the sediments. Conversely, the resulting compression is considered inelastic (irreversible) if the reduction in pressure caused by the removal of the water causes rearrangement of the skeletal structure of the sediments. Compaction of these sediments results in a loss of storage capacity of the aquifer, and also can result in land subsidence.

The dimensionless parameters elastic and inelastic storativity, and the estimates of preconsolidation head (the minimum head value in the aquifer prior to the simulation period) are used in MODFLOW to simulate compaction and subsidence. The GAM implemented MODFLOW's IBS (Interbed Storage) package (Leake and Prudic, 1991) to simulate subsidence. The HAGM used MODFLOW's SUB (Subsidence and Aquifer System Compaction) package (Hoffmann and others, 2003) to simulate subsidence. The SUB package was an update to the IBS package. Both packages simulate compaction and subsidence using the same underlying equations and parameters. However, the SUB packages provide the opportunity to simulate time-delay effects of subsidence. When the time-delay feature of the SUB package is not used, the simulation of subsidence in both packages is the same. The HAGM used the SUB package, but did not utilize the time-delay option. Thus, the GAM and HAGM used the same underlying approach to simulating subsidence.

Figures A12 to A15 present the comparisons of elastic storativity estimates from the GAM and the HAGM. Figures A16 to A19 present the comparisons of inelastic storativity estimates from the GAM and the HAGM. Each of the three counties is color coded. Note that the changes were made in the HAGM as compared to the GAM in layers 1 and 2 for parts of Fort Bend and Waller counties, but not in Austin County. Also note that the GAM had very low estimates of elastic and inelastic storativity in layers 3 and 4, effectively resulting in an assumption that there is no mechanism to cause subsidence in layers 3 and 4. The HAGM has corrected this, and estimates for these parameters are included. In layers 1 and 2, the inelastic storativity values are 2 orders of magnitude higher than elastic storativity values in both the GAM and the HAGM.

A-4 Pumping

Kasmarek and Robinson (2004, pp. 106-107) documented the sources of data used to develop pumping from 1891 to 2000 for the GAM. These data were also used in the HAGM for this time period. Kasmarek (2012, pg. 17) documented the sources of data used to update pumping from 2001 to 2009 for the HAGM. Data from the Harris-Galveston Subsidence District, the Fort Bend Subsidence District, the San Jacinto River Authority, and the Lone Star Groundwater Conservation District were used to update pumping estimates in Fort Bend, Galveston, Harris, and Montgomery Counties. Water use data from 2001 to 2009 were compiled and combined with data from the original GAM, apparently for all other areas outside of the four main counties of interest.

Absent from the reported sources of data are the estimates of pumping used in Scenario 3 of GAM Run 10-023 (Oliver, 2010), which were developed to bridge the gap from 1997 to 2008 in development of the desired future condition for Groundwater Management Area 14, and provide a reasonable 2008 condition, which Groundwater Management 14 used as a starting point for drawdown estimates. Although not using this available dataset may have been consistent with the original intent and objective of the HAGM to the four counties of interest (Fort Bend, Galveston, Harris, and Montgomery), there are implications of not using the estimates used by TWDB in developing estimates of modeled available groundwater from 1997 to 2009 in the HAGM. Comparisons of pumping between the GAM estimates of pumping (including those used in Scenario 3 of GAM Run 10-023), and HAGM estimates of pumping for the three counties of interest (Austin, Fort Bend, and Waller) are presented in Figures A20 to A34 (presented at the end of this report).

The graphs are organized by county and model layer. Pumping estimates for each model layer are plotted with time using the hydrogeologic unit commonly associated with the layer (Layer 1 = Chicot, Layer 2 = Evangeline, Layer 3 = Burkeville, and Layer 4 = Jasper). The total pumping for all layers in each county is also presented. Within each plot, there are two pumping estimates: a blue line that represents the pumping estimates of the GAM from 1981 to 1996 and the estimates from Scenario 3 of GAM Run 10-023 from 1997 to 2060, and a red line that represents the pumping estimates in the HAGM from 1891 to 2009.

Generally, the pumping estimates from 1891 to 1997 are the same, and the red line overlies the blue line. Also, it should be noted that although both models have the same estimates of pumping in Austin and Waller Counties from 1891 to 1997, neither model seemed to have fully incorporated previous estimates of pumping in Austin and Waller Counties from 1930 to 1965 (Wilson, 1967, pg. 39).

Wilson (1967) estimated the peak of pumping from 1945 to 1965 to be much higher than either the GAM or HAGM estimates. Wilson estimated that Austin County irrigation pumping peaked in about 1954 (about 11,000 AF/yr) while the GAM and HAGM estimated a peak in about 1960 of about 8,000 AF/yr (Figure A24). Wilson estimated that Waller County irrigation pumping peaked in about 1954 (about 51,000 AF/yr) while the GAM and HAGM estimated a peak in about 1960 of about 25,000 AF/yr (Figure A34).

Although Wilson (1967) is listed as a reference by Kasmarek and Robinson (2004), there does not appear to be a specific citation where the information from that effort was used in Kasmarek and Robinson (2004). This observation will have limited effect on the four counties of interest to the HAGM (Fort Bend, Galveston, Harris, and Montgomery). However, there are implications when evaluating the potential limitations of the models use in the Bluebonnet GCD area, and in simulations instance where future pumping approaches and/or exceeds the estimates of historic pumping of Wilson (1967), such as the proposed Electro Purification wells.

A-5 Model Layer Elevation versus General Head Boundary

An important feature of the GAM was that also included in the HAGM was the use of the General Head Boundary (GHB) package to simulate recharge and groundwater-surface water interactions in the outcrops of the model layers. As stated in Kasmarek and Robinson (2004, pg. 43) and Kasmarek (2012, pg. 15), the GHB package allows the simulated water table of an aquifer system to function as a head-dependent flux boundary. The rate of flow between the water table and the adjacent deeper zone of the system is controlled by the difference between that water table (a specified head) and the head in the adjacent deeper zone (which changes with model simulation time) and by the vertical hydraulic conductance between the water table and the immediately deeper zone. Although the GHB package includes the ability to vary the GHB head with time (by specifying a different GHB head for each stress period), the implementation of the GHB package in both the GAM and HAGM assumed that the specified head remained constant throughout the simulations (1891 to 2000 for the GAM and 1891 to 2009 for the HAGM).

Figures A35 to A37 present a comparison of model layer top elevations for the outcrop area in each cell within Bluebonnet GCD with GHB head specification. As noted in Kasmarek and Robinson (2004) and in Kasmarek (2012), the GHB head represents a boundary head that can result in recharge to the groundwater system if the boundary head is higher than the aquifer head, or in groundwater discharge to the boundary if the aquifer head is higher than the boundary head. For reference purposes, the model layer top elevation generally represents the land surface elevation in the outcrop area.

Generally, there appears to be only a few differences in GHB head specification in the GAM and the HAGM, thus the red dots (HAGM) are generally overlying the blue dots (GAM). The figures also include a one to one line. If the GHB heads and the model layer elevation are the same (i.e. a boundary condition head such as streams are equal to the land surface elevation), the dots will line up on that one to one line.

It is reasonable to expect that there would be some degree of offset from the one to one line. Generally, it would be expected that the boundary head (labeled GHB elevation on the plots) would lie below the one to one line. This would mean that the boundary head is below land surface (assuming that the layer top elevation represents land surface). In some areas with relatively high topographic variation, some boundary heads above the one to one line would be expected (boundary head is above the land surface). This would be represented by dots above and to the right of the one to one line.

Inspection of Figures A35 to A37 shows that there are several instances where the boundary heads are significantly above or below the one to one line:

- In Austin County, the deviations from the assumed and averaged land surface ranges from boundary heads 92 feet below model layer top elevations to 63 feet above model layer top elevations. 33 percent of the boundary heads are within 10 feet of the model layer top elevations. Figure A38 presents the distribution of the differences using the GAM. The HAGM results are nearly identical since there are only minor differences between GHB head specification in the GAM and HAGM.

- In Fort Bend County, the deviations from the assumed and averaged land surface ranges from boundary heads 53 feet below model layer top elevations to 20 feet above model layer top elevations. 55 percent of the boundary heads are within 10 feet of the model layer top elevations. Figure A39 presents the distribution of the differences using the GAM. The HAGM results are nearly identical since there are only minor differences between GHB head specification in the GAM and HAGM.
- In Waller County, the deviations from the assumed and averaged land surface ranges from boundary heads 67 feet below model layer top elevations to 34 feet above model layer top elevations. 36 percent of the boundary heads are within 10 feet of the model top elevations. Figure A40 presents the distribution of the differences using the GAM. The HAGM results are nearly identical since there are only minor differences between GHB head specification in the GAM and HAGM.

The implication of these differences is that groundwater elevations simulated by the model are somewhat constrained by these boundary heads, and, in turn impact the amount of inflow and outflow of water. As shown below, comparison of hydrographs between actual monitoring well data and model estimates demonstrate offsets by tens of feet in some areas, which may be partly a result of specification of the GHB head.

The original of the HAGM revolved around the four counties of interest (Fort Bend, Galveston, Harris, and Montgomery). The noted differences in GHB head and model layer top elevation in Austin and Waller Counties would likely have no significant impact on the HAGM counties of interest, nor on conclusions drawn in those counties. The differences, however, in Fort Bend County are smaller than in Austin and Waller counties.

Since the GAM and HAGM use the same boundary specification, there is likely no net effect of using the HAGM instead of the GAM. The analysis does, however, highlight an important limitation of the use of the results of either model in Austin and Waller counties due to the differences.

A-6 Changes to General Head Boundary Flows with Time

As reported in Kasmarek and Robinson (2004, pg. 43) and in Kasmarek (2012, pg. 16), a key assumption in the simulating recharge and groundwater-surface water interaction with General Head Boundaries is that there are no long-term trends in the water table. Kasmarek and Robinson (2004, pg. 43) stated that the assumption “is believed reasonable over most of the GAM area, although the assumption might not be valid in some areas of intense withdrawals”. Kasmarek (2012, pg. 16) simply stated that the “assumption is believed reasonable over most of the HAGM study area”. As stated above, GHB heads in the GAM and the HAGM did not vary with time. Thus, the boundary head that controlled recharge to and discharge from the aquifer system was the same from 1891 to 2000 for the GAM, and from 1891 to 2009 for the HAGM despite large increases in pumping over that time period. Also, as previously noted, the GHB package provides for the user to specify the boundary heads for each stress period, thus providing a means to better simulate surface water groundwater interaction, although that feature was not implemented in the HAGM. The use of GHBs to simplify overlying flow processes was noted in Kasmarek and Robinson (2004, pg. 45):

“The rationale for this decision is that the general-head boundary package, assuming the model is adequately calibrated, would account for stream discharge to the level of accuracy that such discharge is known. Few measured data are available on streamflow gains/losses for the major streams that flow across the outcrops of the Gulf Coast aquifers.”

When the issue updating the GAM was originally brought to the TWDB by the USGS and the subsidence districts, the issue of replacing the GHBs with recharge and streams in the update was discussed. As the project went forward and became the HAGM, however, it is apparent that decisions were made to continue to use the GHBs as noted in Kasmarek (2012, pg. 16):

“Because aquifer discharge to streams is not well known, such data are not particularly helpful for comparison with simulated data for purposes of calibration; there was little incentive to add more complexity to an already complex model by explicitly computing flow between streams to the aquifers. Although some additional recharge rates have recently been determined (Tarver, 1968; Sandeen, 1972; Loskot and others, 1982; Baker, 1986; and Kasmarek and Robinson, 2004), the additional complexity of including that information specifically, by substituting the GHB package with the River or Stream package and the Recharge package, was determined to be beyond the scope of this report.”

For the stated objectives of the HAGM and the area of interest (Fort Bend, Galveston, Harris, and Montgomery Counties), the decision to continue to use GHBs to simulate recharge and groundwater-surface water interaction must be viewed in the context of future groundwater management in the area (i.e. decreased pumping). Under this expected condition in the four counties of interest associated with HAGM development, the GHB flow into the aquifer system will tend to decrease with time in the future as pumping decreases and groundwater elevations rise. Thus, for its intended purpose in the four counties of interest, the continued use of GHBs, while not ideal, is certainly not a fatal flaw.

The proposed Electro Purification wells represent a significant increase in the amount of pumping in a relatively small area. Simulating these proposed wells with either the GAM or the HAGM coupled with the use of GHBs heads that do not vary with time will result in simulated increases in GHB flow into the aquifer system that may or may not be accurate.

In order to place this limitation into context with the calibrated models (both GAM and HAGM) and the GAM’s previous use as a tool to estimate modeled available groundwater for the desired future conditions adopted by the groundwater conservation districts of Groundwater Management Area 14, Figures A41 to A43 present the simulated GHB flows into the aquifer system for each of the three counties of interest. Note that the blue line represents the simulation associated with Scenario 3 of GAM Run 10-023 (covering the years 1891 to 2060), and the red line represents the simulation associated with the calibration of the HAGM (covering the years 1891 to 2009).

GHB flows into the aquifer system represent a combined inflow of recharge from precipitation and inflow from and outflow to streams in the outcrop areas of the model. Note that in all three counties, there is a significant increase in inflow from the GHB boundary into the aquifer that

essentially means that there is an increase in the sum of recharge from precipitation plus recharge from streamflow.

The large increase in GHB inflow may have an impact on drawdown estimates (i.e. underestimate drawdown if the inflow increases are unreasonable). Also note the differences in estimates between the GAM and the HAGM.

- Austin County (Figure A41): Simulated GHB inflows rise from less than 6,000 AF/yr in 1891 to slightly over 16,000 AF/yr by 2009, and then are simulated to increase to almost 24,000 AF/yr by 2060 under the DFC condition. Differences between the GAM and the HAGM are relatively minor.
- Fort Bend County (Figure A42): Prior to 1930, there is a net discharge of groundwater to the GHB boundaries (i.e. streams) in Fort Bend County. After 1930, there is an increasing amount of net inflow that is estimated to be about 60,000 AF/yr with the HAGM and about 80,000 AF/yr in the GAM by 2009, and increases only to about 90,000 by 2060.
- Waller County (Figure A43): HAGM simulated inflows are less than GHB inflows simulated by the GAM. In the GAM simulation, inflows are simulated to be slightly over 5,000 AF/yr in 1891 and increase to about 30,000 AF/yr in 2009, and then are simulated to increase to about 45,000 AF/yr in 2060.

A-7 Pumping versus GHB Flows

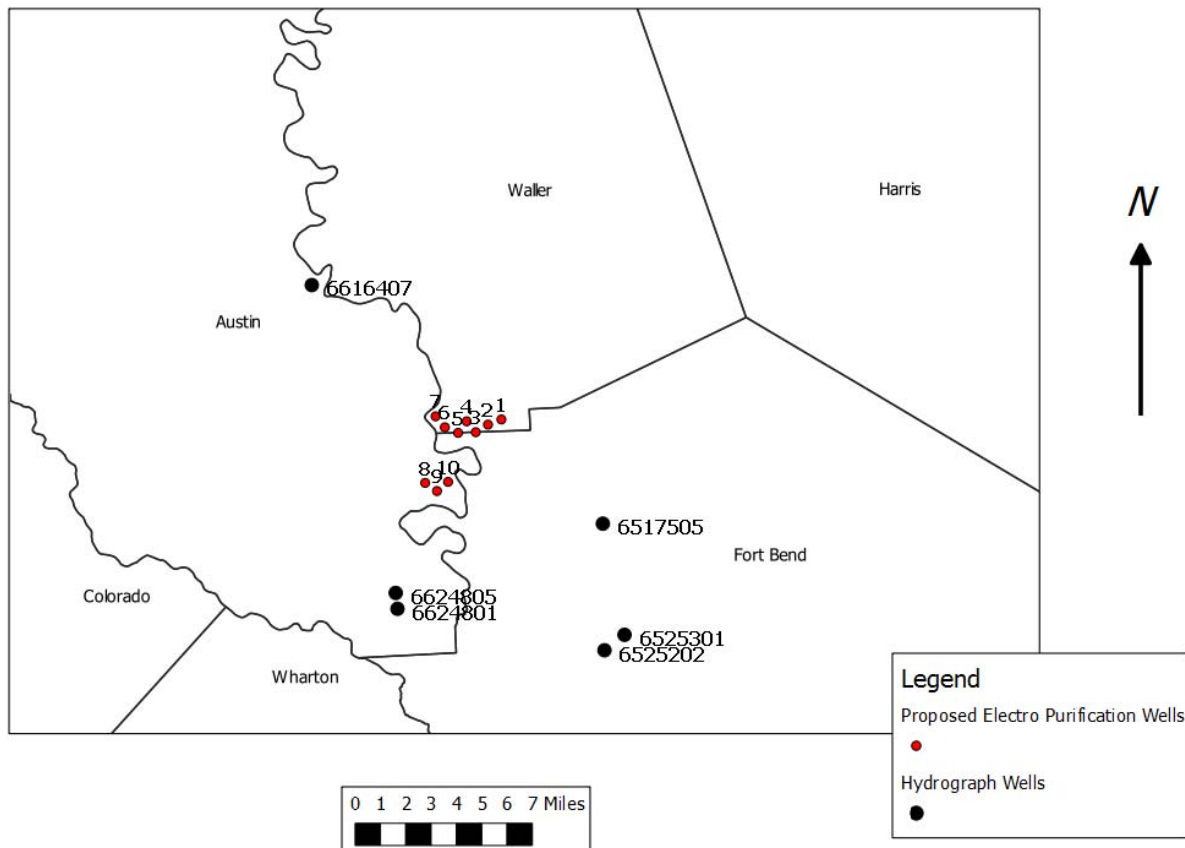
Time series of simulated GHB flows and pumping for both models were presented above. The close association of increases of simulated GHB flows with pumping was discussed. Figures A44 to A46 present plots of pumping versus GHB flows (one for each of the three counties of interest):

- Austin County (Figure A44): Note the strong correlation between pumping and GHB flow for pumping less than about 10,000 AF/yr for both the GAM and the HAGM. For pumping up to 10,000 AF/yr, both models simulate GHB inflows that are slightly higher than the pumping. For pumping between 10,000 AF/yr and about 15,000 AF/yr, GHB flows increase, and tend to be slightly higher than the pumping, but the estimates are spread out more than lower pumping amounts, likely due to transient effects of the increases. The DFC condition (pumping about 23,000 AF/yr) has a range of GHB inflows that are related to the transient effect of the simulated pumping increases after 2010.
- Fort Bend County (Figure A45): Note the correlation between pumping and GHB flows. Also, the condition of net discharge that was seen prior to 1930 is associated with pumping less than about 5,000 AF/yr. Essentially, only a small amount of pumping (according to this model) results in net recharge to the aquifer system in Fort Bend County. Under the DFC condition, pumping that is about 100,000 to 120,000 AF/yr results in an inflow from the GHB boundary of about 90,000 AF/yr.
- Waller County (Figure A46): As with the previous graphs, the correlation between pumping and GHB flows is evident, as is the transient response under predicted conditions after 2010 in GAM Run 10-023.

A-8 Groundwater Elevations

A-8.1 Comparisons in Area of Proposed Electro Purification Wells

As part of the review of the GAM and HAGM in the context of the proposed Electro Purification project, hydrographs of actual groundwater elevations were compared to hydrographs of simulated groundwater elevations. The Texas Water Development Board groundwater database was used to obtain data and information on wells in Austin, Fort Bend and Waller counties relative to well location, well construction details, and historic groundwater elevations. There were 181 wells that met the following criteria: 1) at least one historic groundwater elevation measurement, and 2) screen top and bottom elevation place the well in a single model layer (82 in Austin County, 78 in Fort Bend County, and 21 in Waller County). Of these 181 wells, six were located in the vicinity of the proposed Electro Purification wells and had more than 10 recent groundwater elevation measurements. The locations of these wells, and the locations of the proposed Electro Purification wells are shown below:



Locations of Proposed Electro Purification Wells and Wells with Historic Groundwater Elevation Data for which Hydrographs were constructed

Construction details and data on historic groundwater elevation measurements are shown in Table A1.

Table A1. Summary of Well Construction Data for Selected Wells

Well Number	6517505	6525202	6525301	6616407	6624801	6624805
County	Fort Bend	Fort Bend	Fort Bend	Austin	Austin	Austin
Land Surface Elevation (ft MSL)	104	115	111	121	125	131
Well Depth (ft)	450	292	438	165	610	725
Depth to Top of Screen (ft)	329	120	91	147	586	530
Depth to Bottom of Screen (ft)	450	279	432	165	606	702
Elevation of Screen Top (ft MSL)	-225	-5	20	-26	-461	-399
Elevation of Screen Bottom (ft MSL)	-346	-164	-321	-44	-481	-571
Number of Historic Groundwater Elevation Measurements	22	22	80	38	35	28
Year of Earliest Groundwater Elevation Measurement	1985	1960	1945	1966	1957	1973
Year of Most Recent Groundwater Elevation Measurement	2011	2011	2011	2011	2011	2011
Model Layer	1	1	1	2	2	2
Model Row	59	63	63	45	57	56
Model Column	70	67	68	67	62	62
X-Coordinate (GAM)	6212777.5	6213116	6217299	6152008	6169900.5	6169529
Y-Coordinate (GAM)	19134288	19107890	19111112	19184036	19116538	19119842

Hydrographs of these six wells are presented as Figures A47 to A52 (comparison with GAM results), and Figures A53 to A58 (comparison with HAGM results). The GAM comparison used the simulation from Scenario 3 of GAM Run 10-023 (Oliver, 2010) which covered the time period 1891 to 2060 (1891 to 1997 represented pumping estimates from the calibrated model, 1998 to 2008 represented pumping estimates described in Oliver (2010), and 2009 to 2060 represented pumping estimates that were the basis of the desired future condition/modeled available groundwater). The HAGM comparison used the calibrated estimates of pumping from 1891 to 2009, and added the pumping estimates described in Oliver (2010) to represent the pumping associated with the desired future condition/modeled available groundwater scenario.

These hydrographs presented in Figures A47 to A58 include historic groundwater elevations data, simulated groundwater elevation data from the GAM or HAGM as appropriate, land surface elevation, elevations of the screened interval and historic and future pumping in three zones: Zone 1) pumping within the cell where the well is located, Zone 2) pumping in the eight cells immediately surrounding zone 1, and Zone 3) pumping in the 16 cells immediately surrounding zone 2. Thus, pumping (both historic and projected) in a 25 square mile area surrounding the well of interest is presented in aid interpretation of the groundwater elevation changes.

In order to facilitate comparison of actual groundwater elevations and the estimated groundwater elevations from the GAM and HAGM at these six wells, Figures A59 to A64 were constructed without additional data associated with land surface elevations, screened intervals, and pumping.

Note that in model layer 1 (Chicot Aquifer), the actual groundwater elevations are relatively constant, but that both models tend to simulate a significant drawdown starting in about 1940. Based on these hydrographs, it appears that, in the area of the proposed Electro Purification wells, simulations of future drawdown due to increased pumping in model layer 1 are likely overestimates (drawdown in the model is likely higher than actual drawdown).

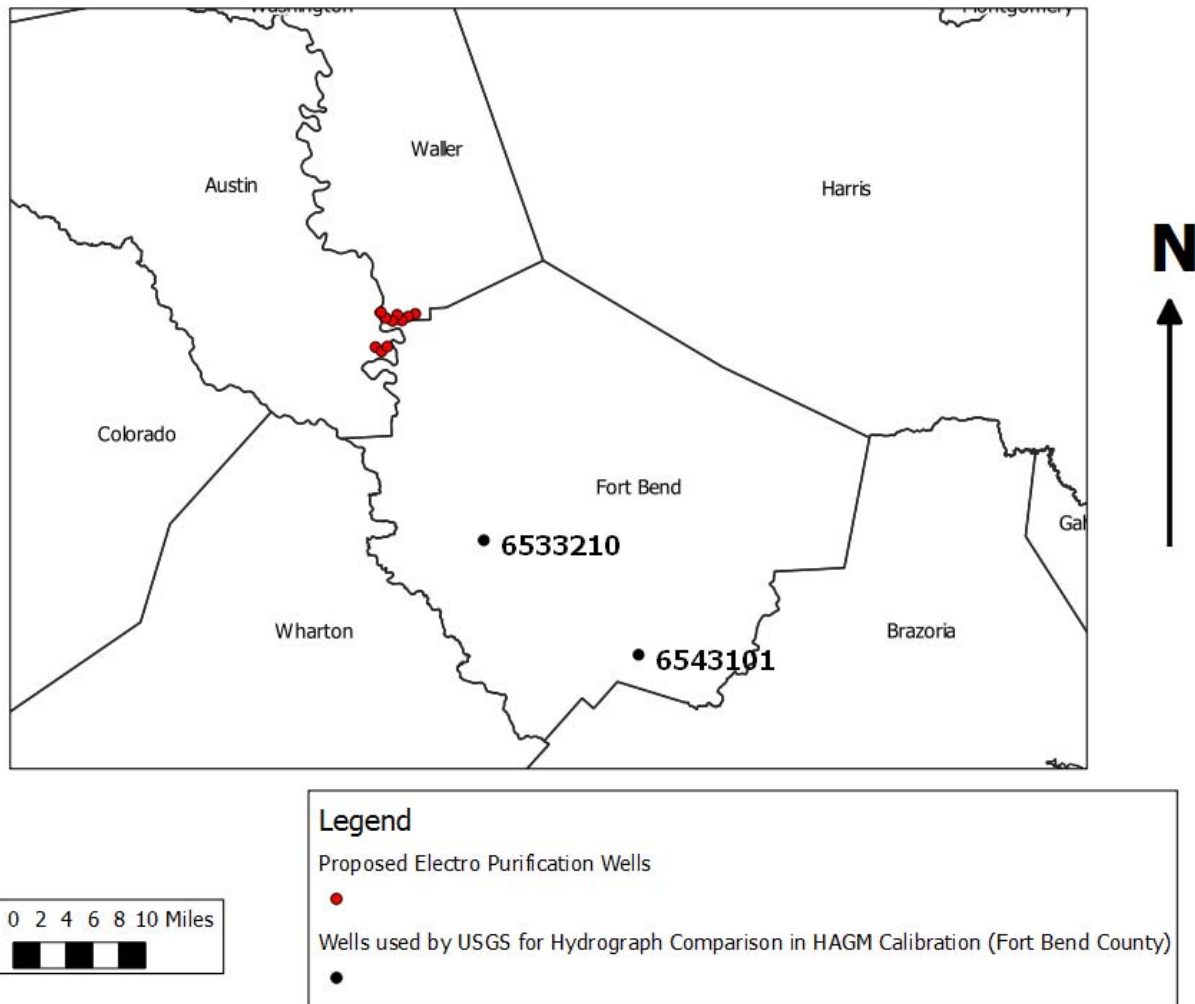
Note that in model layer 2 (Evangeline Aquifer), both models mimic the changes in historic and observed groundwater elevation better than in layer 1 in two of the three wells. However, it appears that the GAM matches the historic groundwater elevations from the 1960s to the 1990s than the HAGM in Well 66-24-801. In contrast, neither model tracks the historic record of Well 66-16-407 where no significant downward trend is present in the historic record, but the models estimate a significant drawdown that began in the 1940s and continues to present.

A-8.2 Discussion of Use of Groundwater Elevation Data in Model Calibration

Kasmarek and Robinson (2004, p 64-88) summarized calibration statistics for the GAM for the years 1977 and 2000, presented comparison contour maps of each model layer and presented hydrographs of selected wells, none of which were located in Austin, Fort Bend, or Waller counties. Kasmarek and Robinson (2004, p. 48-49) describe these elements in model calibration.

Kasmarek (2012, p. 17 and 19) summarized calibration of the HAGM. Calibration statistics for the year 2009 were used reported (Kasmarek, 2012, p. 35 and 36), comparison contour maps of each model layer were presented (Kasmarek, 2012, p. 32-34 and 37-39), and hydrographs of selected wells were presented (Kasmarek, 2012, p. 40-42). None of the selected wells were located in Austin or Waller counties. Two of the selected hydrographs were located in Fort Bend County: one well reportedly completed in the Chicot Aquifer, and one well reportedly completed in the Evangeline Aquifer. The locations of these wells are shown below.

It can be seen that these wells are located in the southern portion of Fort Bend County, and are thus well removed from the area of interest for this review. In reviewing the hydrographs presented by the USGS, the well that the USGS used as a Chicot Aquifer well (65-43-101) may be an Evangeline Aquifer well. The Texas Water Development Board (TWDB) database lists the well depth as 1,195 feet, and it is coded as a “Chicot and Evangeline Aquifer” well. The companion “casing” database maintained by the TWDB does not have any data on this particular well. In contrast, the well the USGS used as an Evangeline Aquifer well in Fort Bend County (65-33-210) is coded by the TWDB as an “Evangeline Aquifer” well, and its depth is 965 feet. The companion casing database lists its screen depths between 852 and 965 feet.



Location of Wells used by USGS for Hydrograph Comparison in HAGM Calibration in Fort Bend County

In comparing these well construction data to the GAM and the HAGM model layer elevations, the well listed as an Evangeline Aquifer well (65-33-210) lies completely within model layer 2, and can be considered an Evangeline Aquifer well. The comparison hydrograph using the GAM for this well is presented as Figure A65 and Figure A66 presents the comparison hydrograph for this well using the HAGM. These figures present the same data as Figures A47 to A58 presented previously (land surface elevation, simulated groundwater elevations, actual groundwater elevations, screened interval elevations, and simulated pumping in three zones around the model cell in which the well is located). Note that the general match of the model estimated groundwater elevations and actual groundwater elevations are good, and there are slight differences between the GAM estimates and the HAGM estimates. Also note that the assumed pumping is relatively low and is somewhat different from 1997 to 2009 as explained earlier.

Well 65-43-101, which was listed by the USGS as a Chicot Aquifer well, but appears to be an Evangeline Aquifer well based on TWDB data was further evaluated by comparing its reported

depth with model layer elevations. The depth of well 65-43-101 is reported as 1,195 feet, and the listed land surface elevation is 76 feet above mean sea level. That means that the depth of the well is at elevation -1,119 feet. In model row 70, column 63 (the reported model cell in which the well is located by the USGS), the bottom elevation of layer 1 (Chicot Aquifer) is -677 feet, and the bottom elevation of layer 2 (Evangeline Aquifer) is -2,339 feet. Thus, this well penetrates partially into the Evangeline Aquifer. Without data on well completion (i.e. screened interval), it is not possible to state with confidence its completion. Figure A67 presents the actual groundwater elevation data and compares it to groundwater elevation estimates from the GAM for both layers 1 and 2 (Chicot and Evangeline, respectively). Figure A68 presents a similar comparison using estimates from the HAGM. Note that the model estimated groundwater elevations for layers 1 and 2 in both the GAM and the HAGM track together and have exhibited a significant decline from pre-development times (i.e. prior to 1930).

These plots demonstrate that there is little significant difference in the choice of which model layer results to use in comparing the actual groundwater elevation data. It also highlights that the model simulates hydraulic connection between layers 1 and 2 (Chicot and Evangeline).

A-9 Subsidence

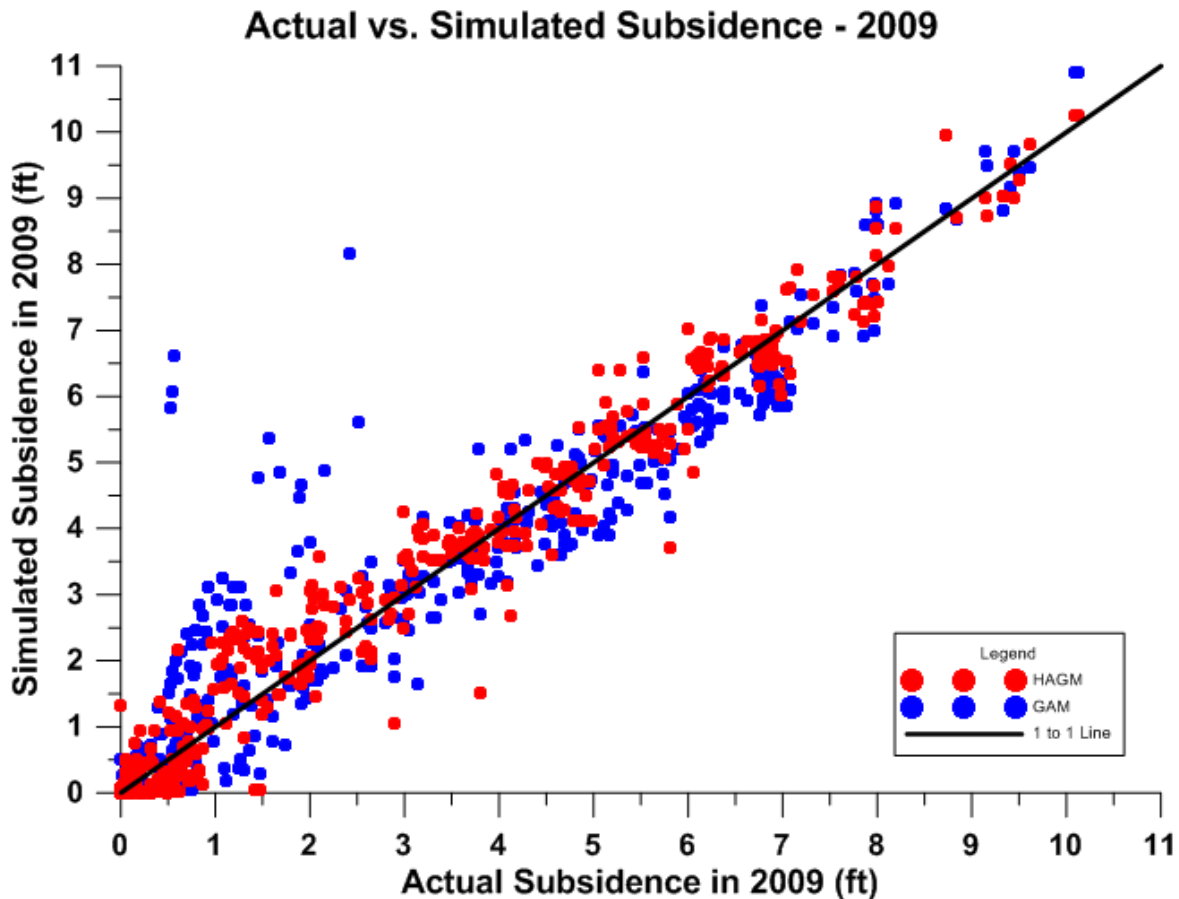
As noted previously, when groundwater is pumped from an aquifer, stored water in confined aquifers enters the well due to expansion of water, the compression of the aquifer material, and the compression of clayey beds that are within and adjacent to the aquifer. The resulting compression is considered elastic (i.e. reversible) if there is no permanent rearrangement of the skeletal structure of the sediments. Conversely, the resulting compression is considered inelastic (irreversible) if the reduction in pressure caused by the removal of the water causes rearrangement of the skeletal structure of the sediments. Compaction of these sediments results in a loss of storage capacity of the aquifer, and also can result in land subsidence.

A-9.1 Comparison of Measured Subsidence and Model Estimated Subsidence

The GAM and HAGM provide estimates of compaction (on a layer-by-layer basis) and estimates of subsidence (essentially the sum of the compaction of the individual layers). Kasmarek and Robinson (2004) and Kasmarek used subsidence results as part of the calibration of the GAM and HAGM. However, the calibration appears to have been limited to end-of-simulation comparisons, and appears that intermediate time-period measurements were not used. This is in contrast to groundwater elevation calibration where hydrographs of groundwater elevations were used to calibrate the model to a certain extent using the trend in groundwater elevation changes.

Kasmarek and Robinson (2004, p. 90 and 93-95) discussed and presented subsidence results for the GAM based on a comparison of actual subsidence data and simulated subsidence data in the year 2000. Kasmarek (2012, p. 35-36 and 45-46) discussed and presented subsidence results for the HAGM based on comparisons of actual subsidence data and simulated subsidence data in the years 2000 and 2009. Accompanying the model files for the HAGM was a file named *subsidence.calibration.targets.csv* that provided actual subsidence measurements at 474 points in the model area, apparently from the year 2000. These data were apparently used by Kasmarek (2012) to construct the subsidence map that appeared on page 46 of the model documentation.

These actual subsidence data from 1906 to 2000 were used to construct a plot that compared actual subsidence as reported by the UGSG in the file provided with the HAGM model files with subsidence estimated by the GAM and the HAGM at those points from 1891 to 2009 as was done by Kasmarek (2012). The plot is presented below, and also includes a one-to-one line to facilitate the comparison:



Comparison of Actual Subsidence from 1906 to 2000 and Estimated Subsidence from 1891 to 2009 from the GAM and the HAGM

Recall that the GAM only simulated compaction in model layers 1 and 2 through the specification of elastic and inelastic storativity values. The HAGM included elastic and inelastic storativity values in all four model layers. Thus, from a subsidence perspective, the HAGM is a more comprehensive model. An inspection of the above plot suggests that the HAGM has fewer outliers than the GAM when comparing the model results to actual subsidence measurements. Based on this plot, it appears that the HAGM estimates subsidence over a near-century timeframe within about a foot of actual subsidence.

A-9.2 Compaction Parameters versus Estimated Subsidence

In reviewing the use of the GAM and HAGM, it was recognized that historic subsidence had occurred mainly in eastern Brazoria County, eastern Fort Bend County, Galveston County, Harris County, and southeastern Waller County. Groundwater pumping in these areas has historically been higher than other parts of the model area where significant subsidence has not been observed. Because of the importance of this issue in the review of the proposed Electro Purification wells, an analysis was completed to further evaluate the relationship of model-estimated compaction parameters (elastic and inelastic storativity) and model-estimated subsidence. A key element of this analysis is to characterize the model-estimated compaction parameters used in the area of the proposed Electro Purification wells, and observe if they are different than model-estimated parameters used in areas where historic subsidence measurement have been taken.

The following figures present this analysis:

- Figure A69 – Elastic Storativity vs. Simulated Subsidence: Layer 1 (GAM and HAGM)
- Figure A70 – Elastic Storativity vs. Simulated Subsidence: Layer 2 (GAM and HAGM)
- Figure A71 – Elastic Storativity vs. Simulated Subsidence: Layer 3 (HAGM Only)
- Figure A72 – Elastic Storativity vs. Simulated Subsidence: Layer 4 (HAGM Only)
- Figure A73 – Inelastic Storativity vs. Simulated Subsidence: Layer 1 (GAM and HAGM)
- Figure A74 – Inelastic Storativity vs. Simulated Subsidence: Layer 2 (GAM and HAGM)
- Figure A75 – Inelastic Storativity vs. Simulated Subsidence: Layer 3 (HAGM Only)
- Figure A76 – Inelastic Storativity vs. Simulated Subsidence: Layer 4 (HAGM Only)

In each of these plots, the x-axis is the parameter of interest (elastic or inelastic storativity), and the y-axis is the estimated subsidence. Each point on the plot represents one of the locations in the USGS file that accompanied the HAGM files for which a measured subsidence value was reported. The model files were queried to obtain the elastic and inelastic storativity values at each of those points for each model layer. The plots, therefore, provide the ability to evaluate correlation between compaction parameters and estimated subsidence by observing the range of parameter values used, and the associated subsidence estimate.

The vertical lines in the plot represent the average parameter value in the five cells that represent the locations of the proposed Electro Purification wells. This provides the ability to evaluate if compaction parameter values in the area of the proposed Electro Purification wells are significantly different than in areas where subsidence has been observed.

The blue points and blue lines in the plots represent the parameter estimates and subsidence estimates from the GAM, and the red points and red lines represent the parameter estimates and subsidence estimates from the HAGM. Note that the blue dots only appear on plots for layers 1 and 2. As discussed earlier, the GAM did not simulate compaction in layers 3 and 4 (i.e. parameter estimates were 1E-10). Including compaction parameters in layers 3 and 4 was a key feature of the updated HAGM.

It can be seen that the GAM and HAGM did not bias the model with certain compaction parameters in areas with observed subsidence versus areas with little or no observed subsidence. It is also

clear that the area of the proposed Electro Purification wells has compaction parameters that are consistent with parameters in areas where subsidence has occurred. There is nothing in this analysis to suggest that the GAM or the HAGM would yield unusual results (compared to areas where subsidence has occurred) with respect to compaction or subsidence when simulating pumping in the area of the proposed Electro Purification wells.

A-10 Discussion of Results

The HAGM is an update of the GAM, and, it would be expected that there would be an advantage in using the HAGM for the review of the Electro Purification permit application. This is particularly true with respect to simulation of potential subsidence effects

Both models, as currently implemented, are limited by the use of the GHB package (particularly the assumption of static GHB heads) to simulate recharge and groundwater-surface water interactions. In areas where groundwater pumping is expected to decrease, the approach used in the GAM and HAGM, while not ideal, is not a fatal flaw. However, in areas where pumping is expected to increase in the future, the assumption of static GHB heads will result in increases in GHB flows into the aquifer system that may not be realistic.

The comparison of actual historic groundwater elevation data with model estimates of groundwater elevations during the historic period in six wells in the vicinity of the proposed Electro Purification wells suggests that predictions in layer 1 (the Chicot Aquifer) are not reliable.

Until a model of the area is developed that simulated recharge and groundwater-surface water interaction with more realistic constraints under increasing pumping scenarios (e.g. with the MODFLOW recharge and stream packages), the limitations of the model with respect to groundwater elevation estimates must be acknowledged. Neither model is likely reliable with respect to estimates of future drawdown, especially in the case of a proposed substantial increase in pumping. However, long-term subsidence estimates may be considered more reliable than the drawdown estimates given the evaluation that is presented in this Appendix.

Overall, the accuracy of long-term subsidence estimates are within a foot of actual long-term subsidence measurements as documented by the US Geological Survey in other areas of the model where subsidence has been measured. There is still a considerable degree of uncertainty in the subsidence estimates in an area where a large and concentrated increase in pumping is proposed.

A-11 References

Hoffmann, J., Leake, S.A., Galloway, D.L., and Wilson, A.M., 2003. MODFLOW-2000 Groundwater Model – User Guide to the Subsidence and Aquifer Compaction (SUB) Package. U.S. Geological Survey Open File Report 03-233, 52 p.

Kasmarek, M.C., and Robinson, J.L., 2004, Hydrogeology and Simulation of Groundwater Flow and Land-Surface Subsidence in the Northern Part of the Gulf Coast Aquifer System, Texas: United States Geological Survey Scientific investigations Report 2004-5102, 111 p.

Kasmarek, M.C., 2012, Hydrogeology and Simulation of Groundwater Flow and Land-Surface Subsidence in the Northern Part of the Gulf Coast Aquifer System, Texas, 1891-2009: United States Geological Survey Scientific investigations Report 2012-5154, 55 p.

Leake, S.A. and Prudic, D.E., 1991. Documentation of a Computer Program to Simulate Aquifer-System Compaction using the Modular Finite-Difference Ground-Water Flow Model. Techniques of Water-Resource Investigations of the United States Geological Survey, Book 6, Chapter A2, 74 p.

Oliver, W., 2010, GAM Run 10-023, Texas Water Development Board, GAM Run Report, 32 p.

Thornhill Group, Inc., 2012. Phase 1 Hydrogeologic Report – Non-Exempt Well Permit Application, Bluebonnet Groundwater Conservation District, Austin and Waller Counties, Texas. Report prepared for Mt. Tim Throckmorton, Electro Purification, LLC, 38 p.

Wilson, C., 1967, Ground-Water Resources of Austin and Waller Counties, Texas, Texas Water Development Board Report Number 68, 201 p.

Appendix A Figures - Model Parameters

Figure Number	Model Parameter	Model Layer	Plotting Approach	County	Page Number
A1	Hydraulic Conductivity	1	GAM vs. HAGM	Austin, Fort Bend, Waller	1
A2	Hydraulic Conductivity	2	GAM vs. HAGM	Austin, Fort Bend, Waller	1
A3	Hydraulic Conductivity	3	GAM vs. HAGM	Austin, Fort Bend, Waller	2
A4	Hydraulic Conductivity	4	GAM vs. HAGM	Austin, Fort Bend, Waller	2
A5	Storativity	1	GAM vs. HAGM	Austin, Fort Bend, Waller	3
A6	Storativity	2	GAM vs. HAGM	Austin, Fort Bend, Waller	3
A7	Storativity	3	GAM vs. HAGM	Austin, Fort Bend, Waller	4
A8	Storativity	4	GAM vs. HAGM	Austin, Fort Bend, Waller	4
A9	Vertical Leakance	1 & 2	GAM vs. HAGM	Austin, Fort Bend, Waller	5
A10	Vertical Leakance	2 & 3	GAM vs. HAGM	Austin, Fort Bend, Waller	5
A11	Vertical Leakance	3 & 4	GAM vs. HAGM	Austin, Fort Bend, Waller	6
A12	Elastic Storativity	1	GAM vs. HAGM	Austin, Fort Bend, Waller	7
A13	Elastic Storativity	2	GAM vs. HAGM	Austin, Fort Bend, Waller	7
A14	Elastic Storativity	3	GAM vs. HAGM	Austin, Fort Bend, Waller	8
A15	Elastic Storativity	4	GAM vs. HAGM	Austin, Fort Bend, Waller	8
A16	Inelastic Storativity	1	GAM vs. HAGM	Austin, Fort Bend, Waller	9
A17	Inelastic Storativity	2	GAM vs. HAGM	Austin, Fort Bend, Waller	9
A18	Inelastic Storativity	3	GAM vs. HAGM	Austin, Fort Bend, Waller	10
A19	Inelastic Storativity	4	GAM vs. HAGM	Austin, Fort Bend, Waller	10
A20	Pumping	Chicot	Time Series	Austin	11
A21	Pumping	Evangeline	Time Series	Austin	11
A22	Pumping	Burkeville	Time Series	Austin	12
A23	Pumping	Jasper	Time Series	Austin	12
A24	Pumping	Total	Time Series	Austin	13
A25	Pumping	Chicot	Time Series	Fort Bend	14
A26	Pumping	Evangeline	Time Series	Fort Bend	14
A27	Pumping	Burkeville	Time Series	Fort Bend	15
A28	Pumping	Jasper	Time Series	Fort Bend	15
A29	Pumping	Total	Time Series	Fort Bend	16
A30	Pumping	Chicot	Time Series	Waller	17
A31	Pumping	Evangeline	Time Series	Waller	17
A32	Pumping	Burkeville	Time Series	Waller	18
A33	Pumping	Jasper	Time Series	Waller	18
A34	Pumping	Total	Time Series	Waller	19
A35	Layer Top vs. GHB	Top	Elevation Comparison	Austin	20
A36	Layer Top vs. GHB	Top	Elevation Comparison	Fort Bend	20
A37	Layer Top vs. GHB	Top	Elevation Comparison	Waller	21
A38	Layer Top and GHB	Top	Distribution of Differences	Austin	21
A39	Layer Top and GHB	Top	Distribution of Differences	Fort Bend	22
A40	Layer Top and GHB	Top	Distribution of Differences	Waller	22
A41	GHB Flow	Top	Time Series	Austin	23
A42	GHB Flow	Top	Time Series	Fort Bend	23
A43	GHB Flow	Top	Time Series	Waller	24
A44	Pumping vs. GHB	Top	Pumping vs. GHB	Austin	24
A45	Pumping vs. GHB	Top	Pumping vs. GHB	Fort Bend	25
A46	Pumping vs. GHB	Top	Pumping vs. GHB	Waller	25
A47	Well 65-17-505	1	Hydrograph (GAM)	Fort Bend	26
A48	Well 65-25-202	1	Hydrograph (GAM)	Fort Bend	26
A49	Well 65-25-301	1	Hydrograph (GAM)	Fort Bend	27
A50	Well 66-16-407	2	Hydrograph (GAM)	Austin	27
A51	Well 66-24-801	2	Hydrograph (GAM)	Austin	28
A52	Well 66-24-805	2	Hydrograph (GAM)	Austin	28
A53	Well 65-17-505	1	Hydrograph (HAGM)	Fort Bend	29
A54	Well 65-25-202	1	Hydrograph (HAGM)	Fort Bend	29
A55	Well 65-25-301	1	Hydrograph (HAGM)	Fort Bend	30
A56	Well 66-16-407	2	Hydrograph (HAGM)	Austin	30
A57	Well 66-24-801	2	Hydrograph (HAGM)	Austin	31
A58	Well 66-24-805	2	Hydrograph (HAGM)	Austin	31
A59	Well 65-17-505	1	Hydrograph (GAM and HAGM)	Fort Bend	32
A60	Well 65-25-202	1	Hydrograph (GAM and HAGM)	Fort Bend	32
A61	Well 65-25-301	1	Hydrograph (GAM and HAGM)	Fort Bend	33
A62	Well 66-16-407	2	Hydrograph (GAM and HAGM)	Austin	33
A63	Well 66-24-801	2	Hydrograph (GAM and HAGM)	Austin	34
A64	Well 66-24-805	2	Hydrograph (GAM and HAGM)	Austin	34
A65	Well 65-33-210	2	Hydrograph (GAM)	Fort Bend	35
A66	Well 65-33-210	2	Hydrograph (HAGM)	Fort Bend	35
A67	Well 65-43-101	1 and 2	Hydrograph (GAM)	Fort Bend	36
A68	Well 65-43-101	1 and 2	Hydrograph (HAGM)	Fort Bend	36
A69	Elastic Storativity vs. Subsidence	1	Elastic Storativity vs. Subsidence	Entire Model Area	37
A70	Elastic Storativity vs. Subsidence	2	Elastic Storativity vs. Subsidence	Entire Model Area	37
A71	Elastic Storativity vs. Subsidence	3	Elastic Storativity vs. Subsidence	Entire Model Area	38
A72	Elastic Storativity vs. Subsidence	4	Elastic Storativity vs. Subsidence	Entire Model Area	38
A73	Inelastic Storativity vs. Subsidence	1	Inelastic Storativity vs. Subsidence	Entire Model Area	39
A74	Inelastic Storativity vs. Subsidence	2	Inelastic Storativity vs. Subsidence	Entire Model Area	39
A75	Inelastic Storativity vs. Subsidence	3	Inelastic Storativity vs. Subsidence	Entire Model Area	40
A76	Inelastic Storativity vs. Subsidence	4	Inelastic Storativity vs. Subsidence	Entire Model Area	40

Figure A1
Hydraulic Conductivity (ft/day) - Layer 1

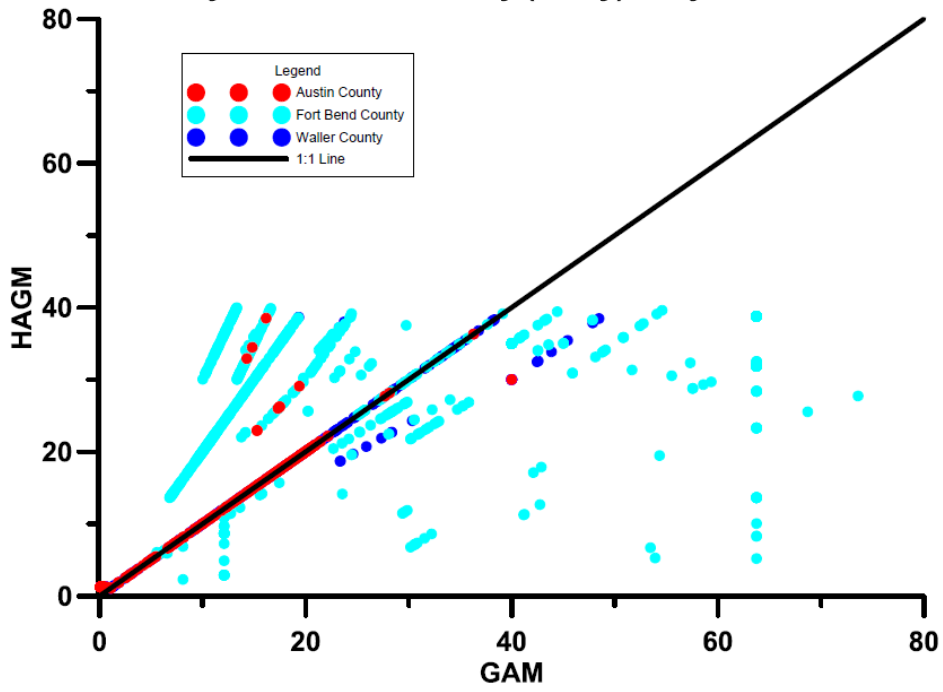


Figure A2
Hydraulic Conductivity (ft/day) - Layer 2

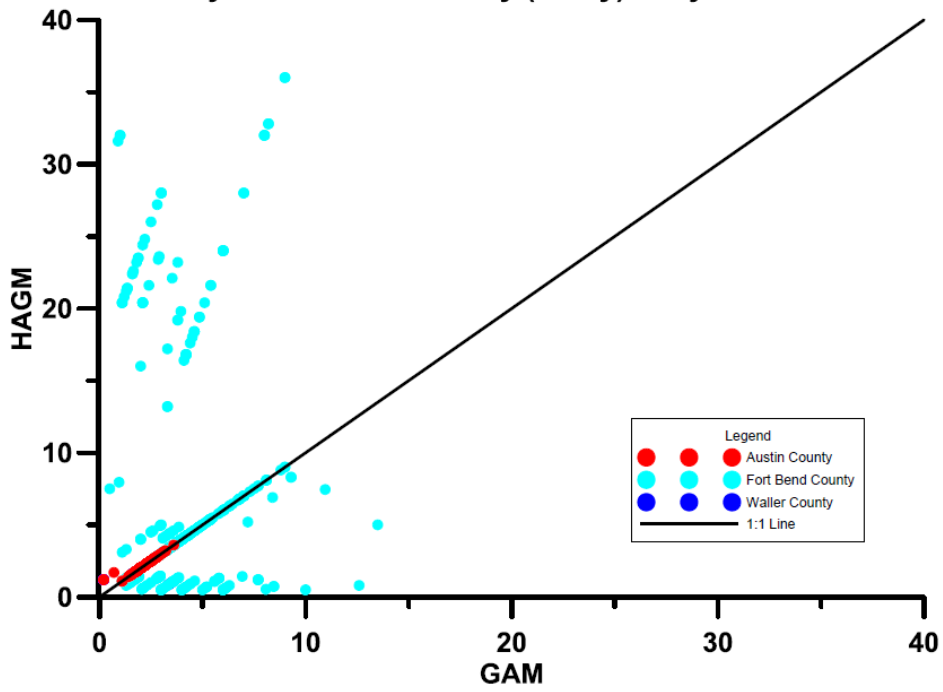


Figure A3
Hydraulic Conductivity (ft/day) - Layer 3

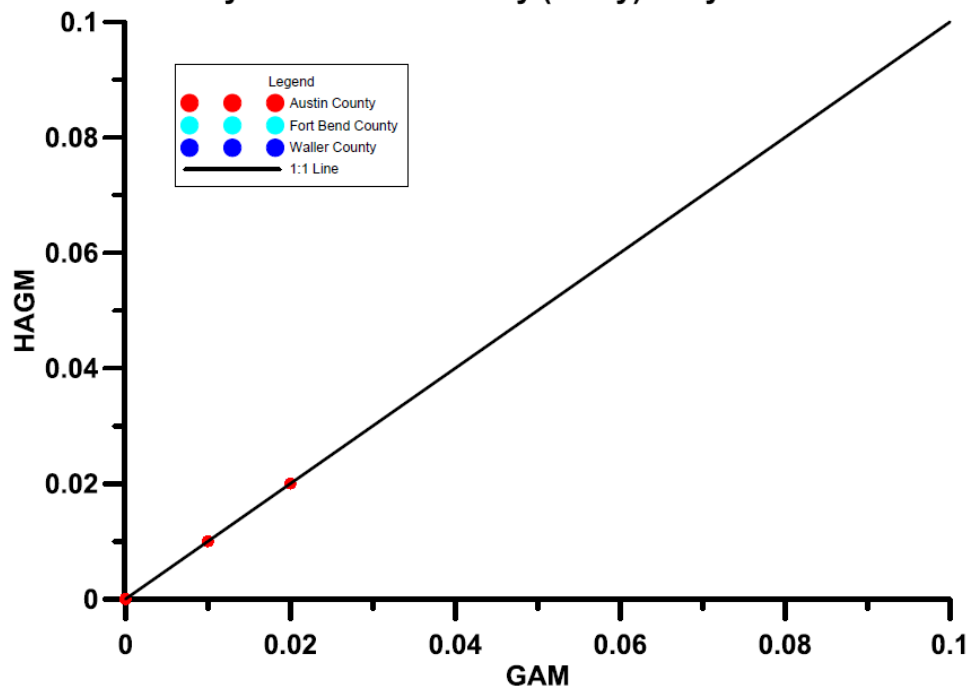


Figure A4
Hydraulic Conductivity (ft/day) - Layer 4

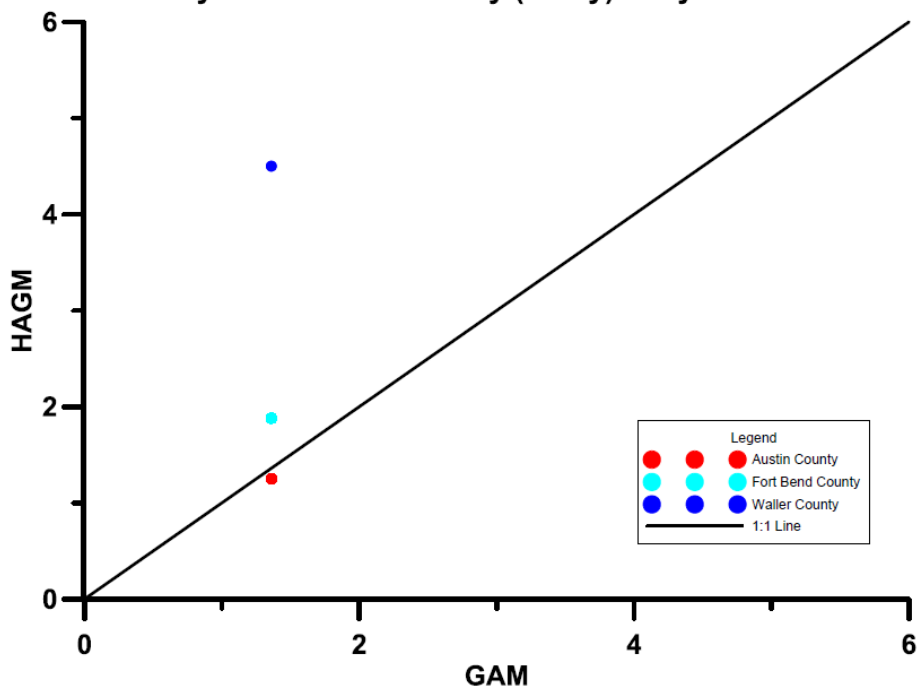


Figure A5
Storativity (dimensionless) - Layer 1

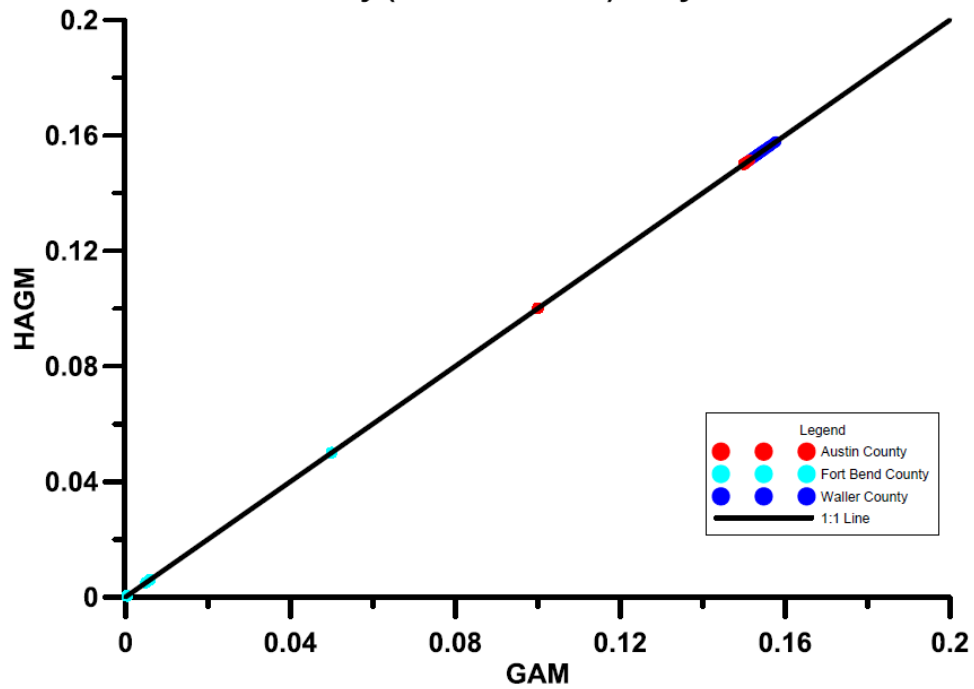


Figure A6
Storativity (dimensionless) - Layer 2

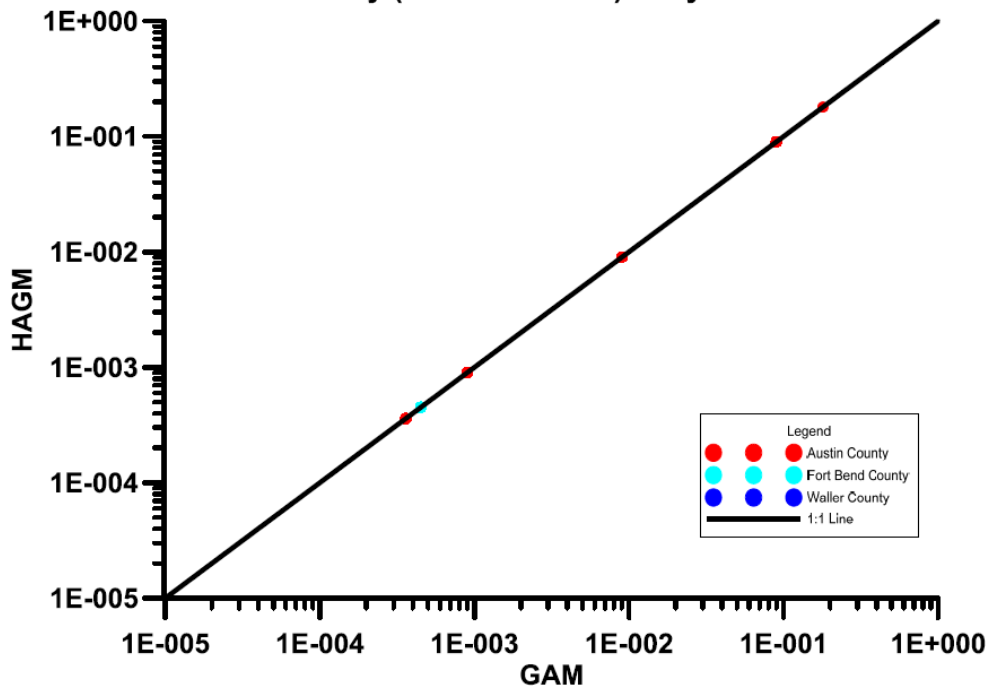


Figure A7
Storativity (dimensionless) - Layer 3

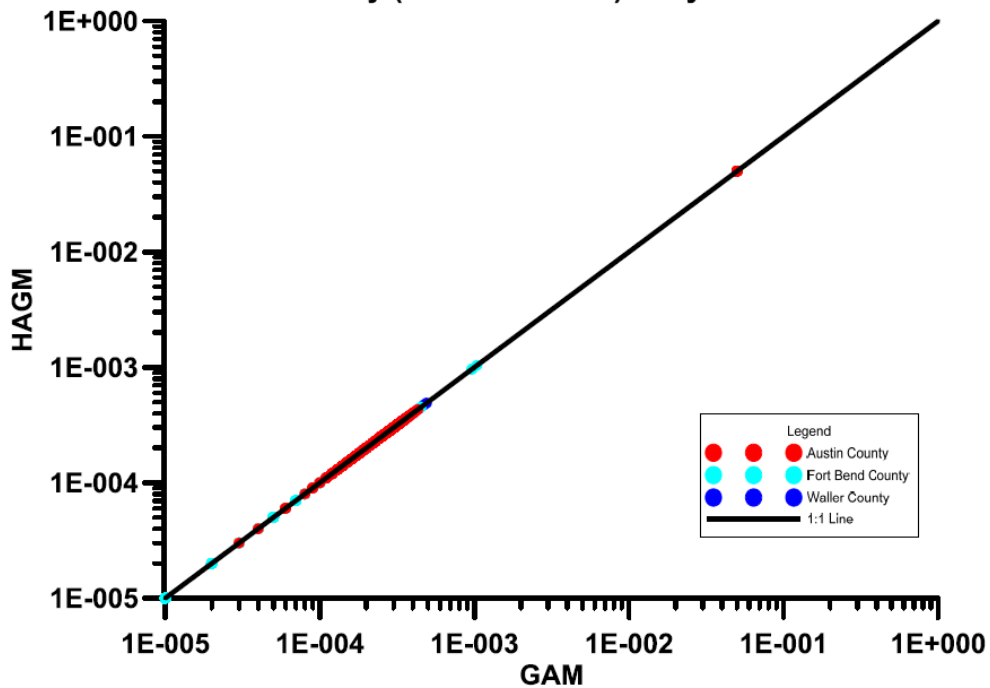


Figure A8
Storativity (dimensionless) - Layer 4

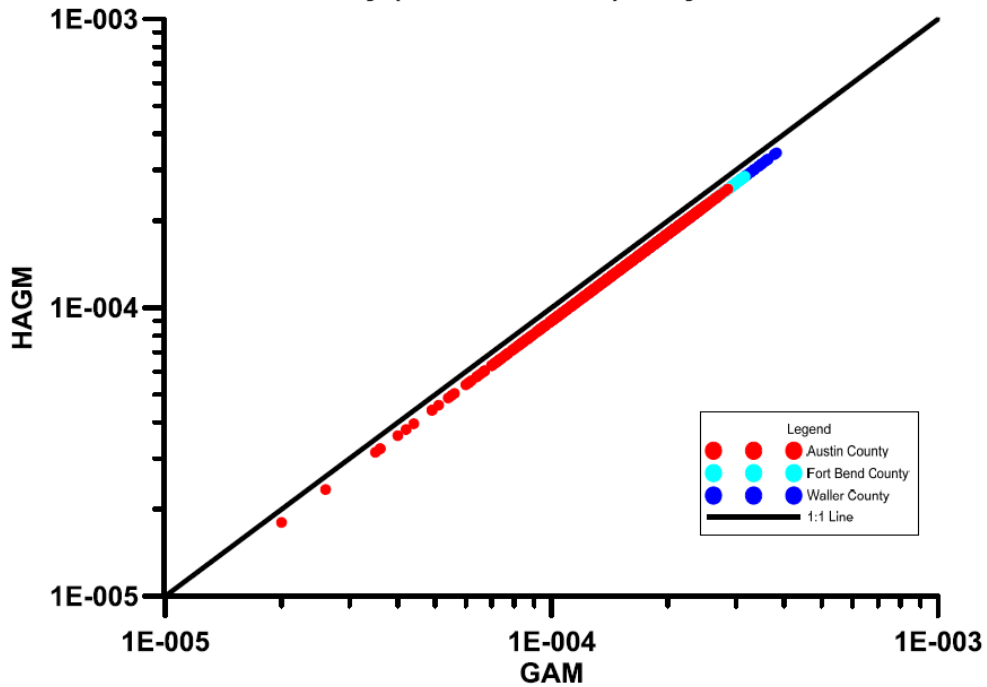


Figure A9
Vertical Leakance between Layers 1 and 2 (day⁻¹)

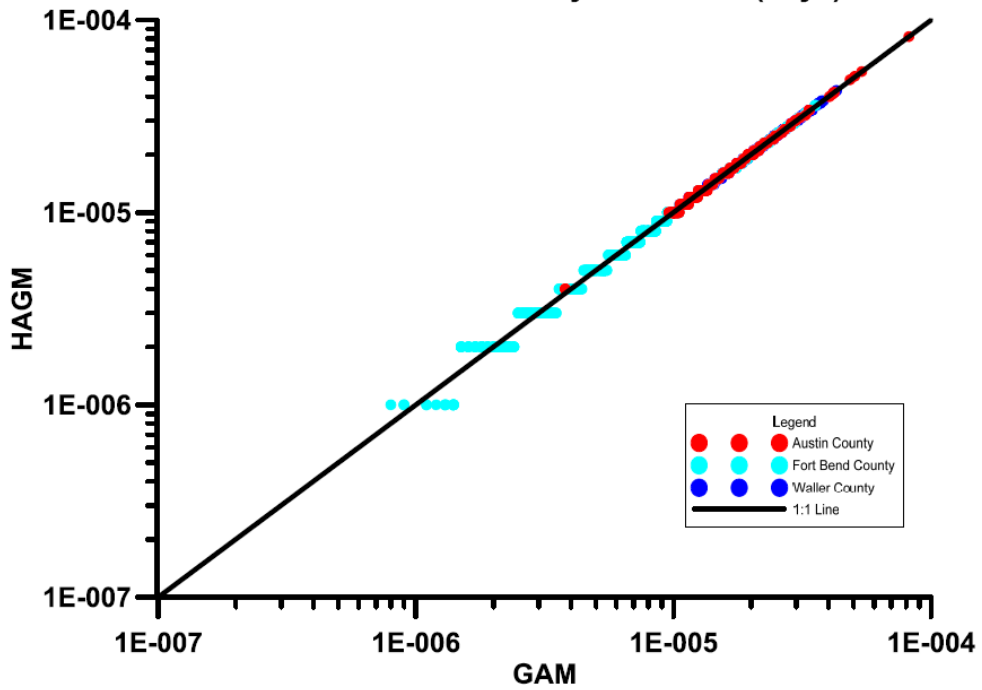


Figure A10
Vertical Leakance between Layers 2 and 3 (day⁻¹)

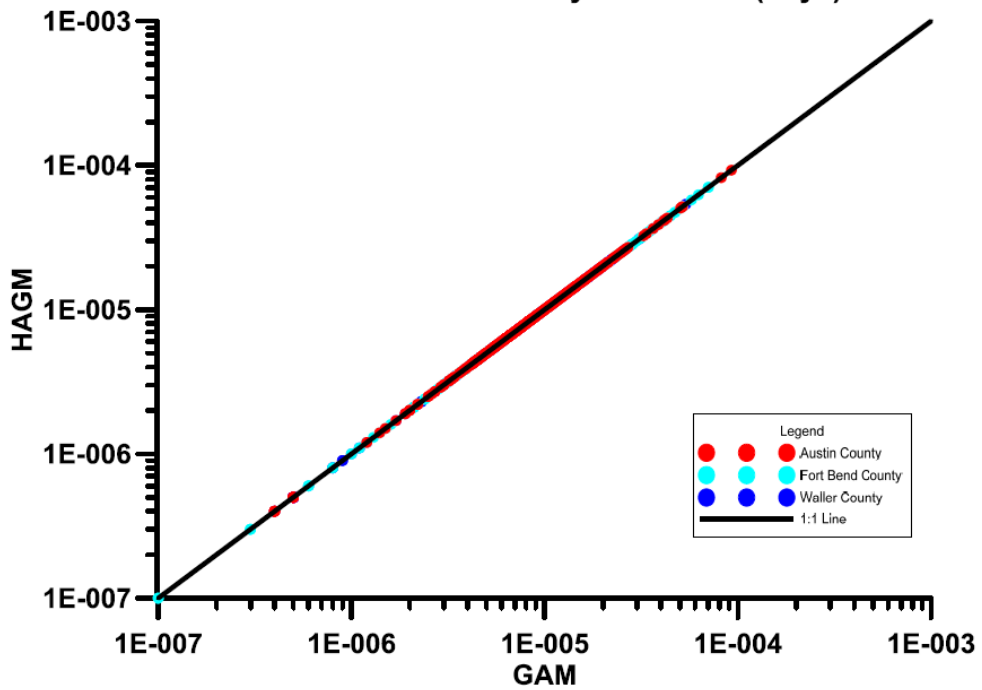


Figure A11
Vertical Leakance between Layers 3 and 4 (day⁻¹)

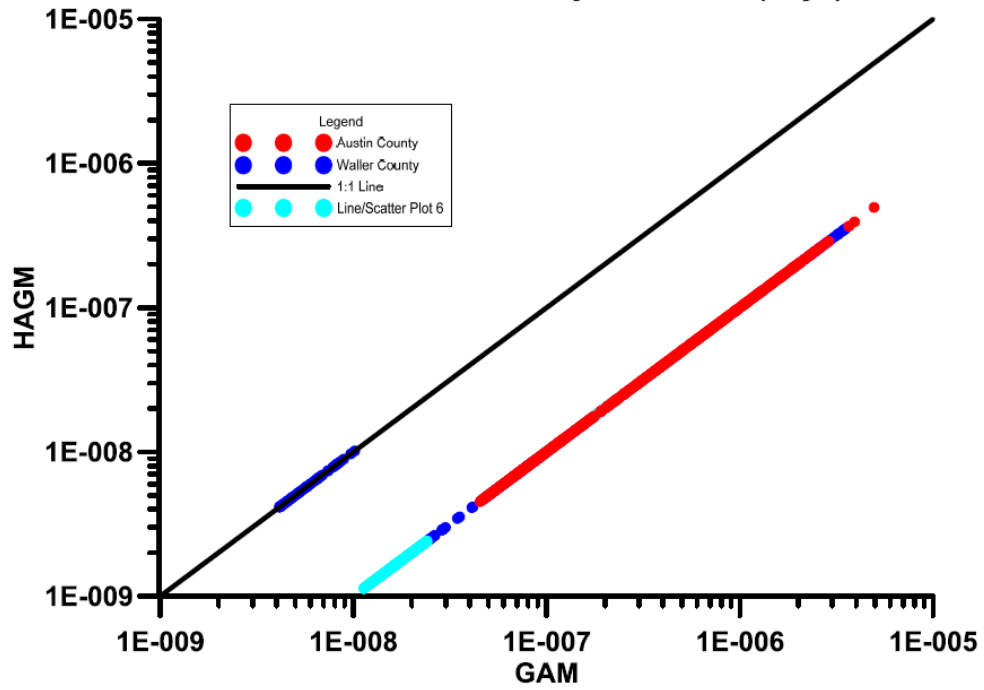


Figure A12
Elastic Storativity (dimensionless) - Layer 1

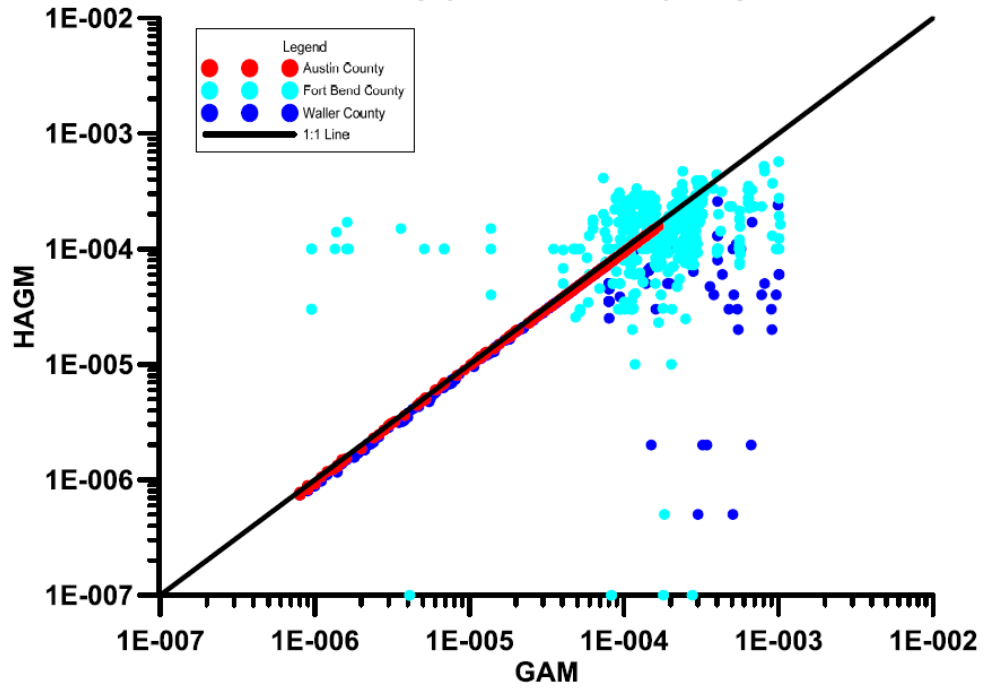
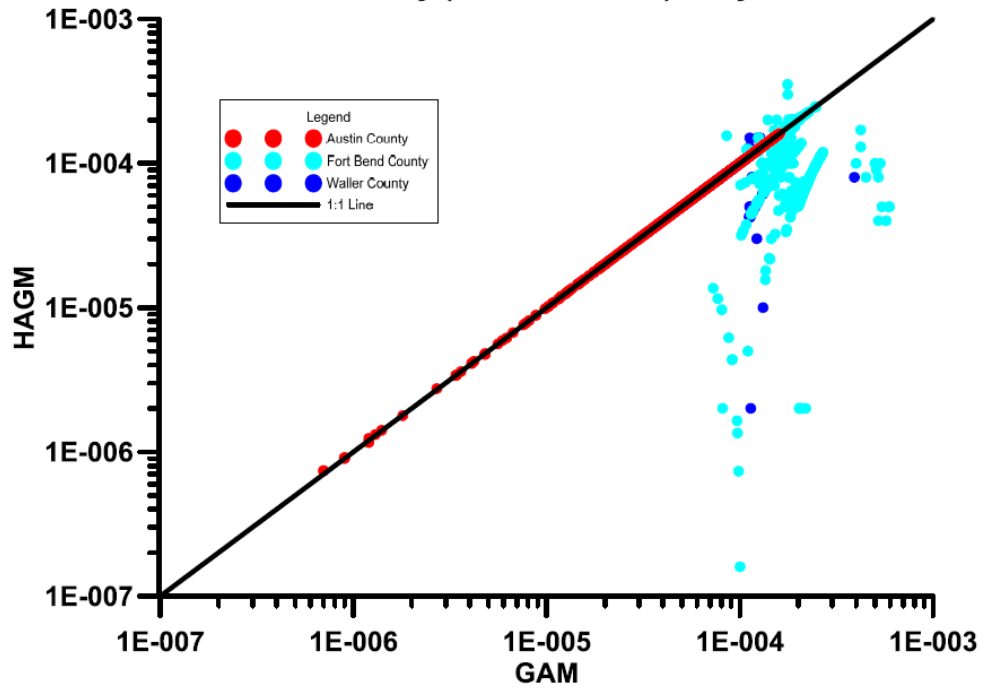


Figure A13
Elastic Storativity (dimensionless) - Layer 2



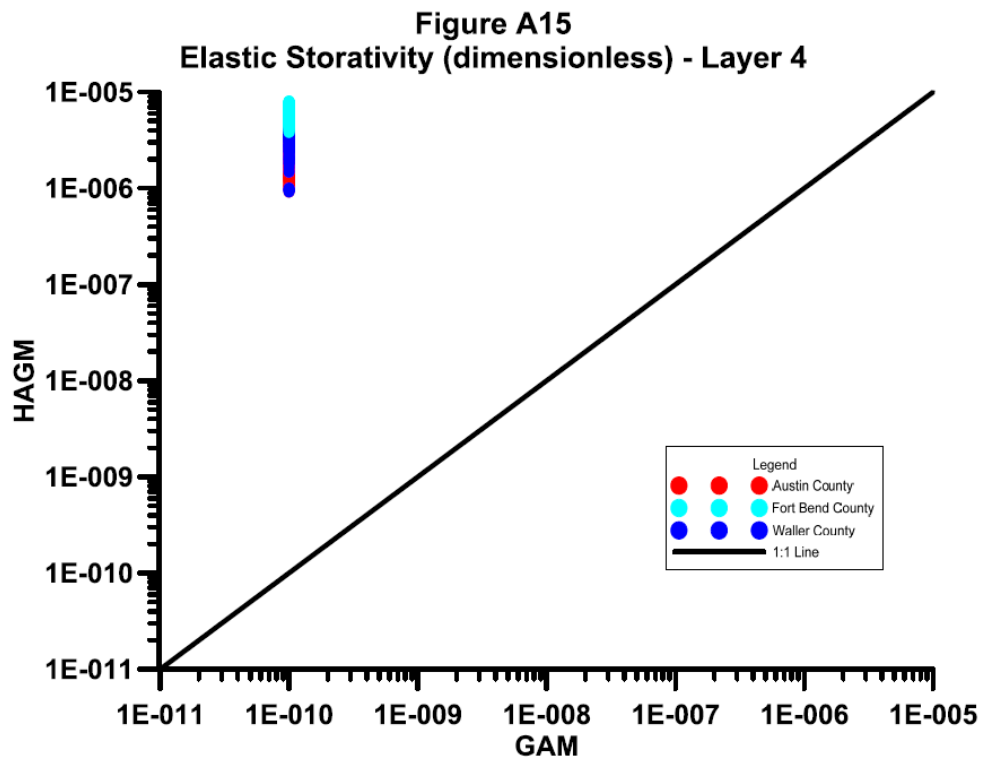
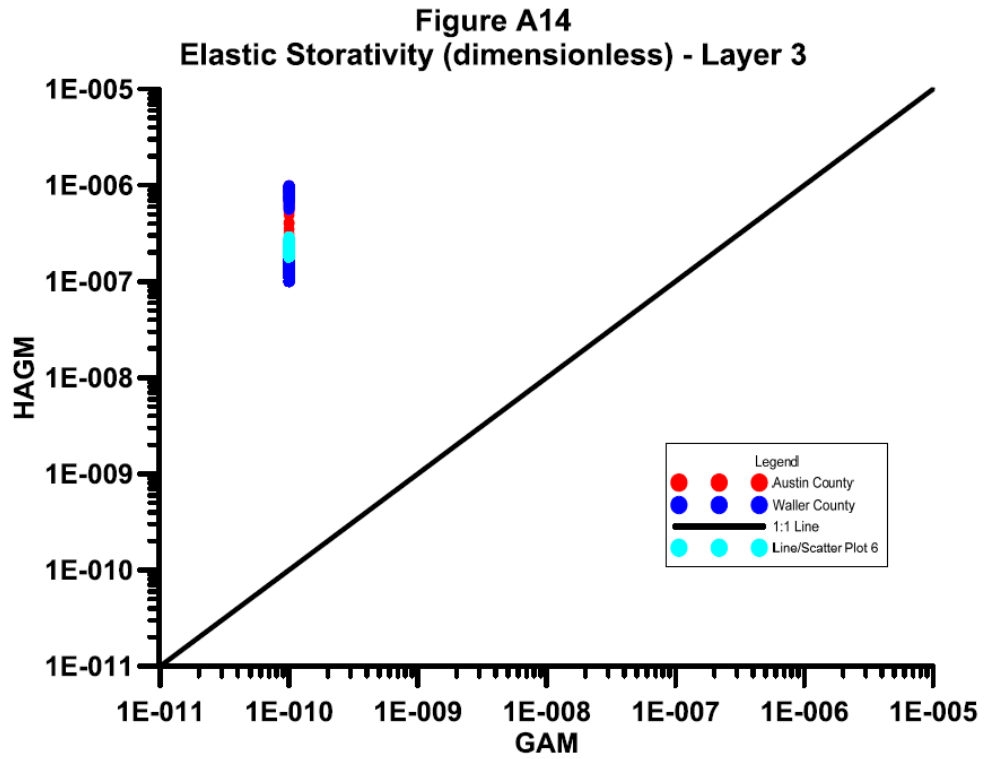


Figure A16
Inelastic Storativity (dimensionless) - Layer 1

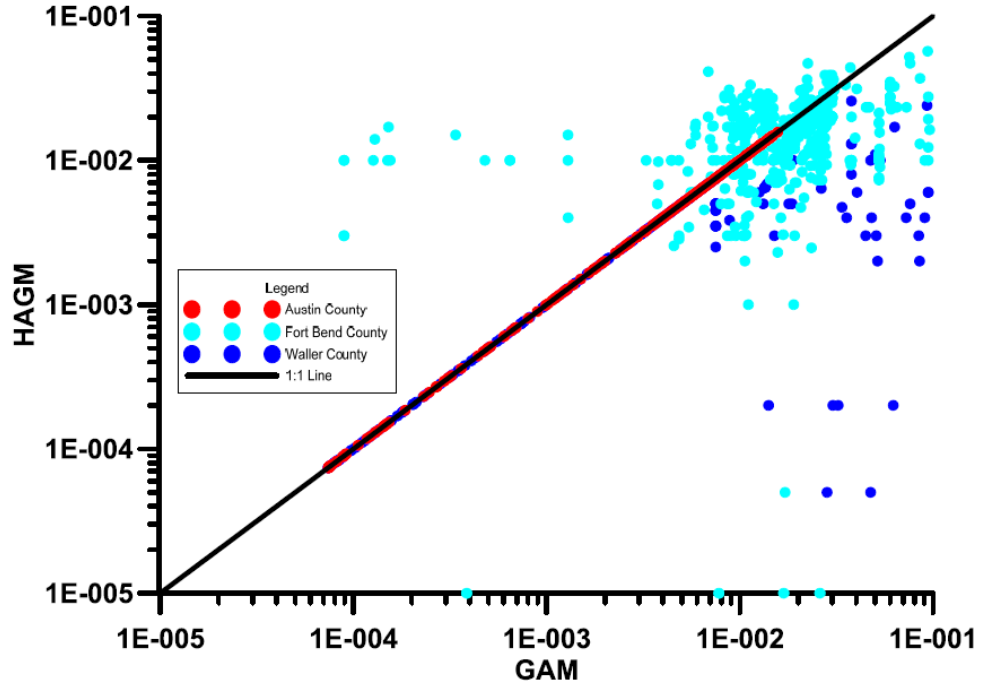
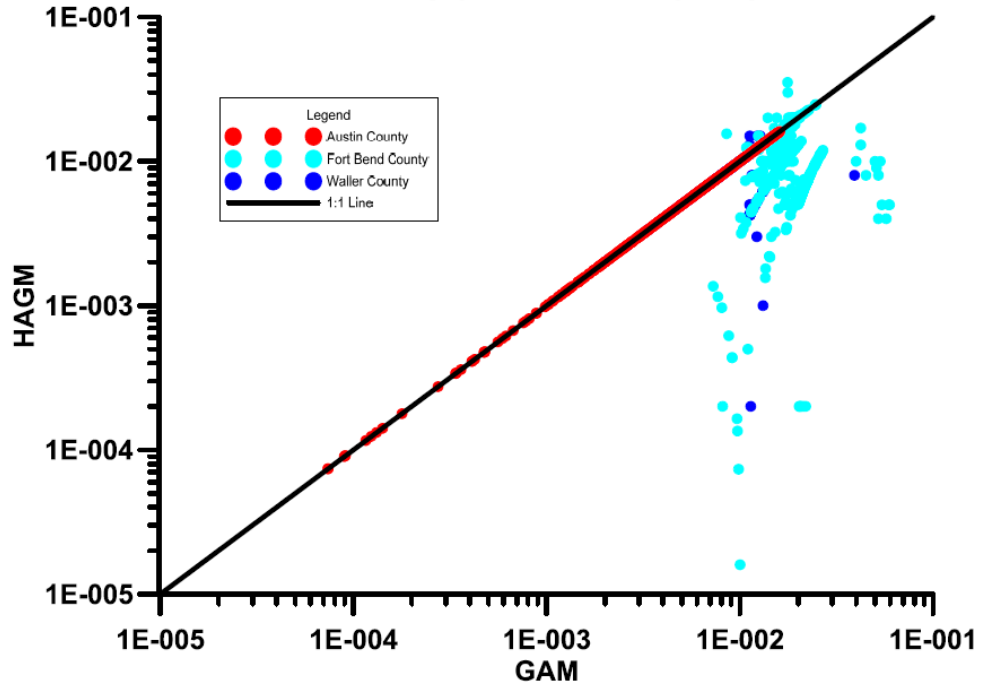


Figure A17
Inelastic Storativity (dimensionless) - Layer 2



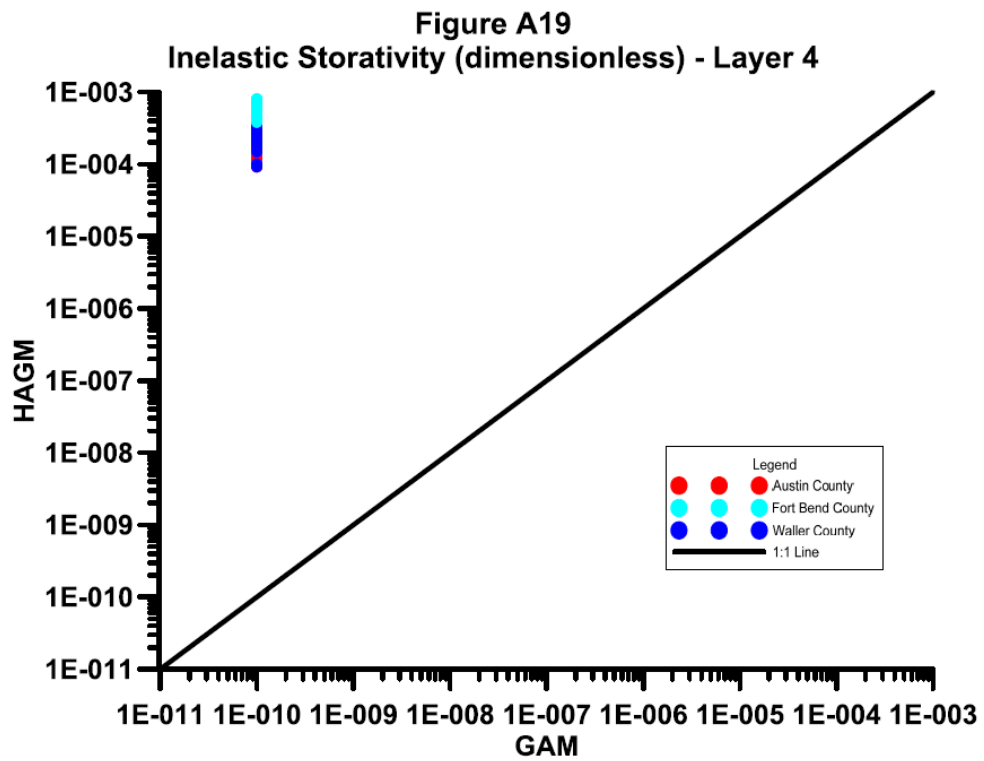
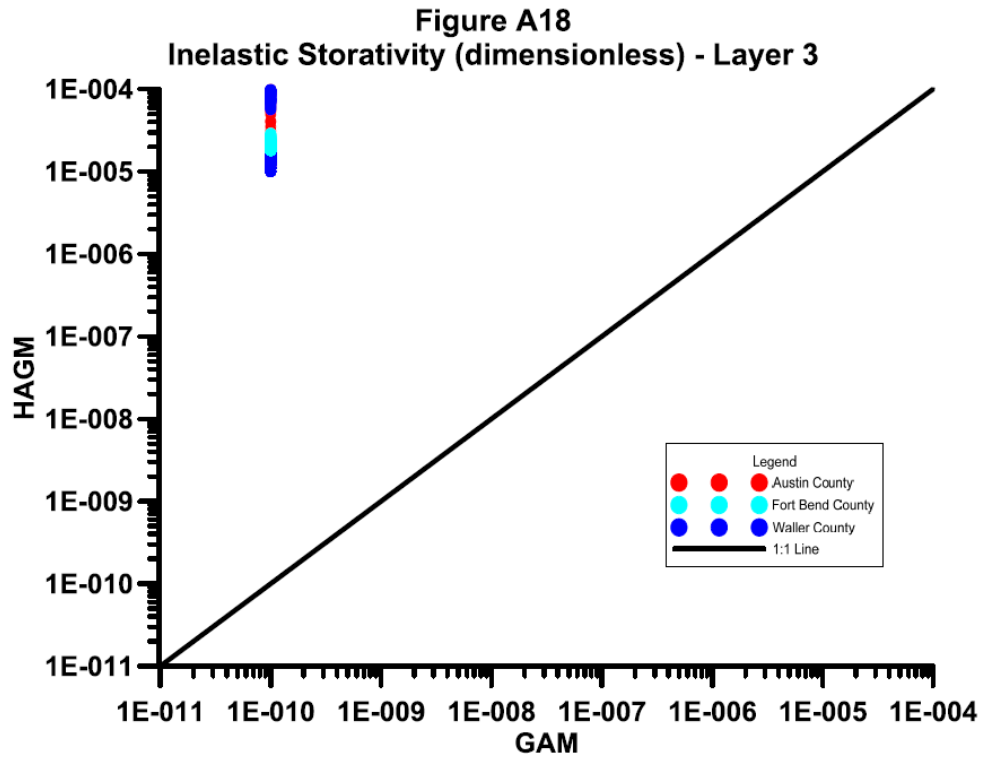


Figure A20
Austin County Pumping - Chicot

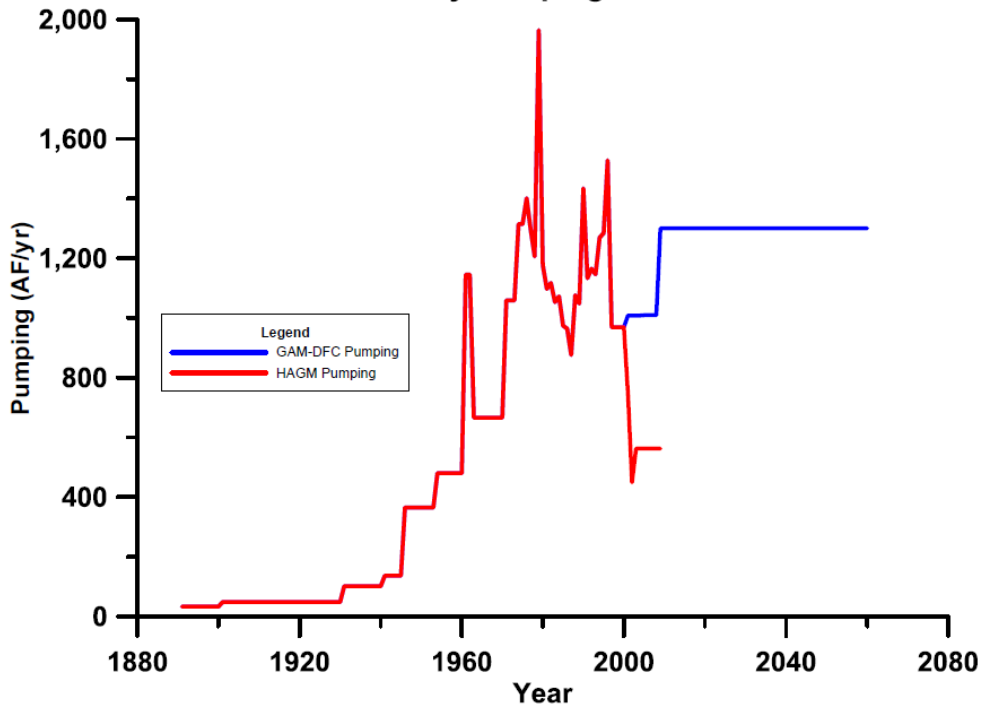


Figure A21
Austin County Pumping - Evangeline

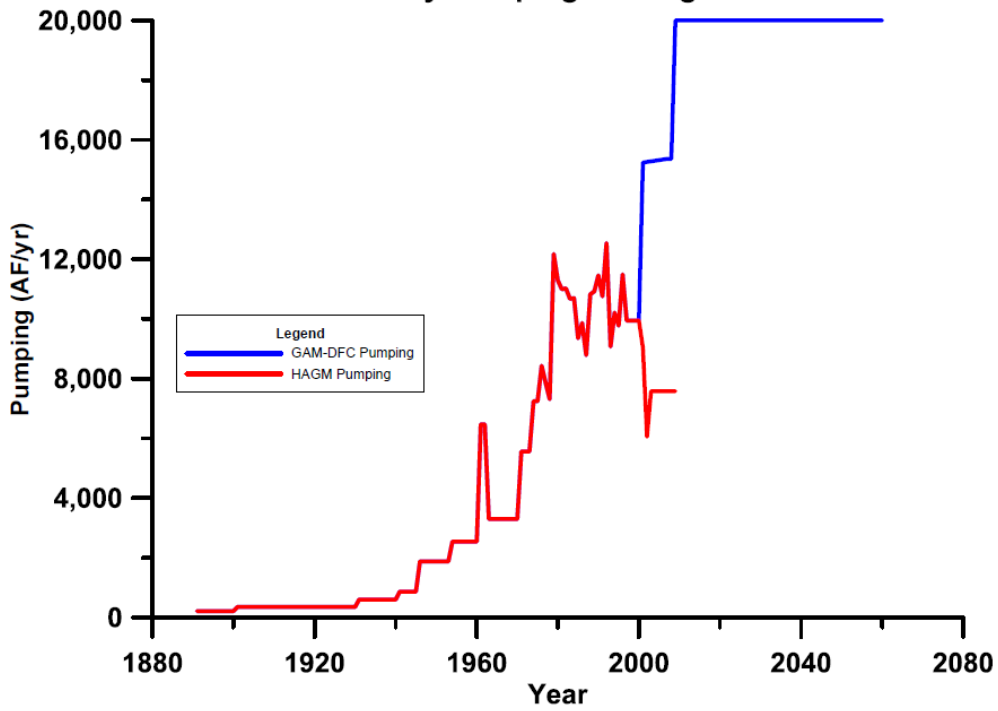


Figure A22
Austin County Pumping - Burkeville

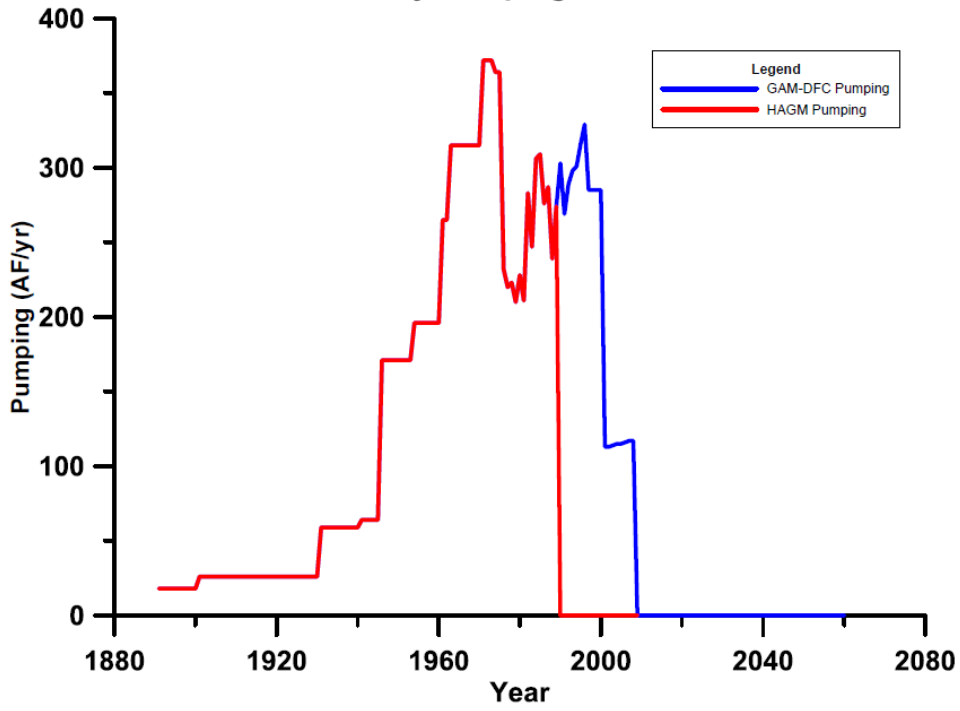


Figure A23
Austin County Pumping - Jasper

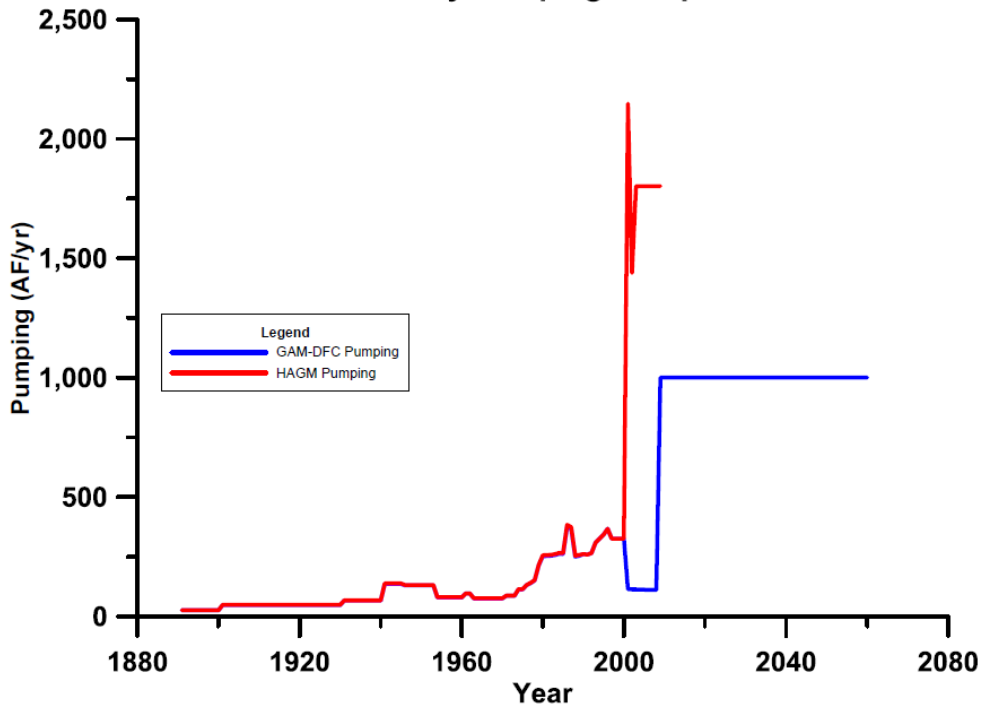


Figure A24
Austin County Total Pumping

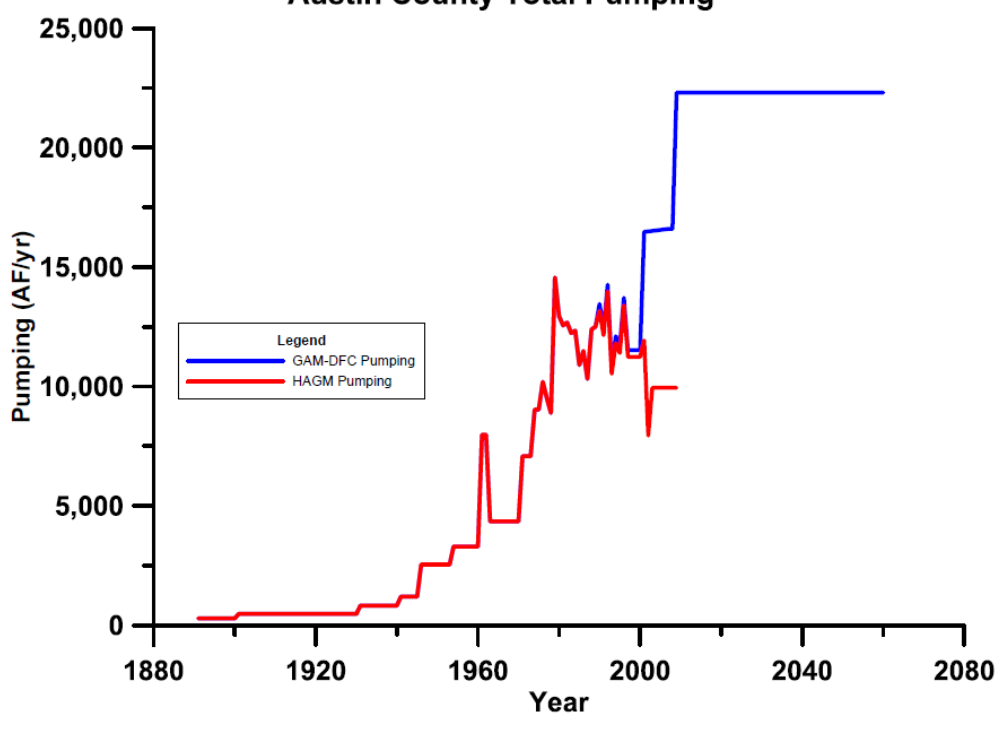


Figure A25
Fort Bend County Pumping - Chicot

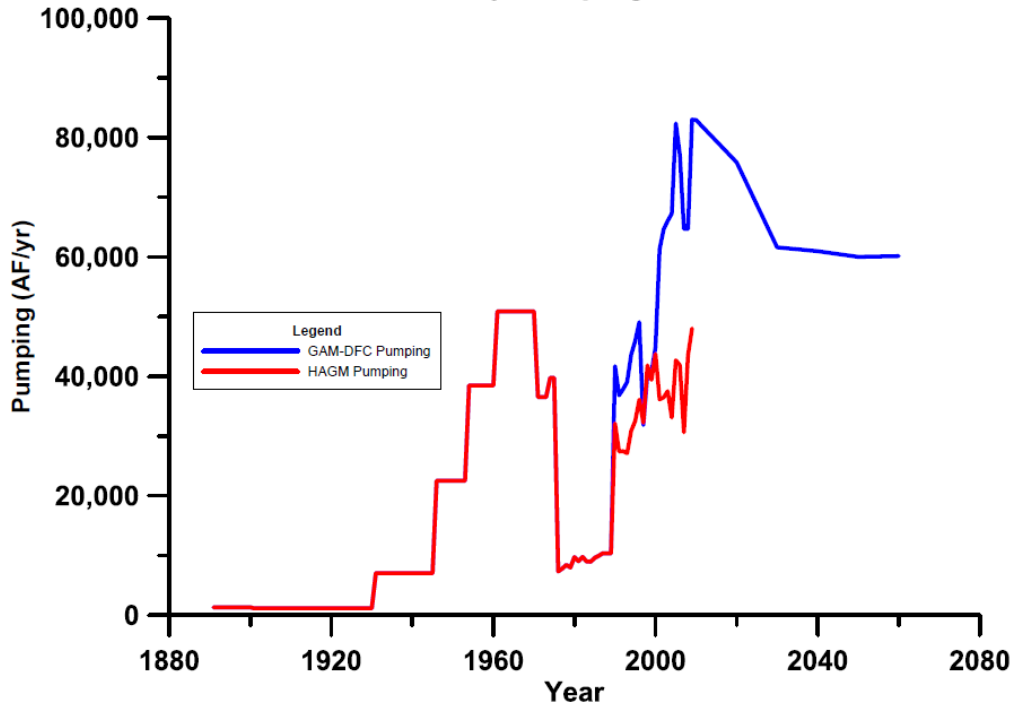


Figure A26
Fort Bend County Pumping - Evangeline

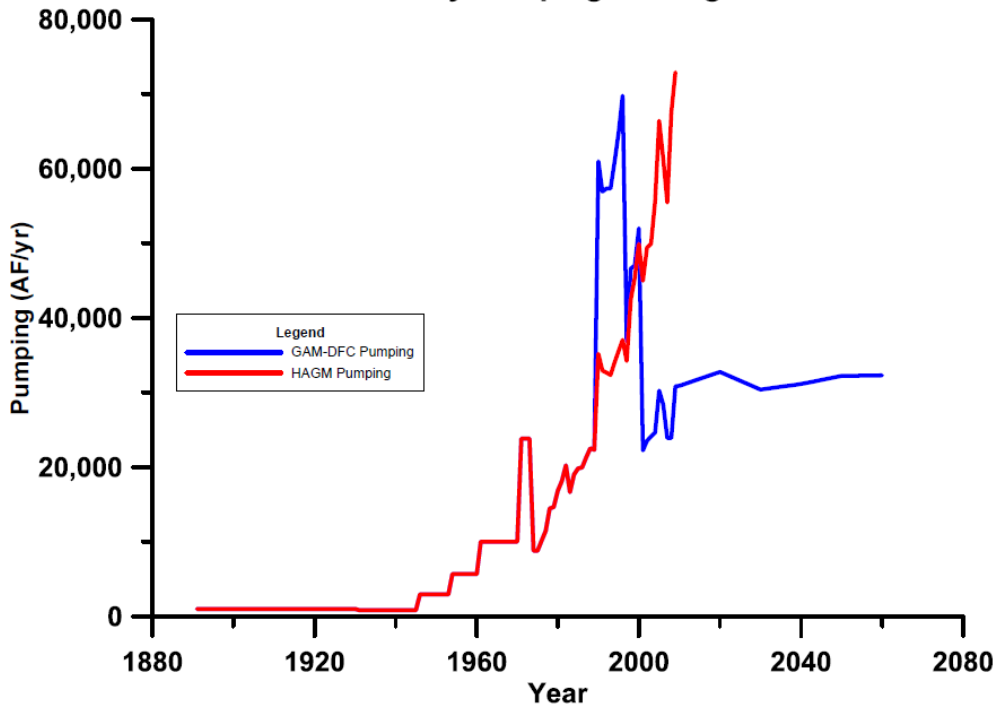


Figure A27
Fort Bend County Pumping - Burkeville

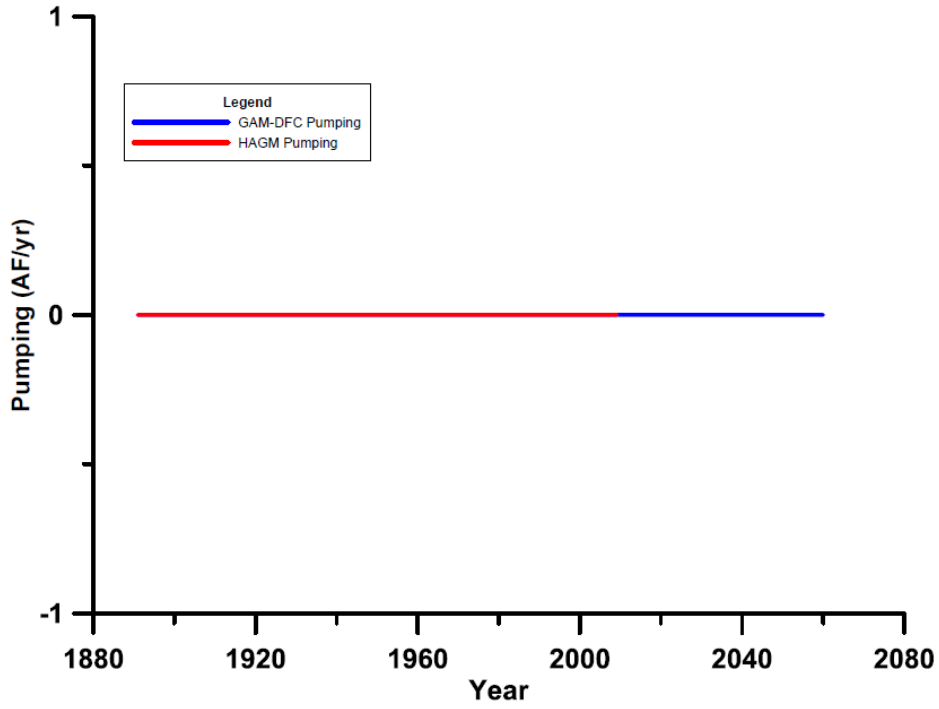


Figure A28
Fort Bend County Pumping - Jasper

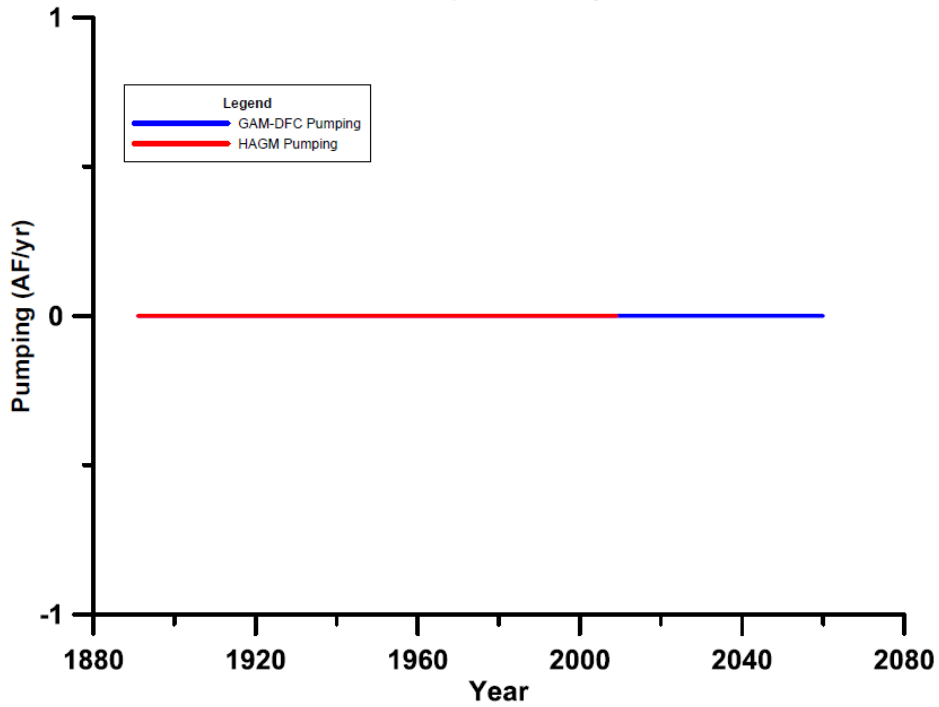


Figure A29
Fort Bend County Total Pumping

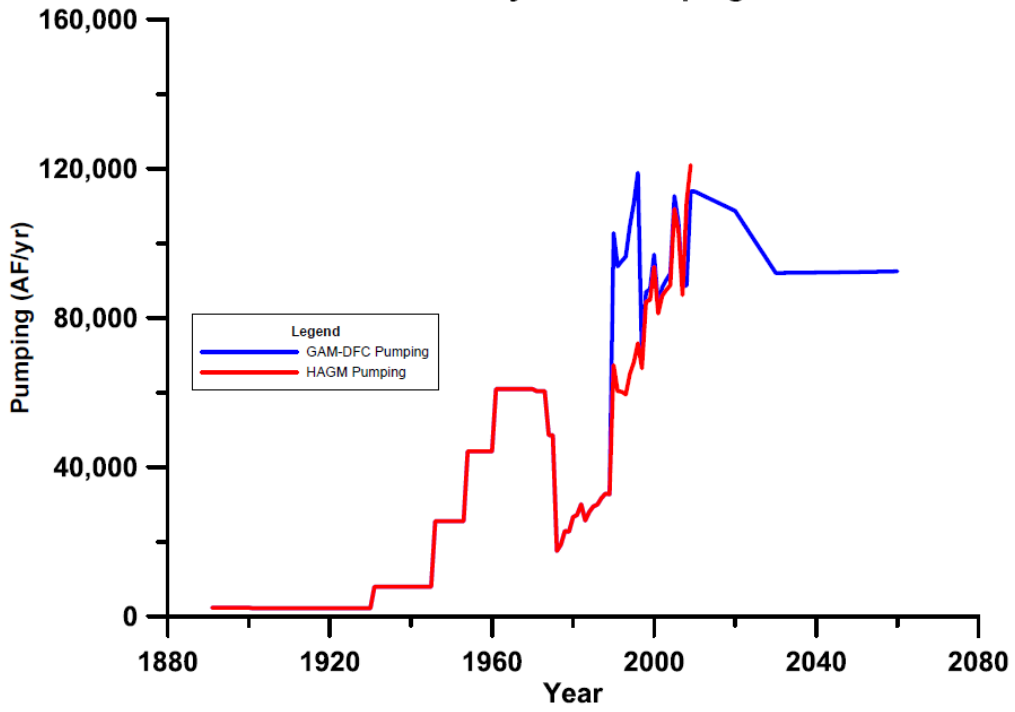


Figure A30
Waller County Pumping - Chicot

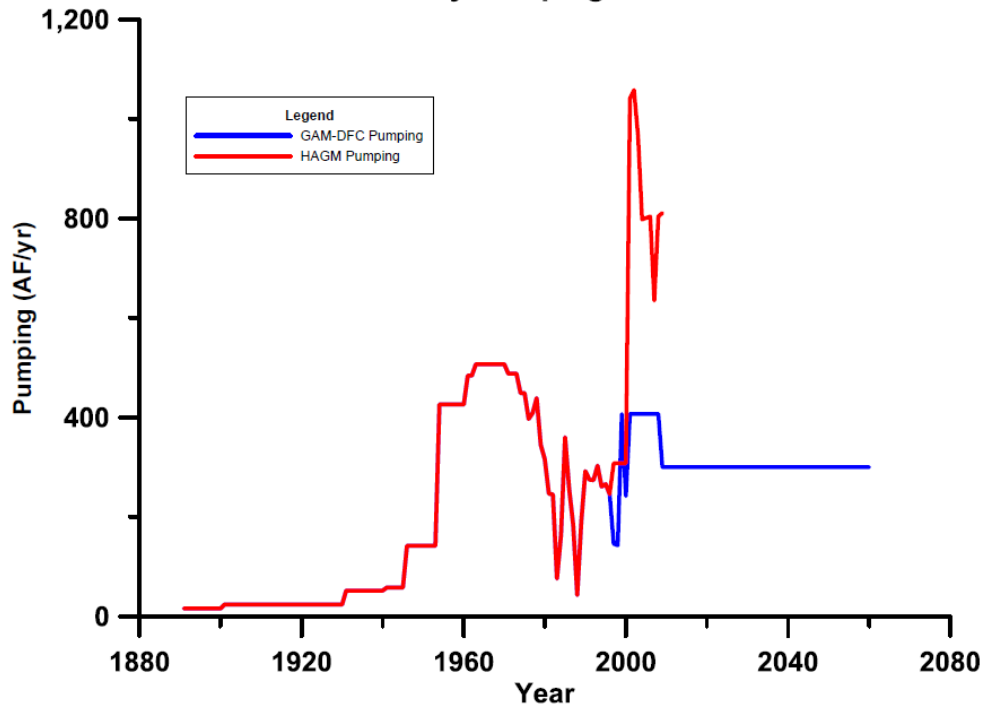


Figure A31
Waller County Pumping - Evangeline

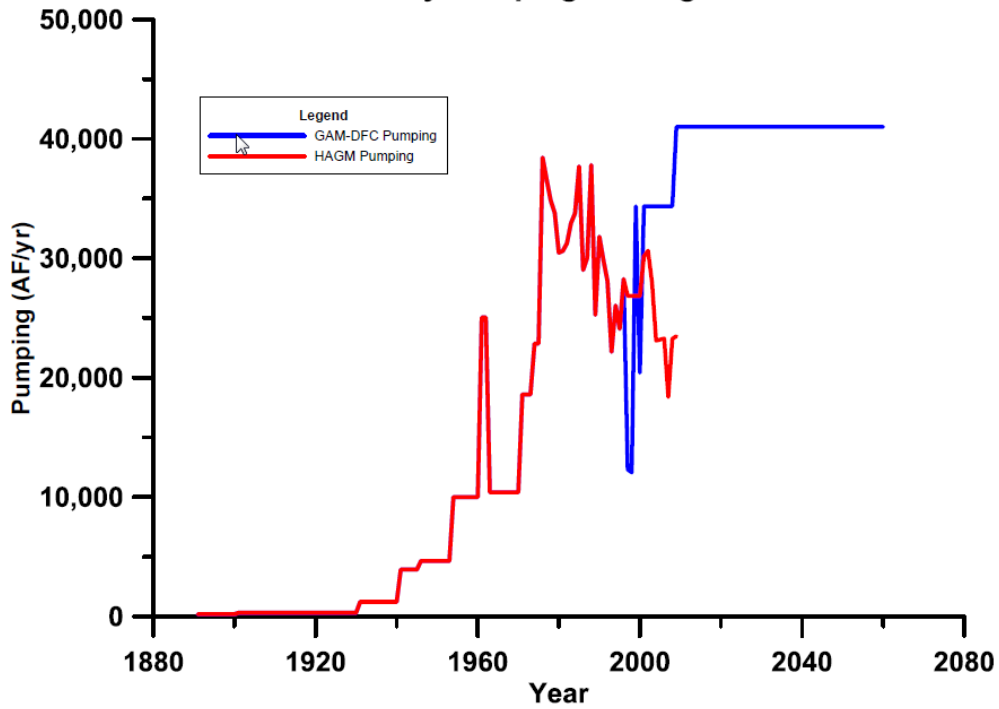


Figure A32
Waller County Pumping - Burkeville

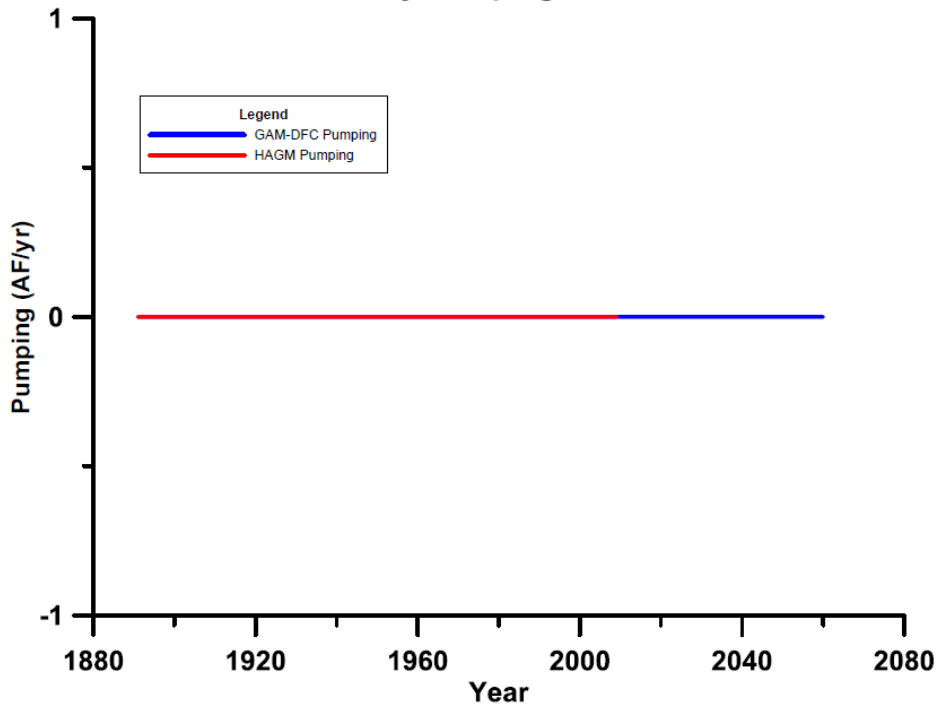


Figure A33
Waller County Pumping - Jasper

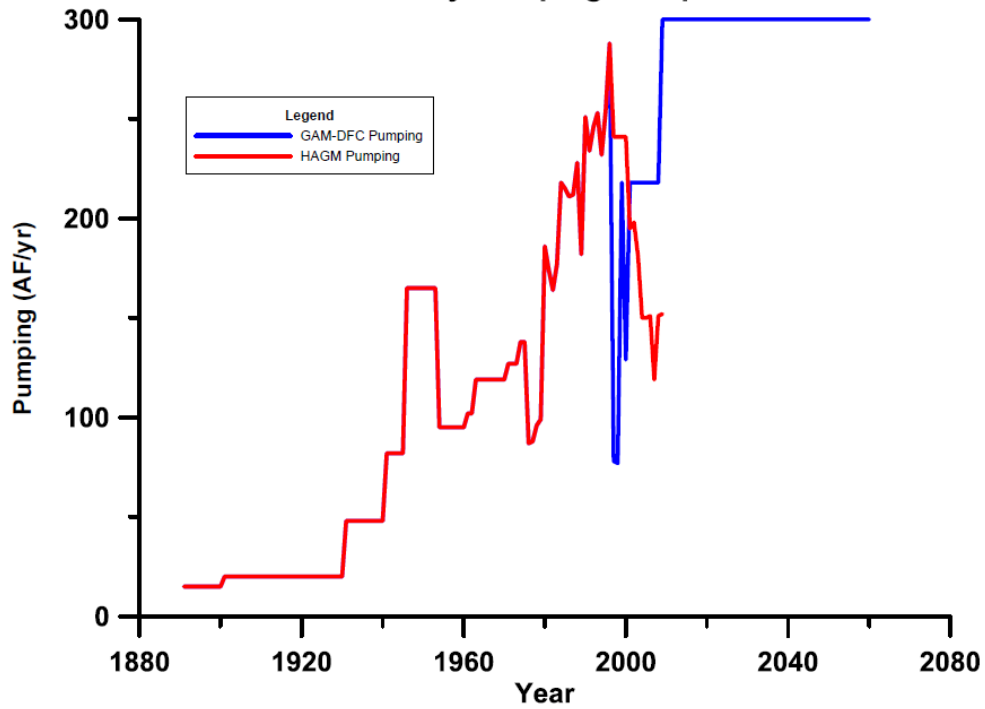


Figure A34
Waller County Total Pumping

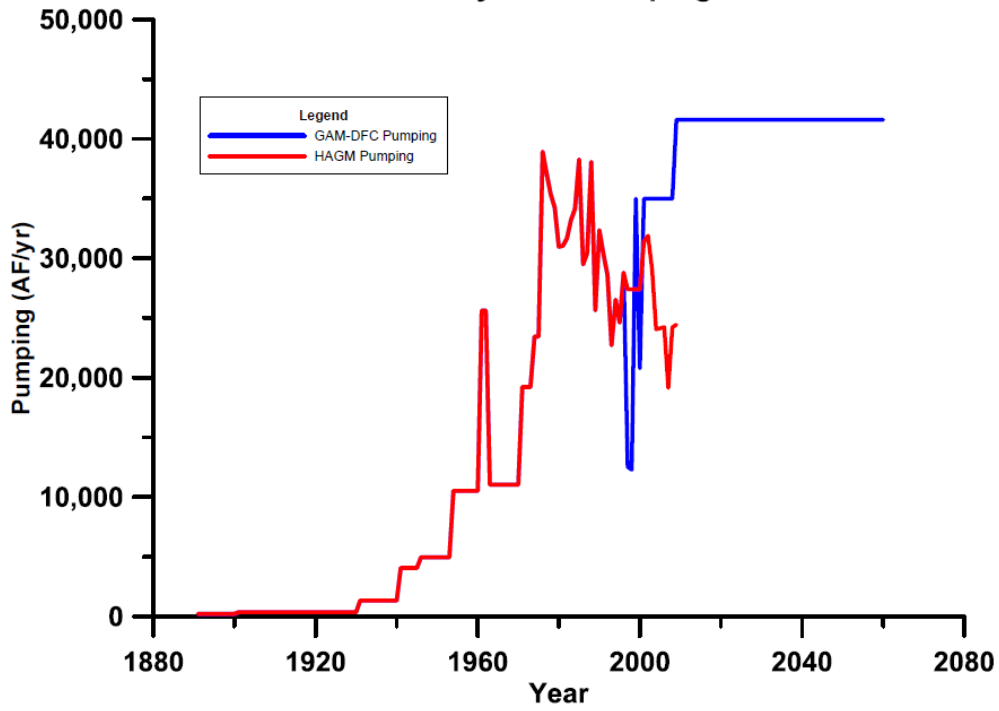


Figure A35
Layer Top Elevation vs. GHB Elevation
Austin County

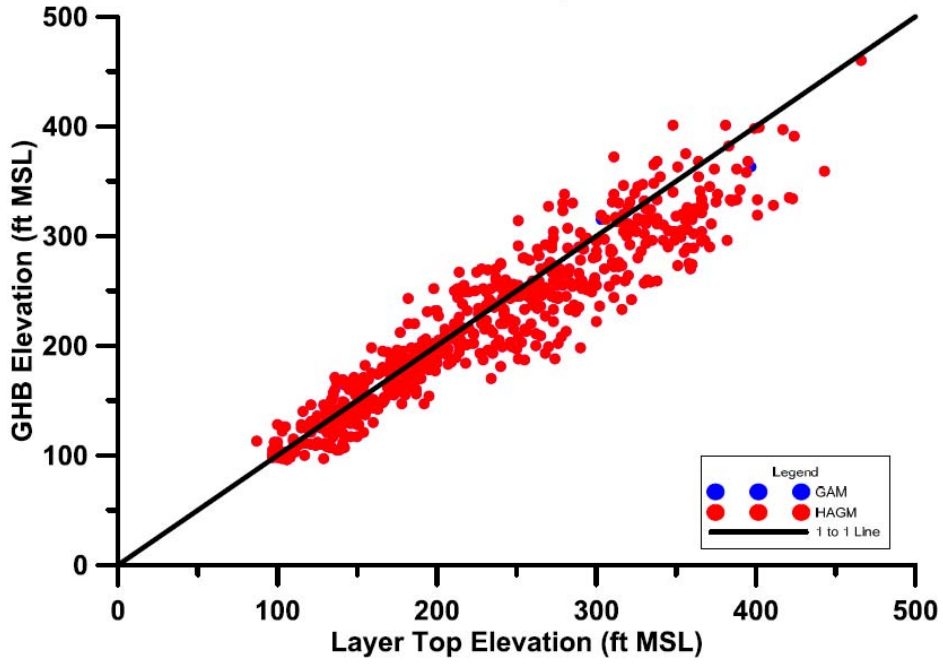


Figure A36
Layer Top Elevation vs. GHB Elevation
Fort Bend County

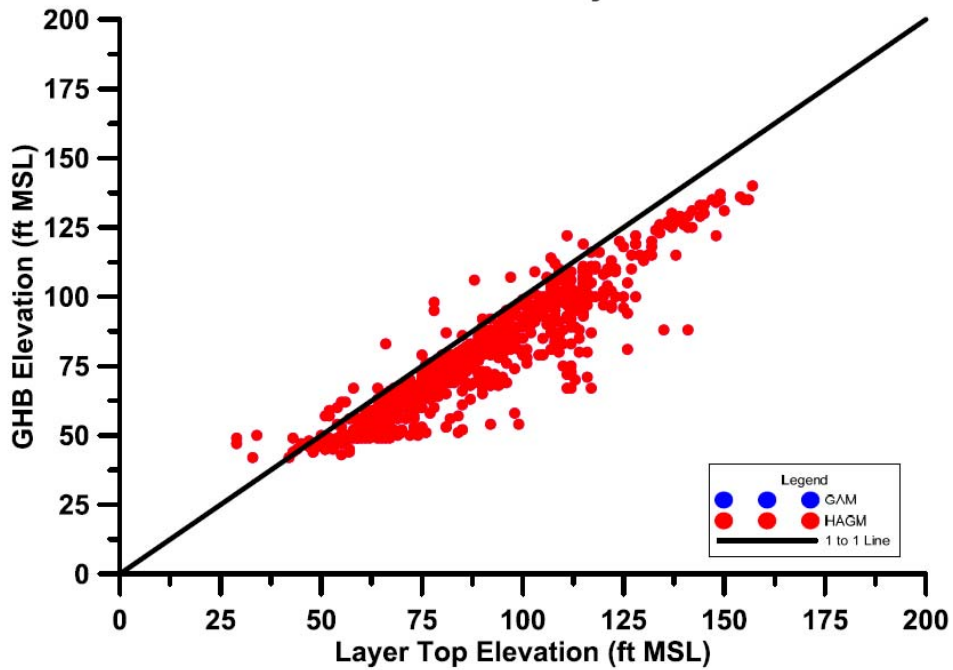


Figure A37
Layer Top Elevation vs. GHB Elevation
Waller County

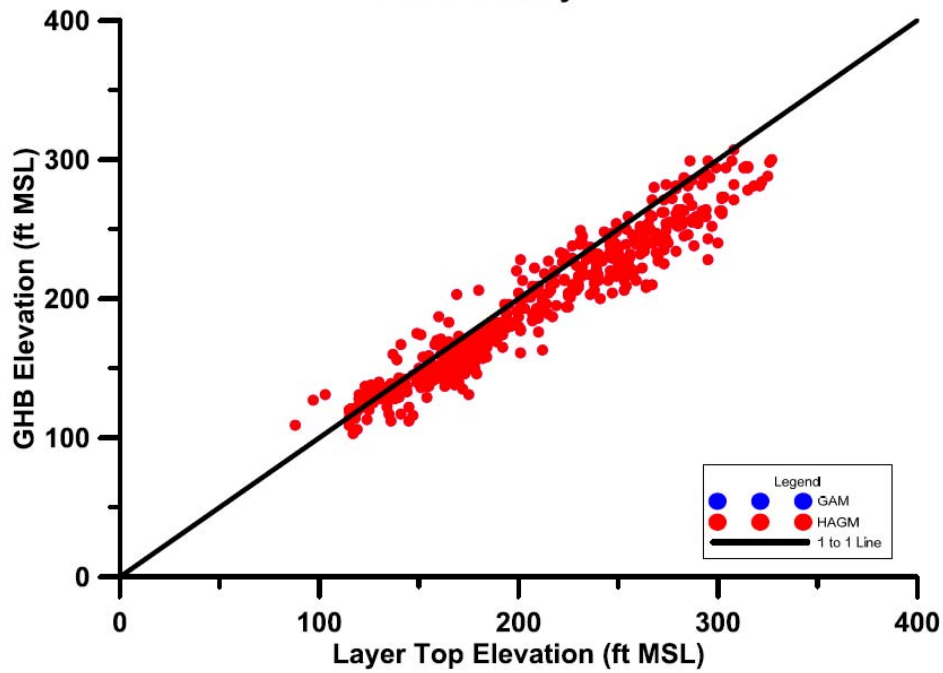


Figure A38
Distribution of Differences in Elevation and GHB Head
Austin County

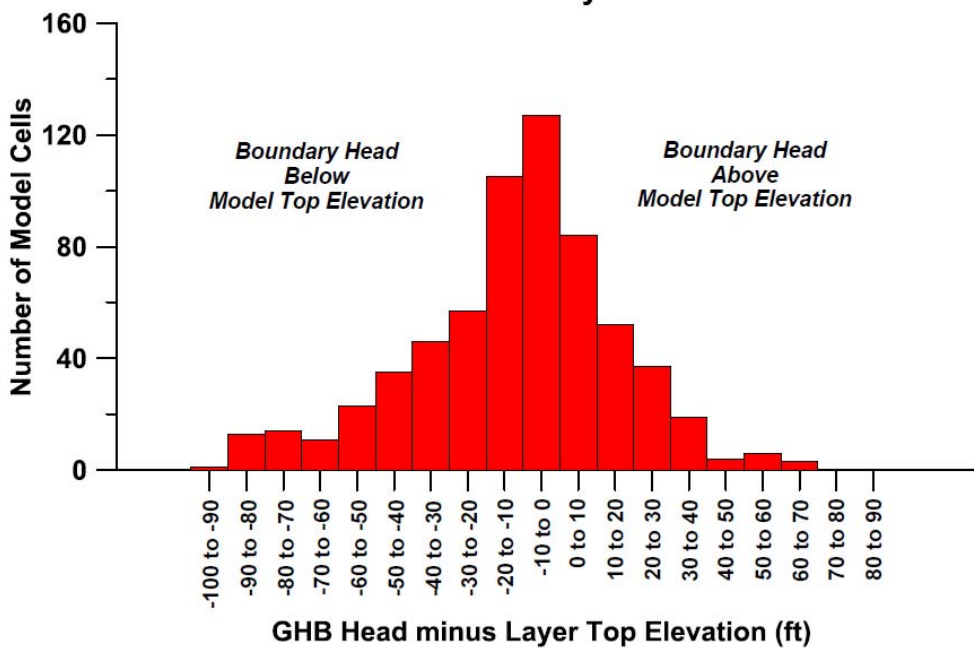


Figure A39
Distribution of Differences in Elevation and GHB Head
Fort Bend County

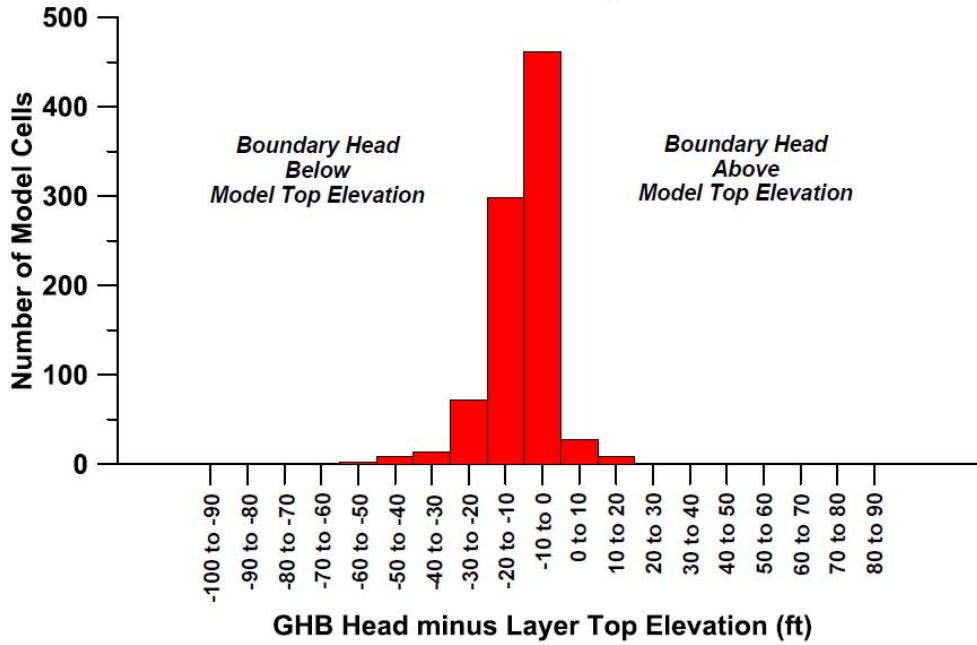
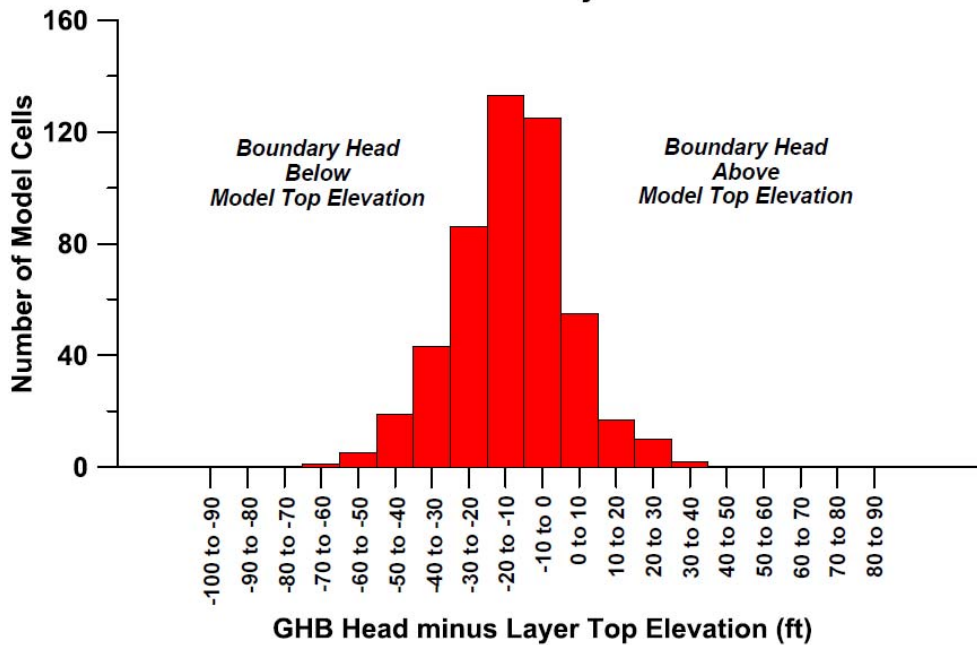


Figure A40
Distribution of Differences in Elevation and GHB Head
Waller County



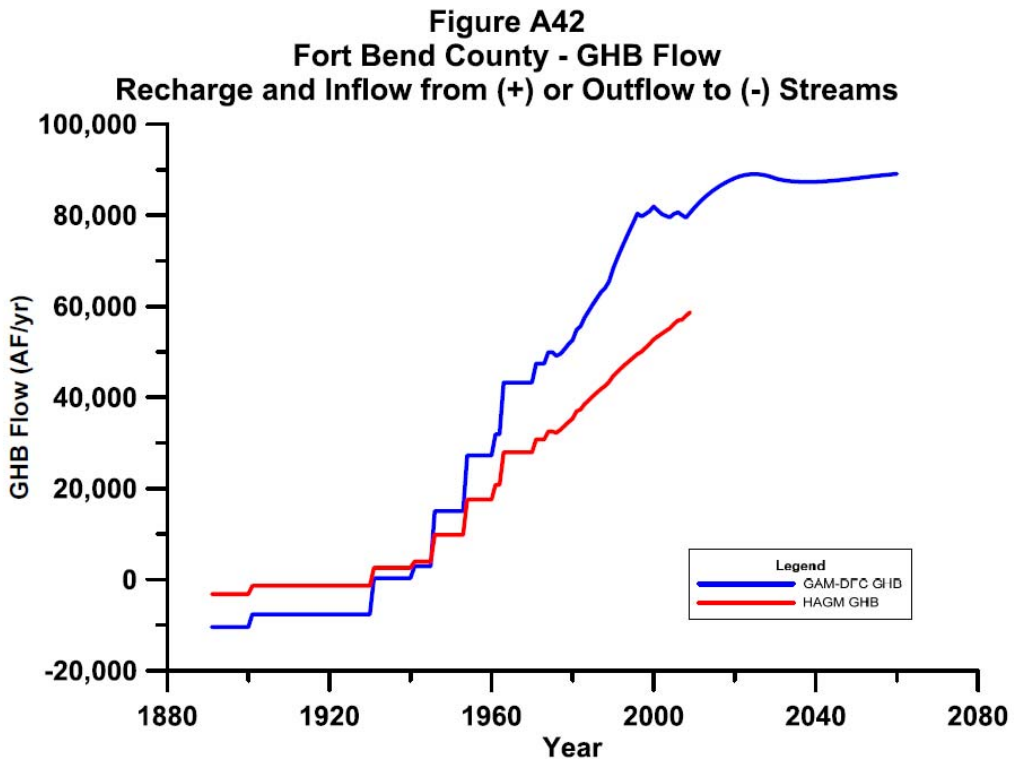
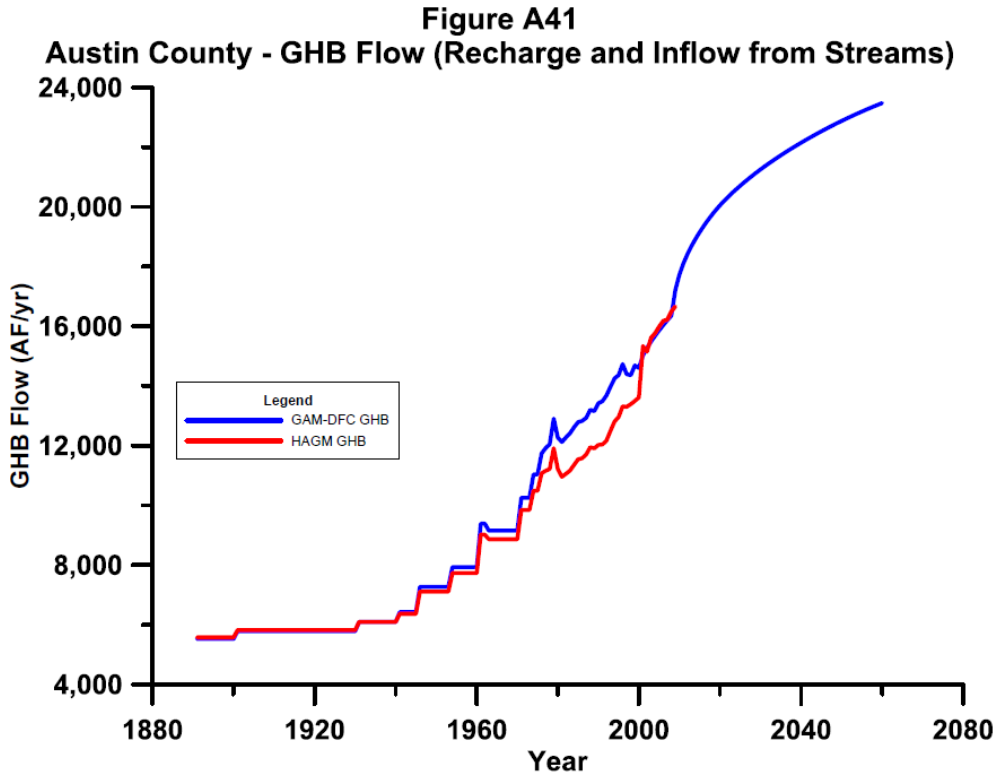


Figure A43
Waller County - GHB Flows (Recharge and Inflow from Streams)

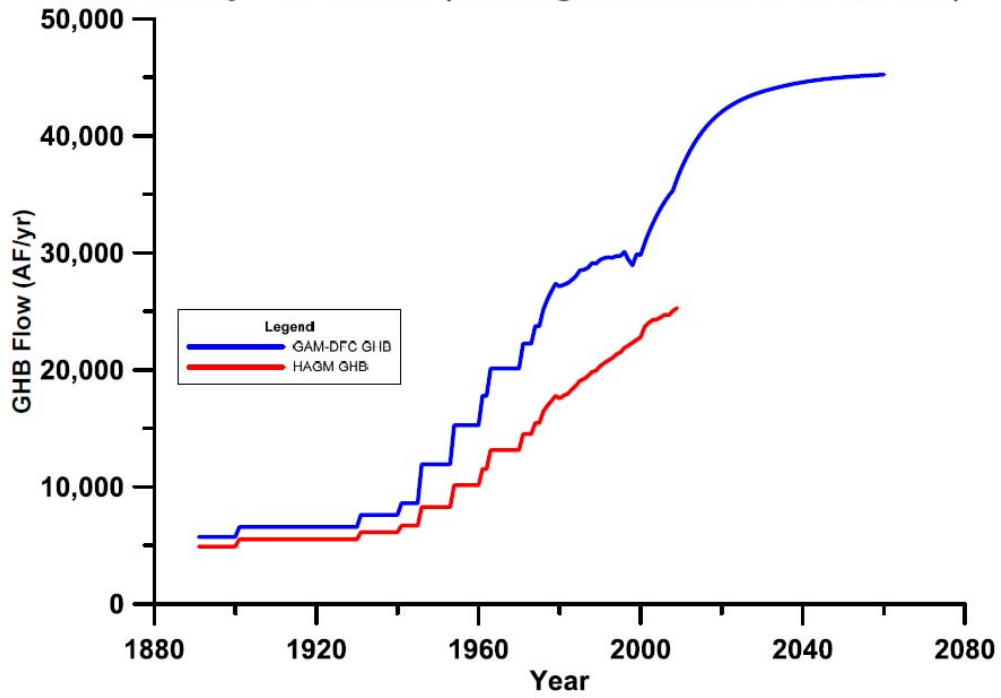


Figure A44
Austin County Pumping vs. GHB Flows

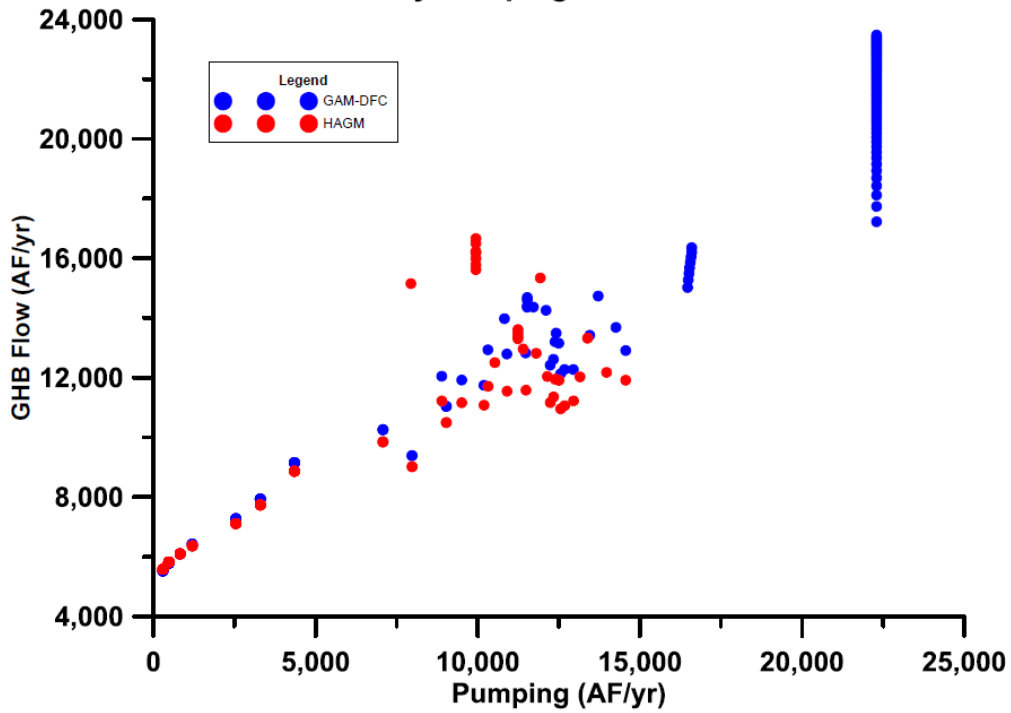


Figure A45
Fort Bend County Pumping vs. GHB Flows

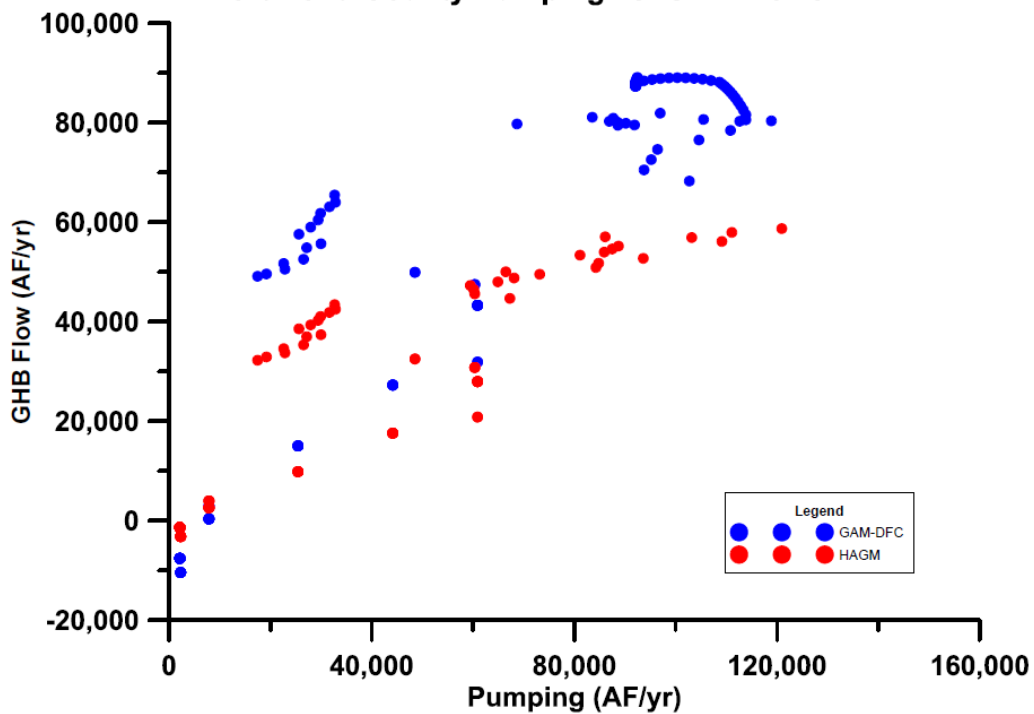
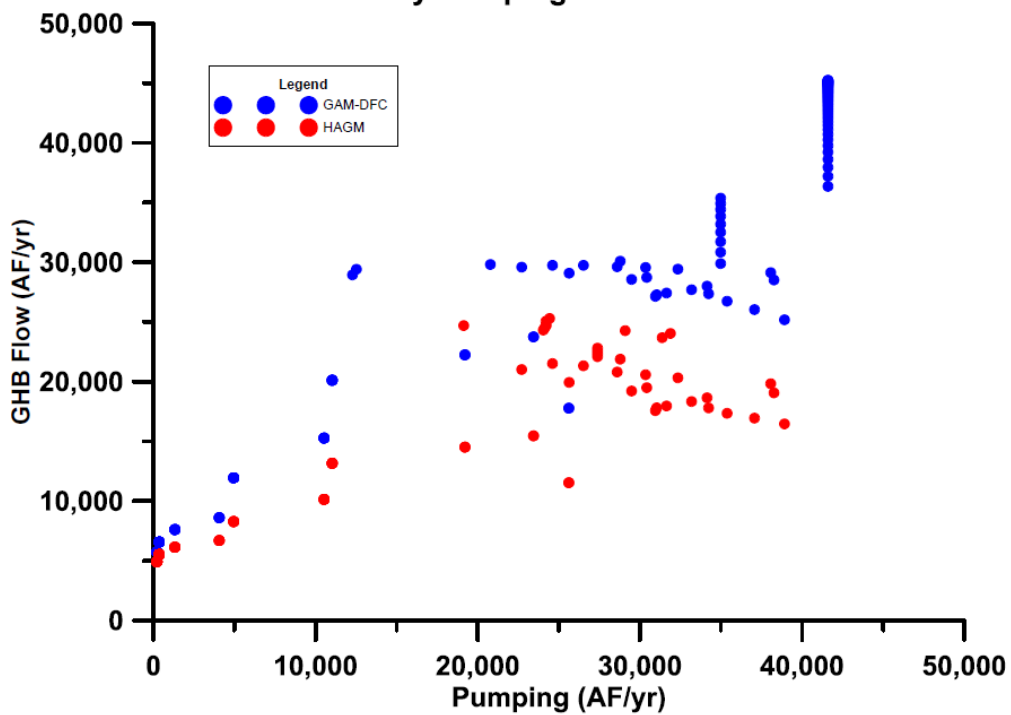
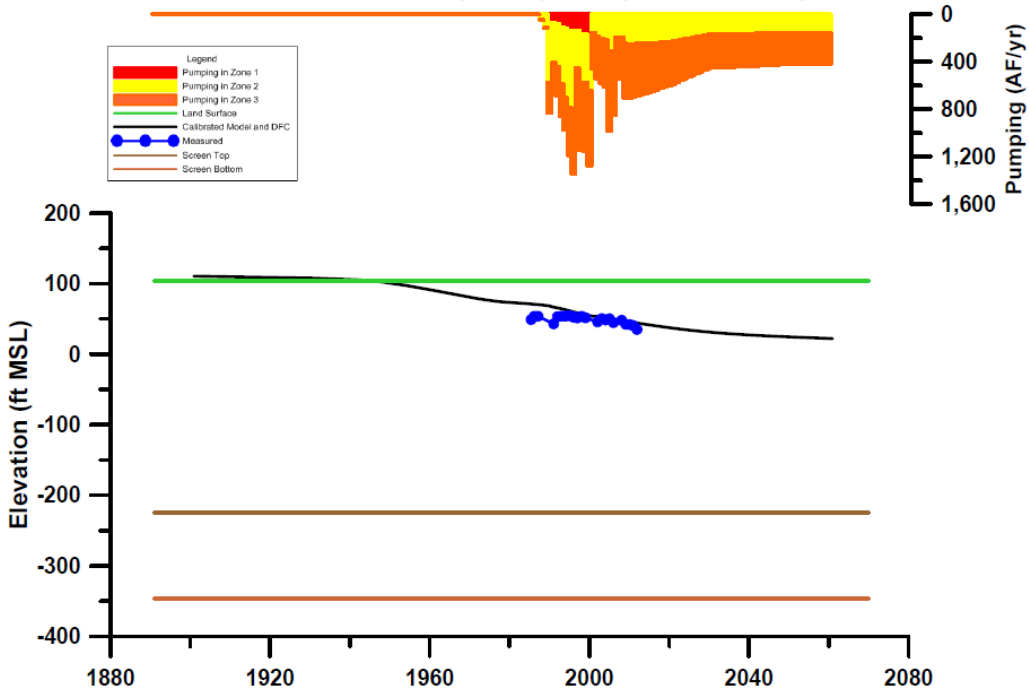


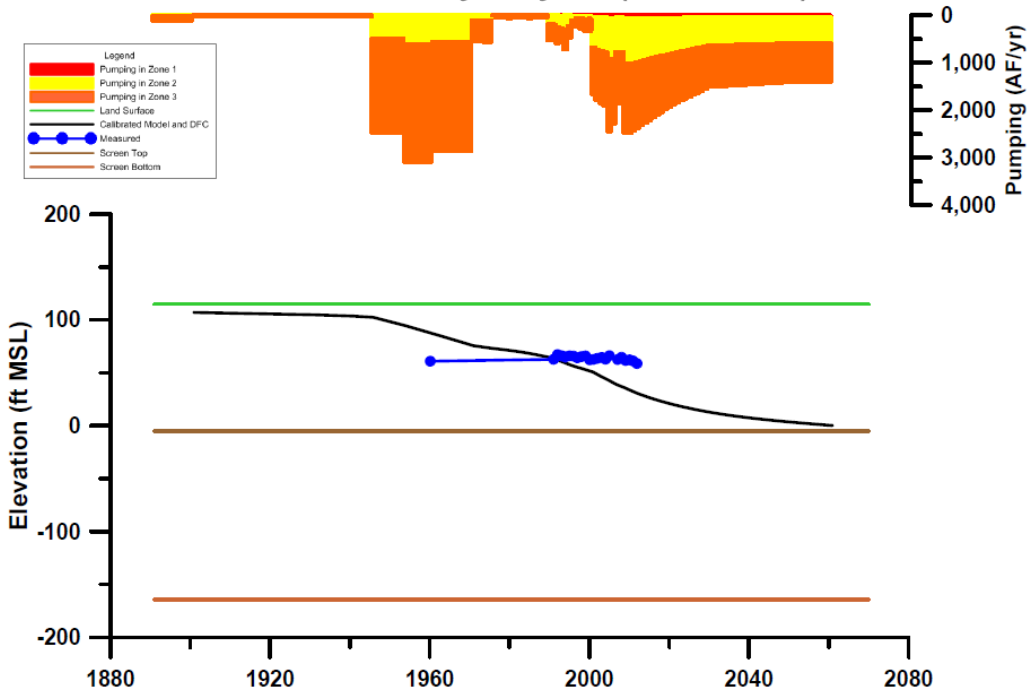
Figure A46
Waller County Pumping vs. GHB Flows



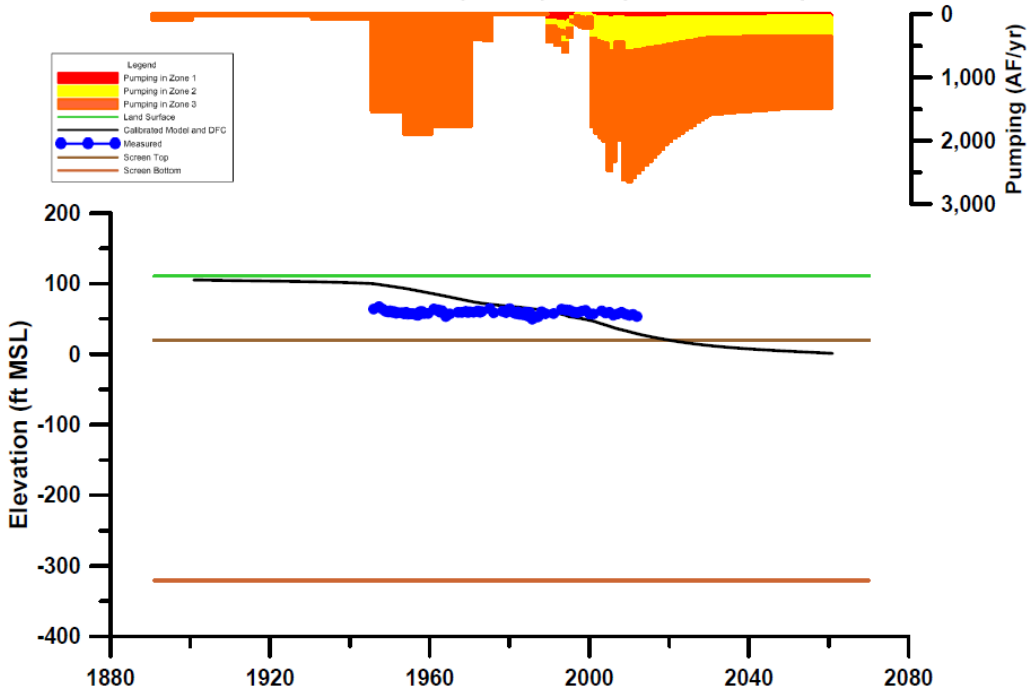
**Figure A47 - Well 65-17-505
Fort Bend County - Layer 1 (GAM & DFC)**



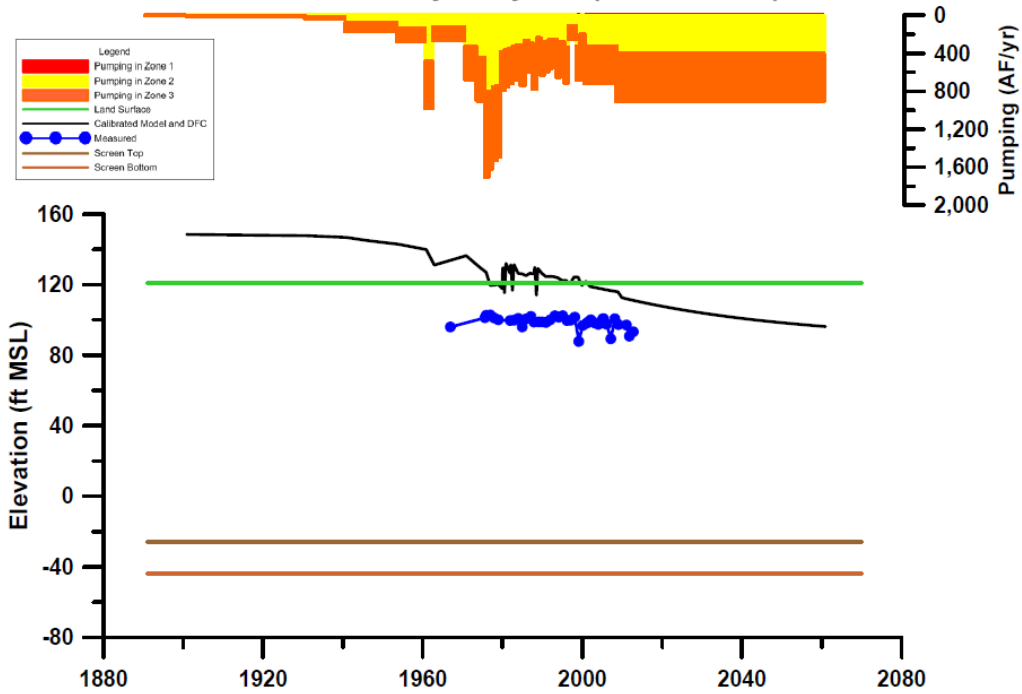
**Figure A48 - Well 65-25-202
Fort Bend County - Layer 1 (GAM & DFC)**



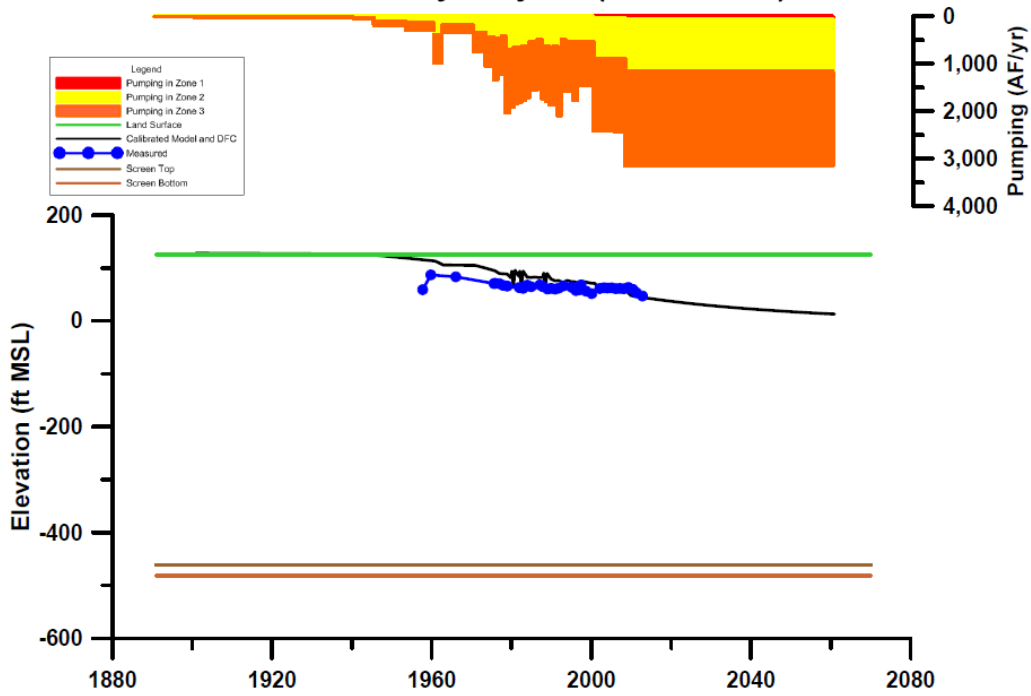
**Figure A49 - Well 65-25-301
Fort Bend County - Layer 1 (GAM & DFC)**



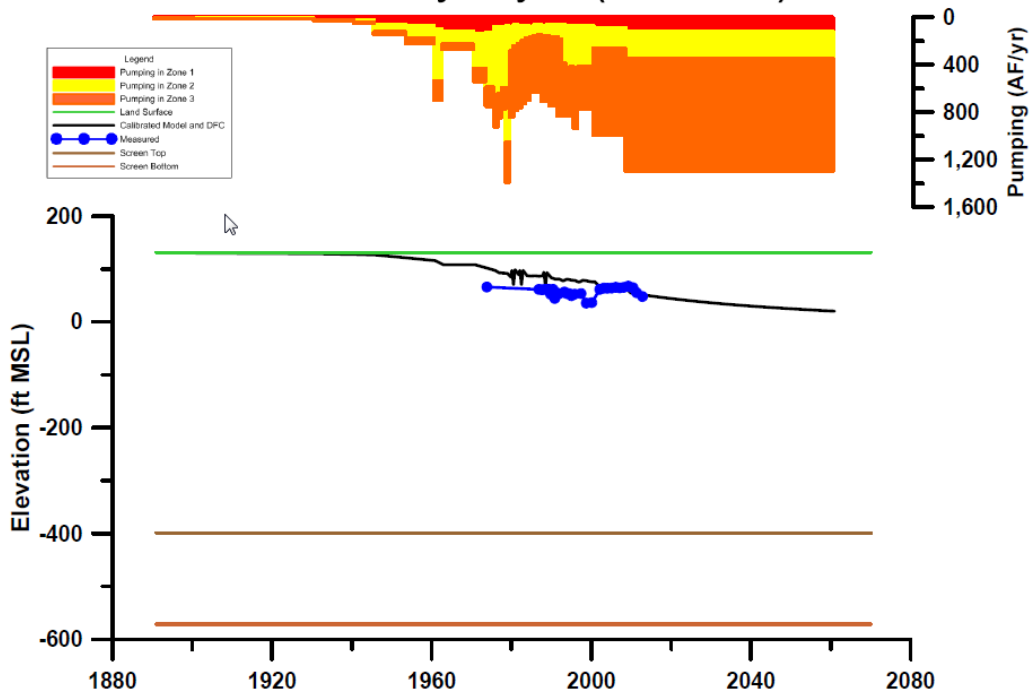
**Figure A50 - Well 66-16-407
Austin County - Layer 2 (GAM & DFC)**



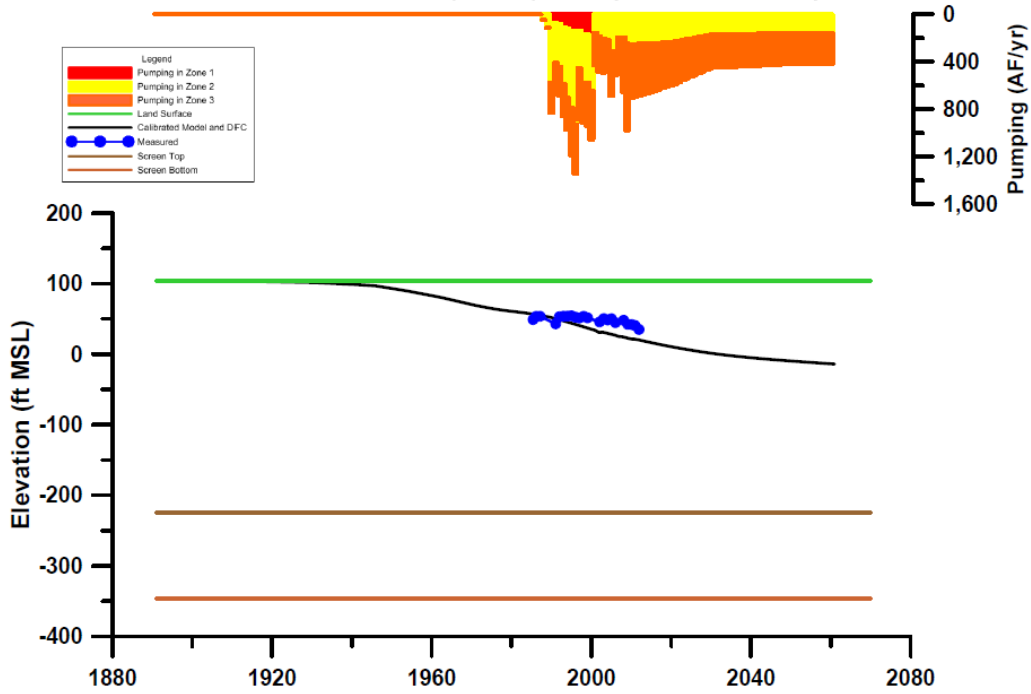
**Figure A51 - Well 66-24-801
Austin County - Layer 2 (GAM & DFC)**



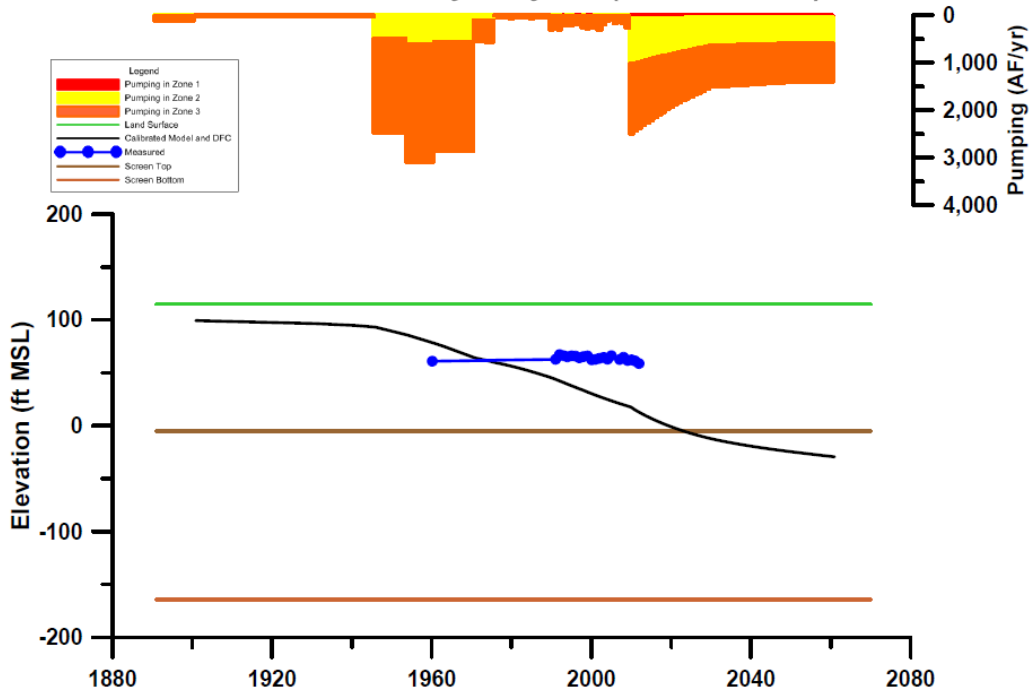
**Figure A52 - Well 66-24-805
Austin County - Layer 2 (GAM & DFC)**



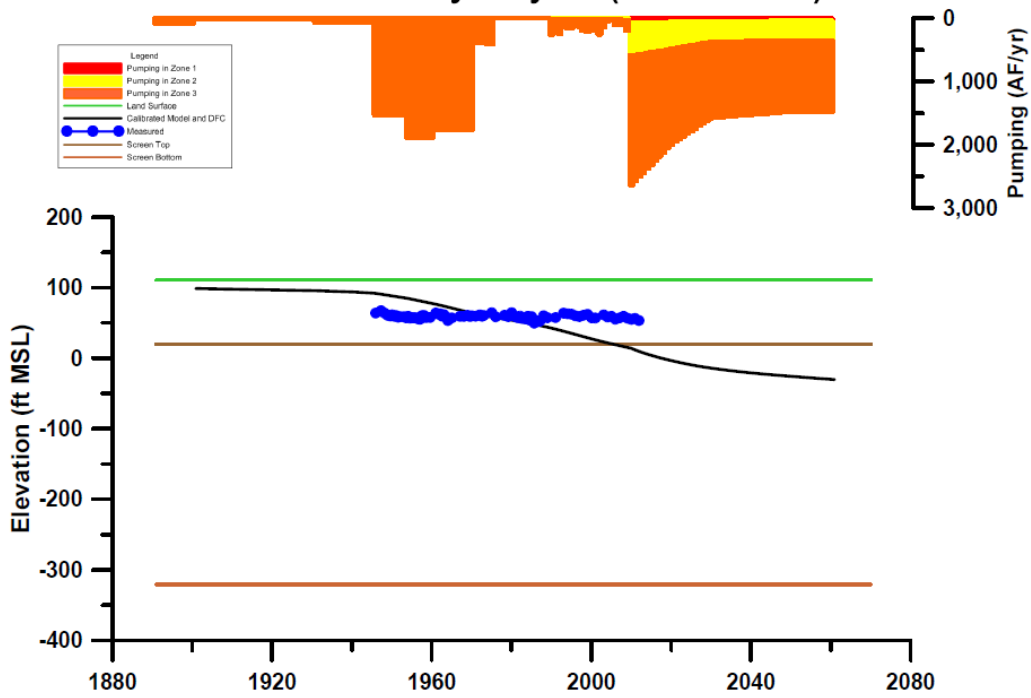
**Figure A53 - Well 65-17-505
Fort Bend County - Layer 1 (HAGM & DFC)**



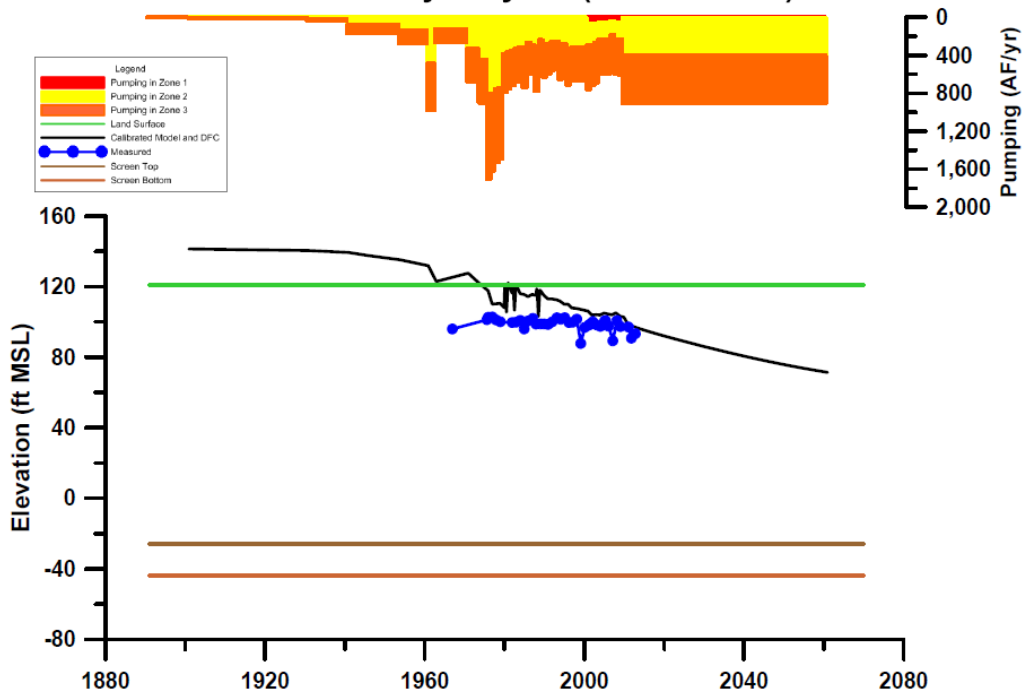
**Figure A54 - Well 65-25-202
Fort Bend County - Layer 1 (HAGM & DFC)**



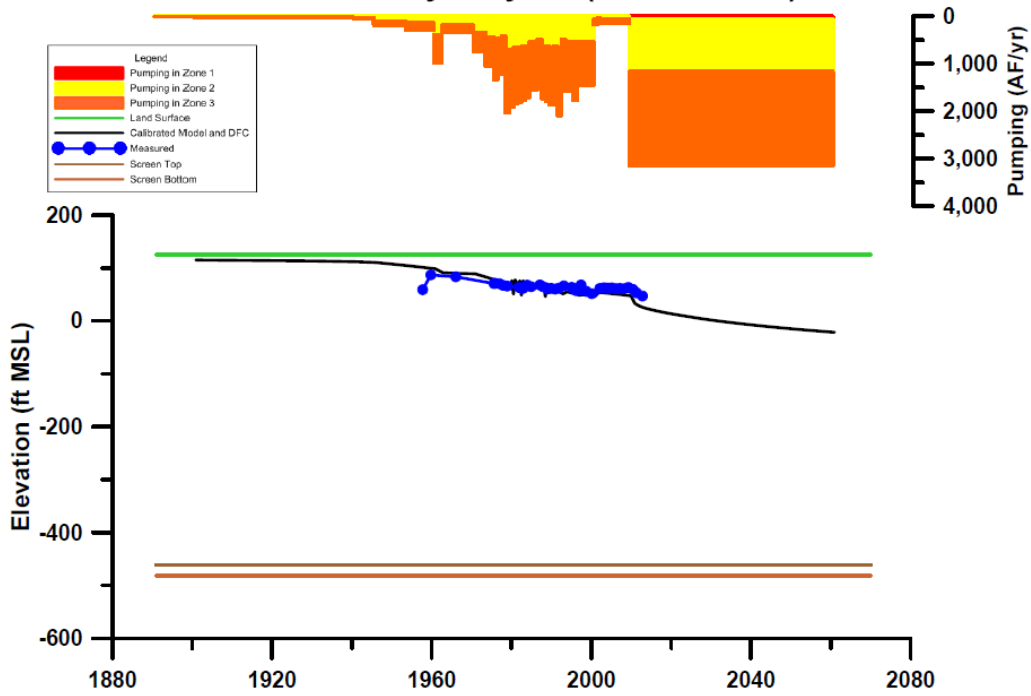
**Figure A55 - Well 65-25-301
Fort Bend County - Layer 1 (HAGM & DFC)**



**Figure A56 - Well 66-16-407
Austin County - Layer 2 (HAGM & DFC)**



**Figure A57 - Well 66-24-801
Austin County - Layer 2 (HAGM & DFC)**



**Figure A58 - Well 66-24-805
Austin County - Layer 2 (HAGM & DFC)**

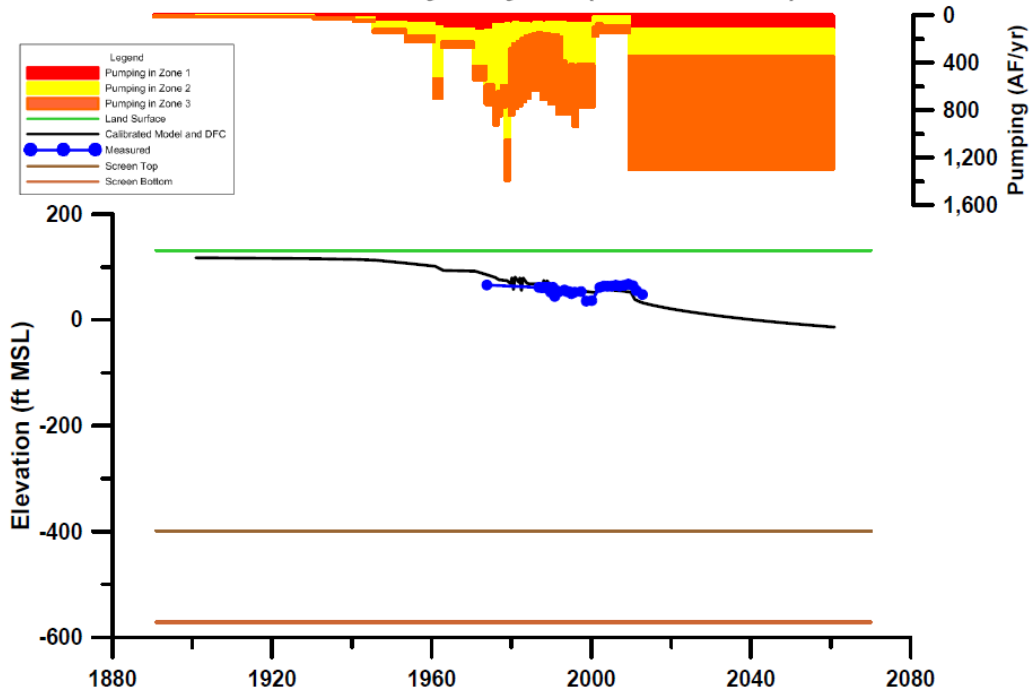


Figure A59 - Well 65-17-505
Fort Bend County - Layer 1 (GAM and HAGM Comparison)

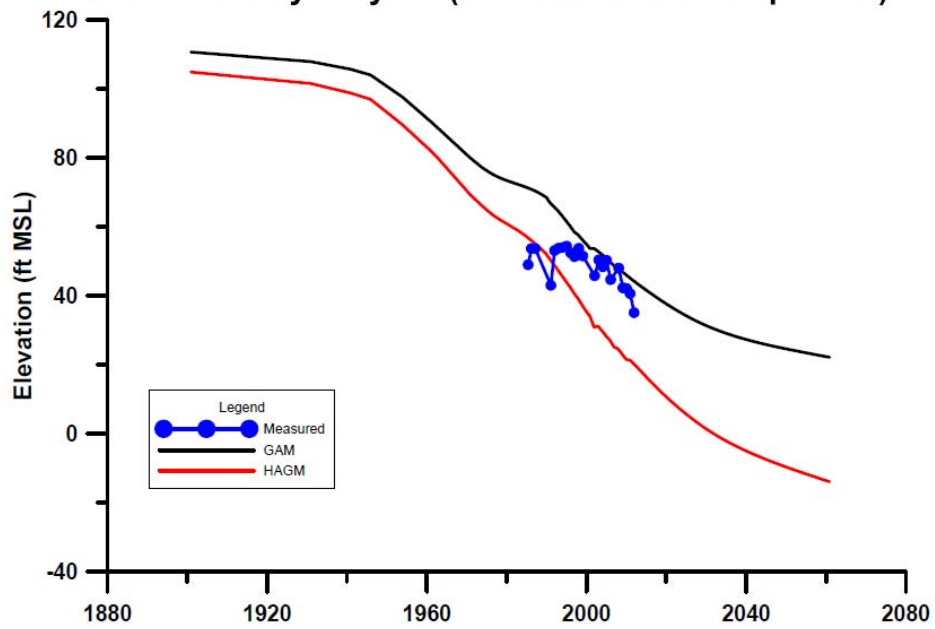
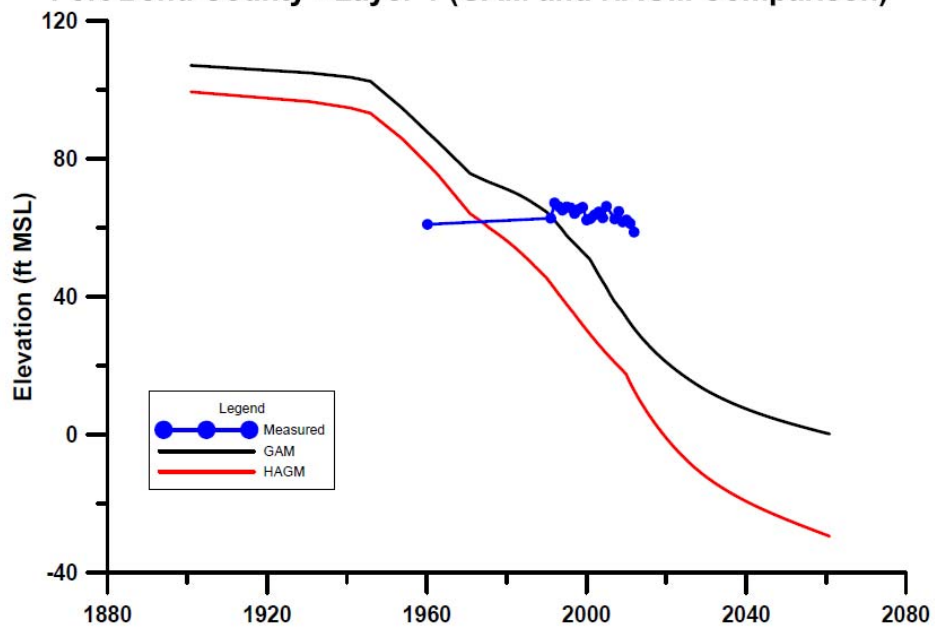
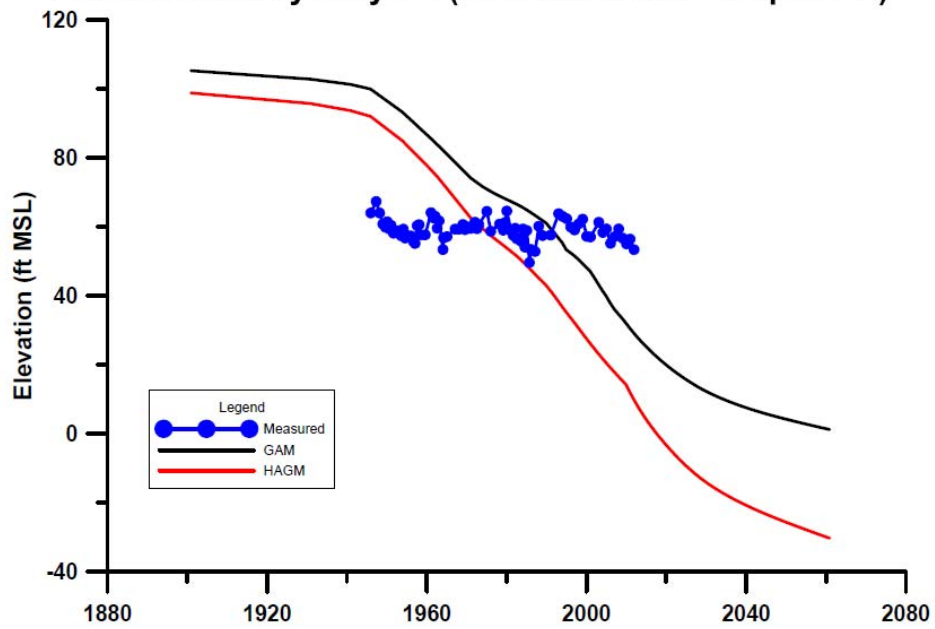


Figure A60 - Well 65-25-202
Fort Bend County - Layer 1 (GAM and HAGM Comparison)



**Figure A61 - Well 65-25-301
Fort Bend County - Layer 1 (GAM and HAGM Comparison)**



**Figure A62 - Well 66-16-407
Austin County - Layer 2 (GAM and HAGM Comparison)**

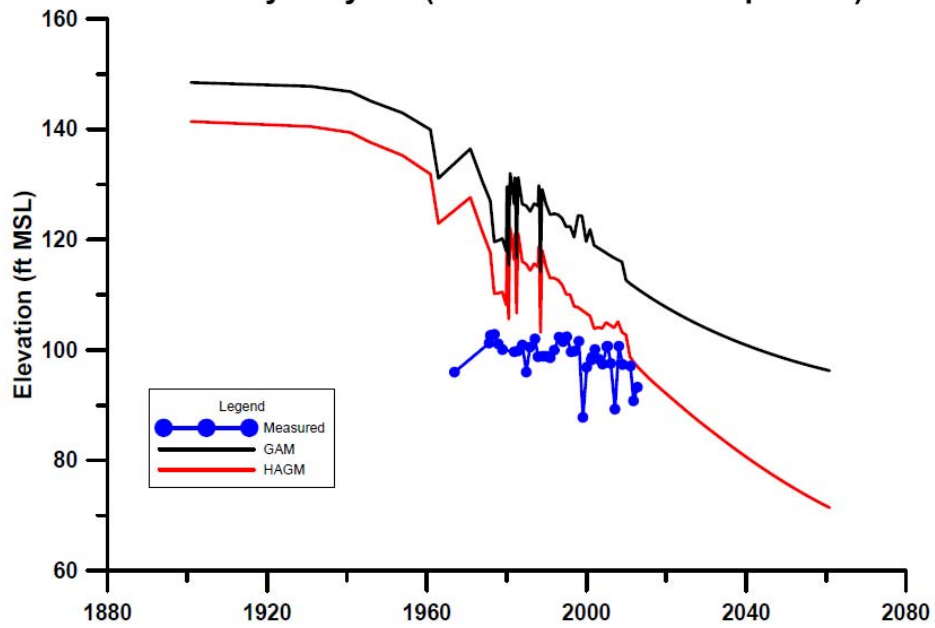


Figure A63 - Well 66-24-801
Austin County - Layer 2 (GAM and HAGM Comparison)

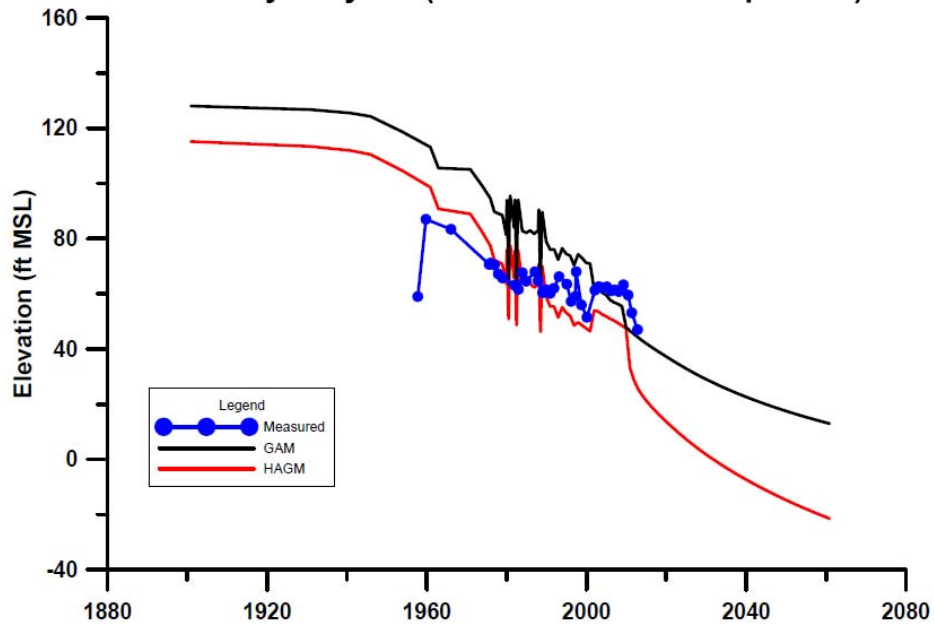
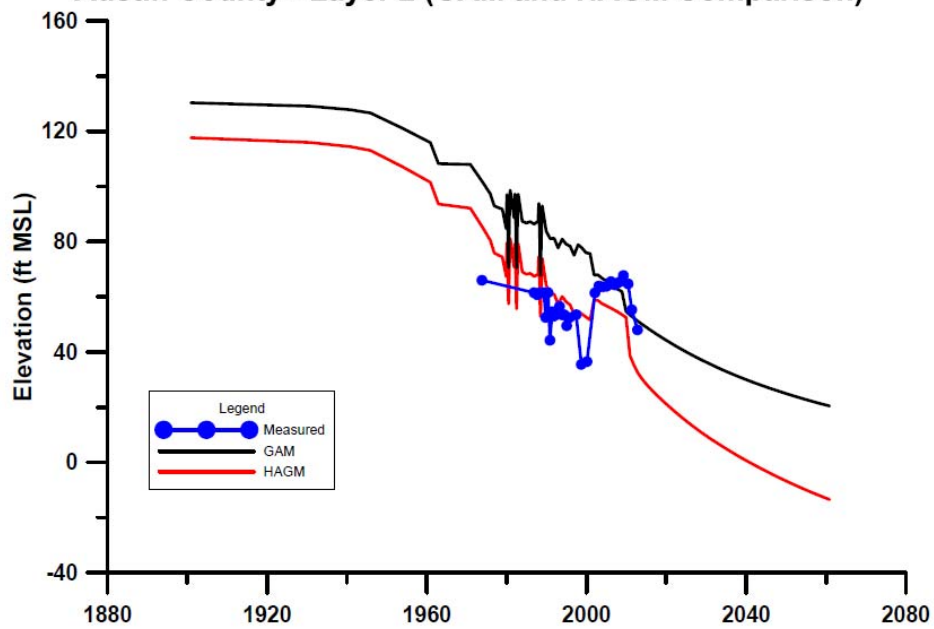
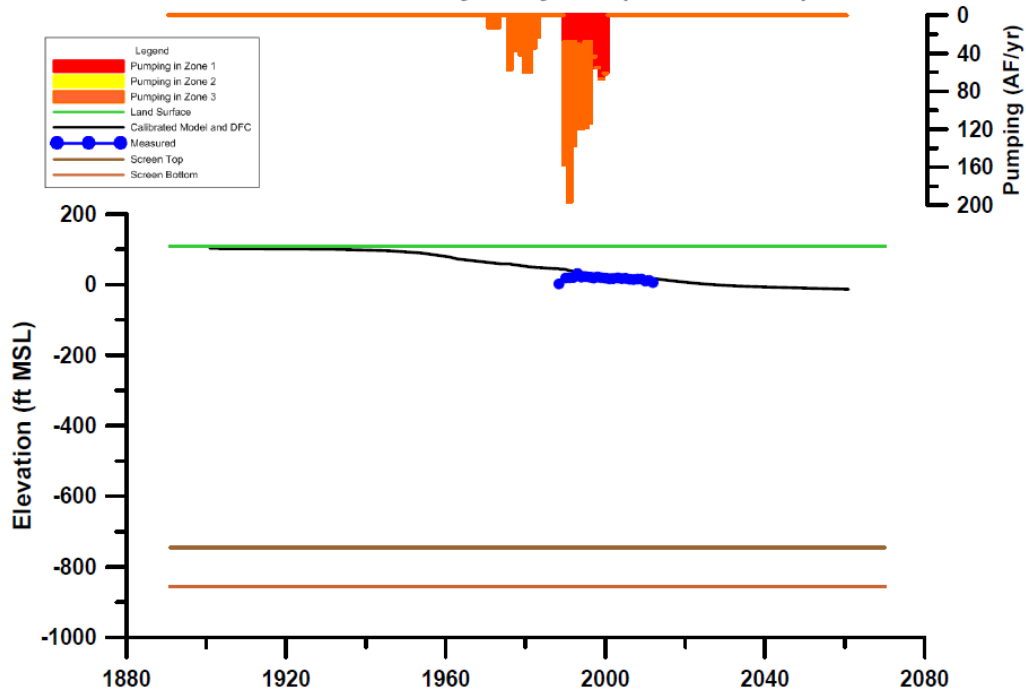


Figure A64 - Well 66-24-805
Austin County - Layer 2 (GAM and HAGM Comparison)



**Figure A65 - Well 65-33-210
Fort Bend County - Layer 2 (GAM & DFC)**



**Figure A66 - Well 65-33-210
Fort Bend County - Layer 2 (HAGM & DFC)**

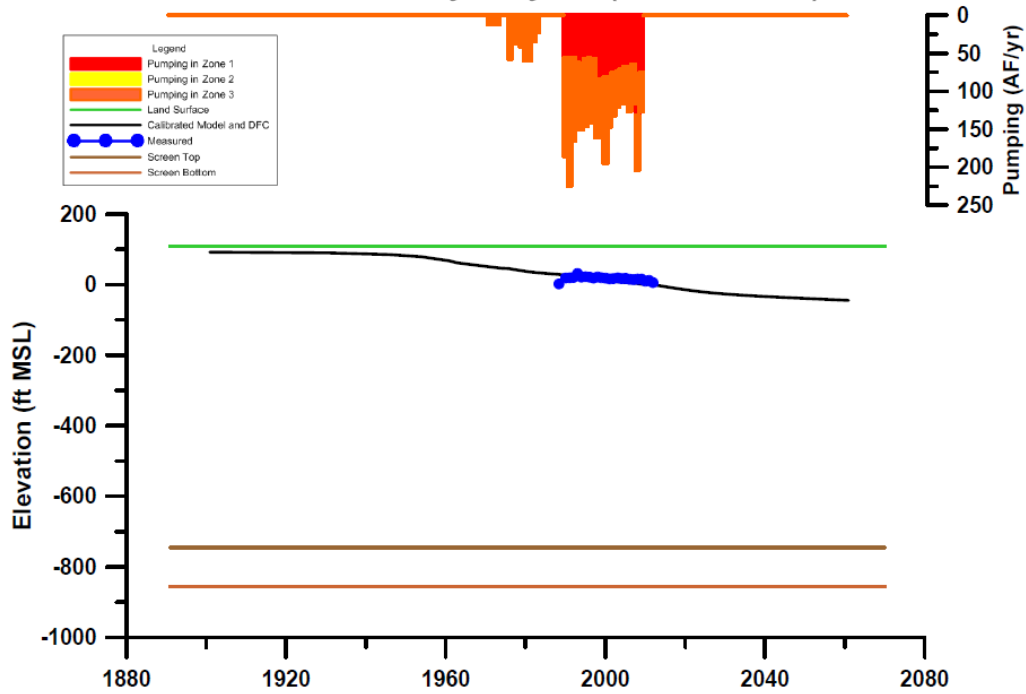


Figure A67 - Well 65-43-101
Comparison of Actual with GAM (Layers 1 and 2)

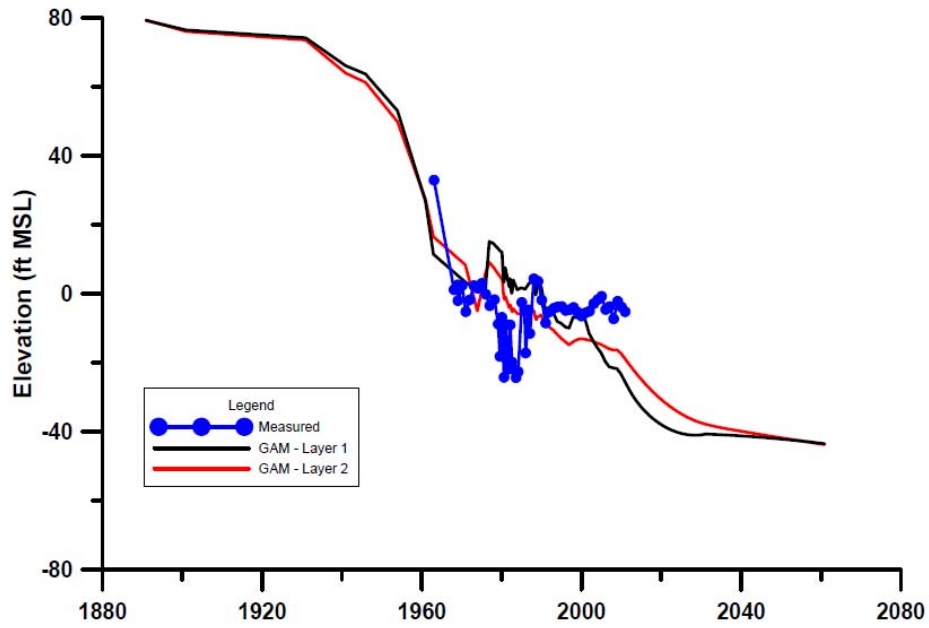
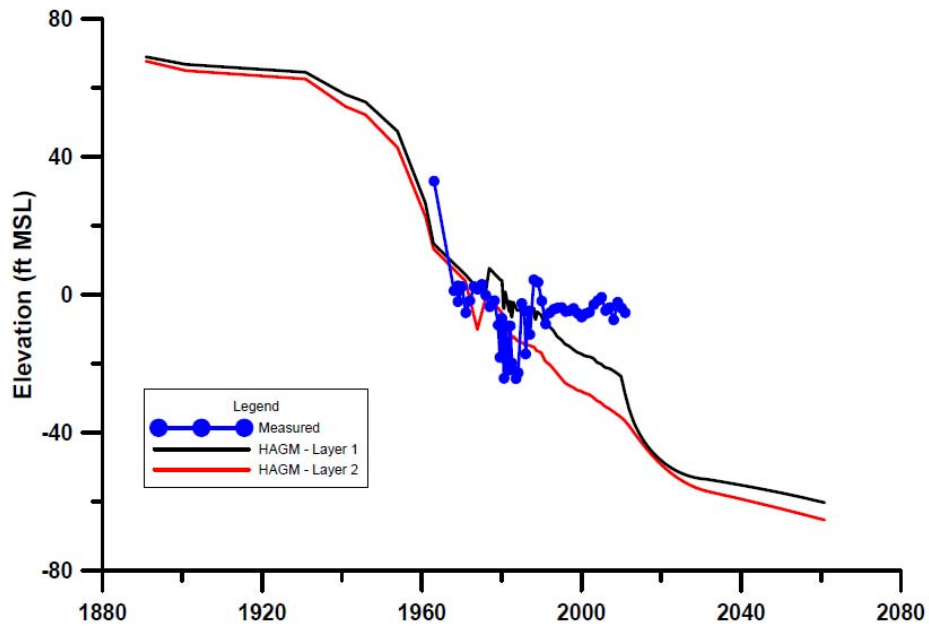
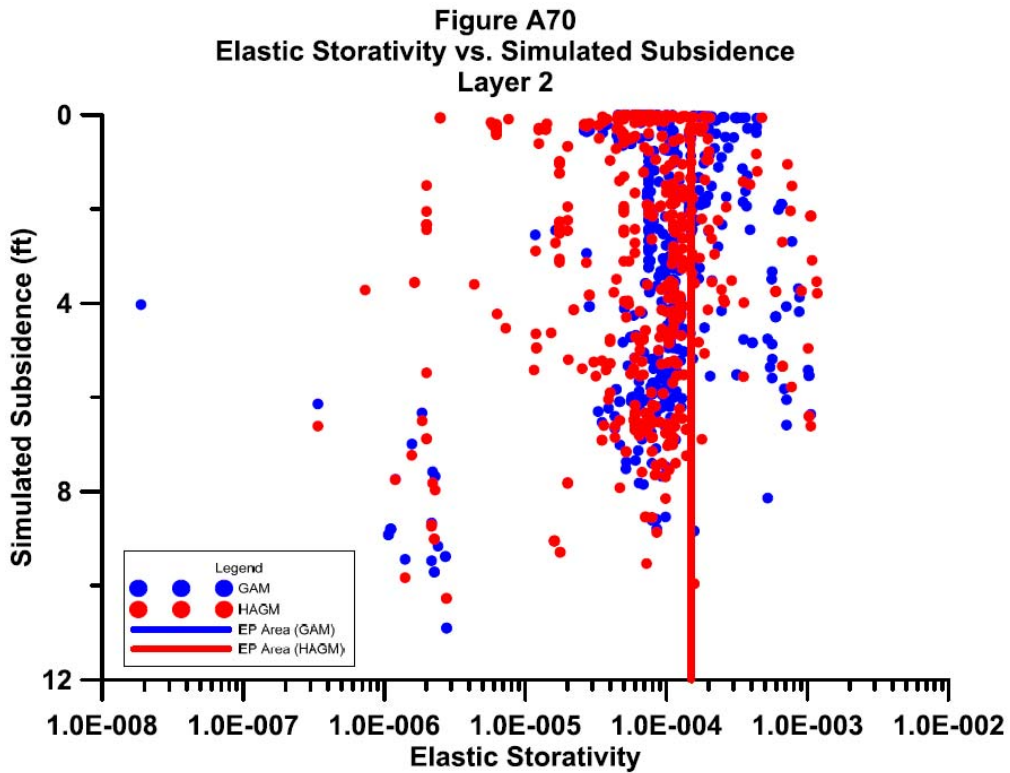
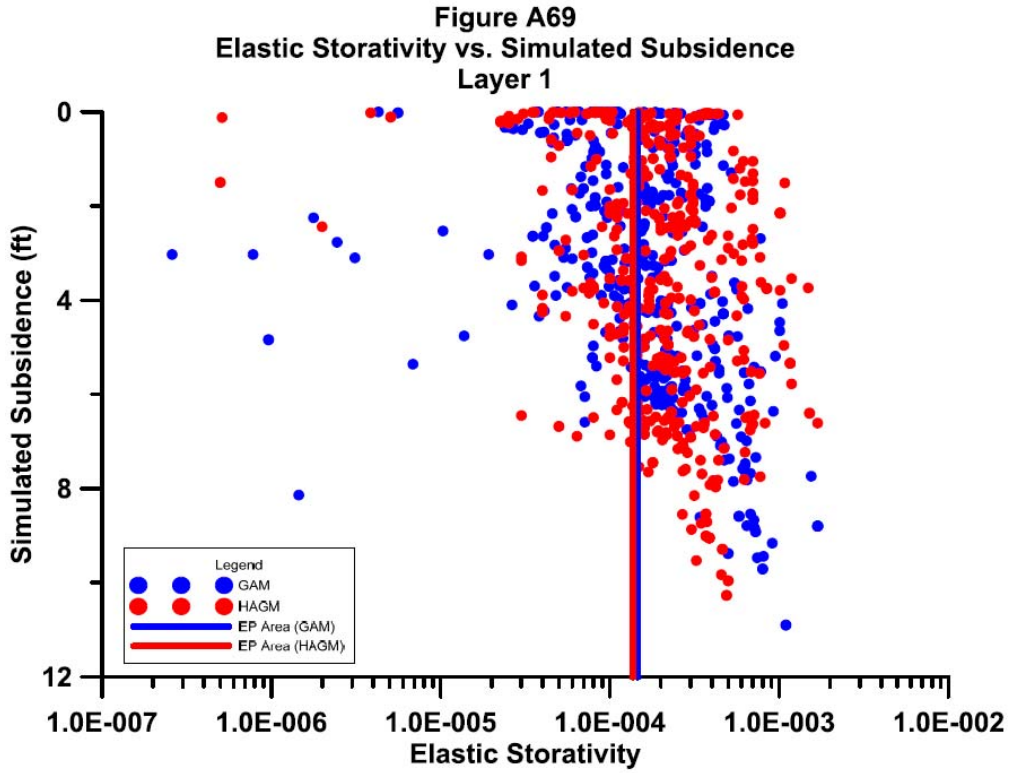


Figure A68 - Well 65-43-101
Comparison of Actual with HAGM (Layers 1 and 2)





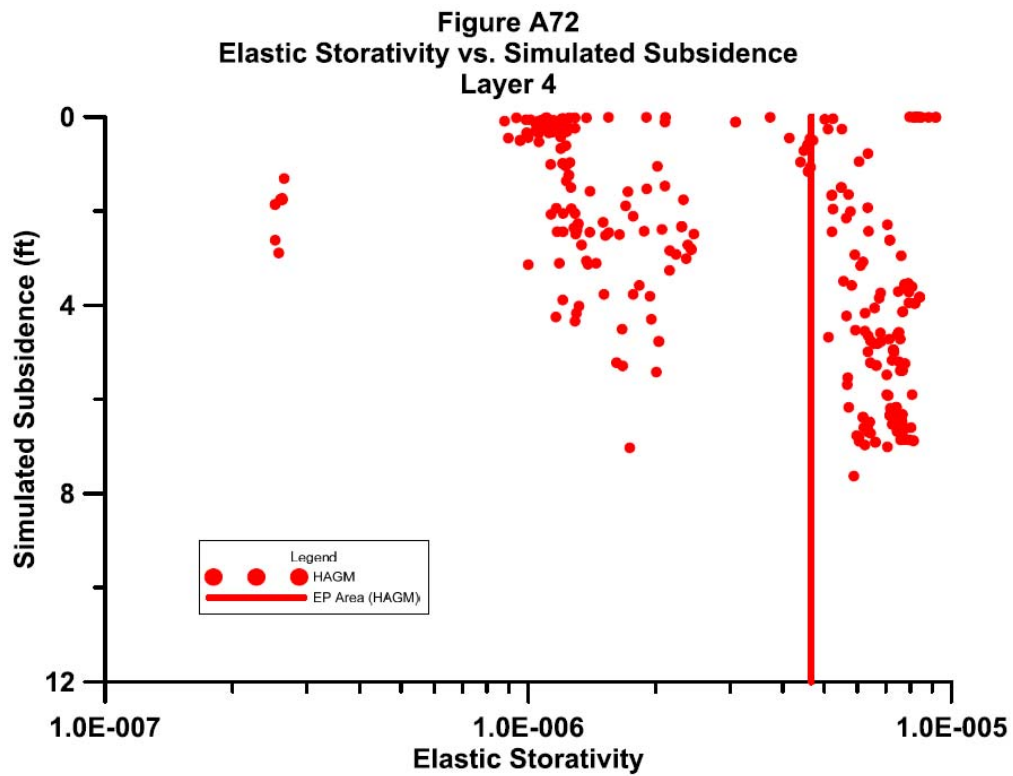
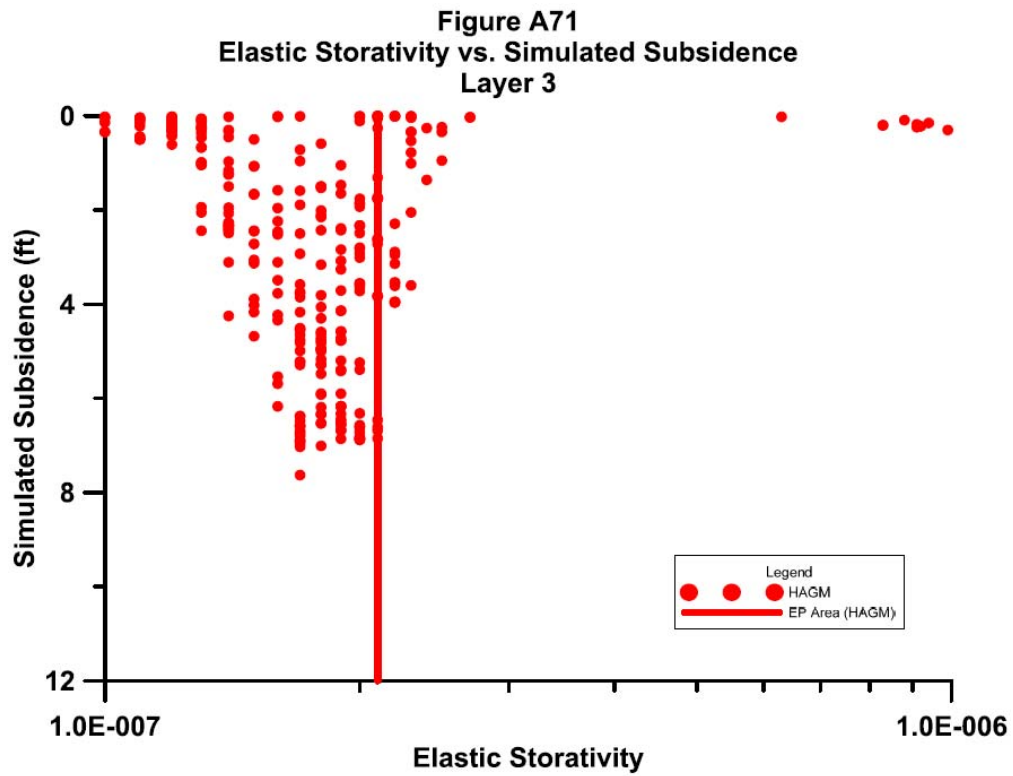


Figure A73
Inelastic Storativity vs. Simulated Subsidence
Layer 1

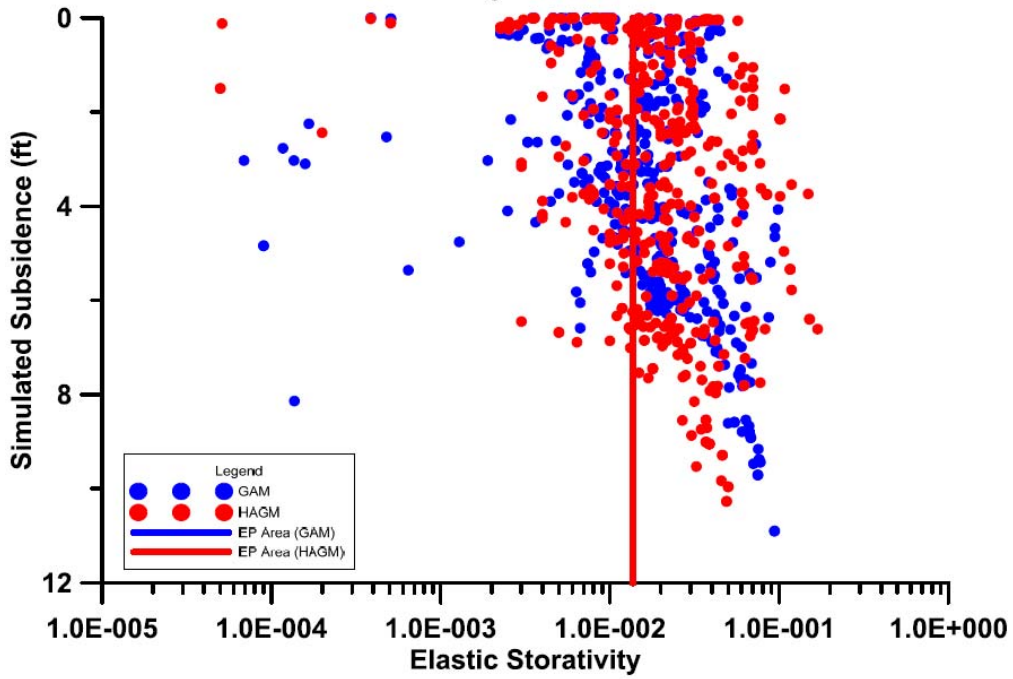


Figure A74
Inelastic Storativity vs. Simulated Subsidence
Layer 2

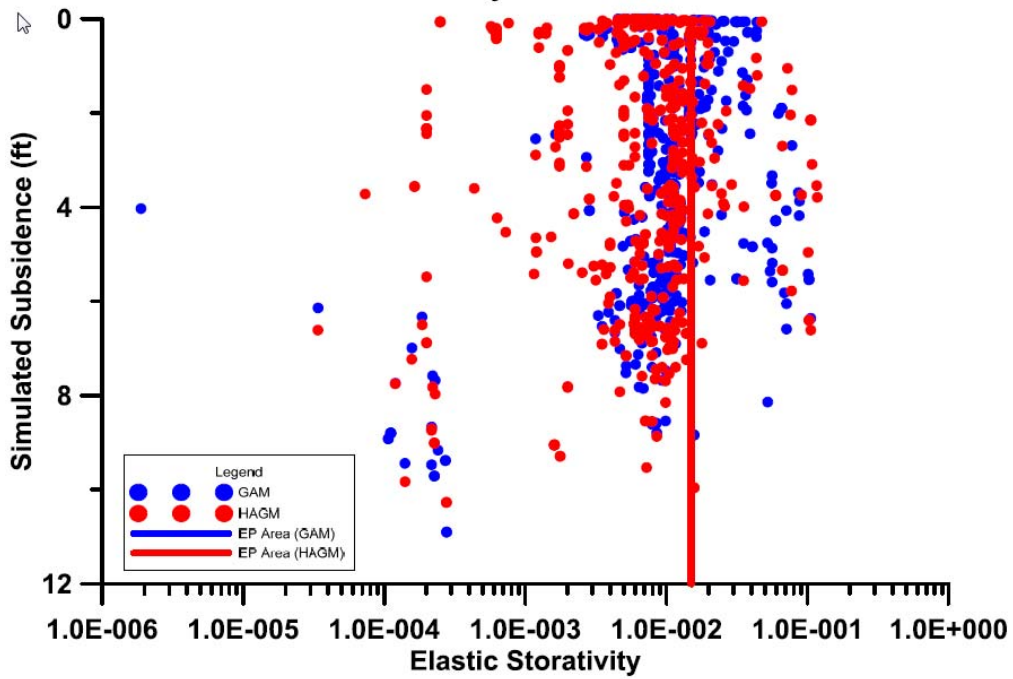


Figure A75
Inelastic Storativity vs. Simulated Subsidence
Layer 3

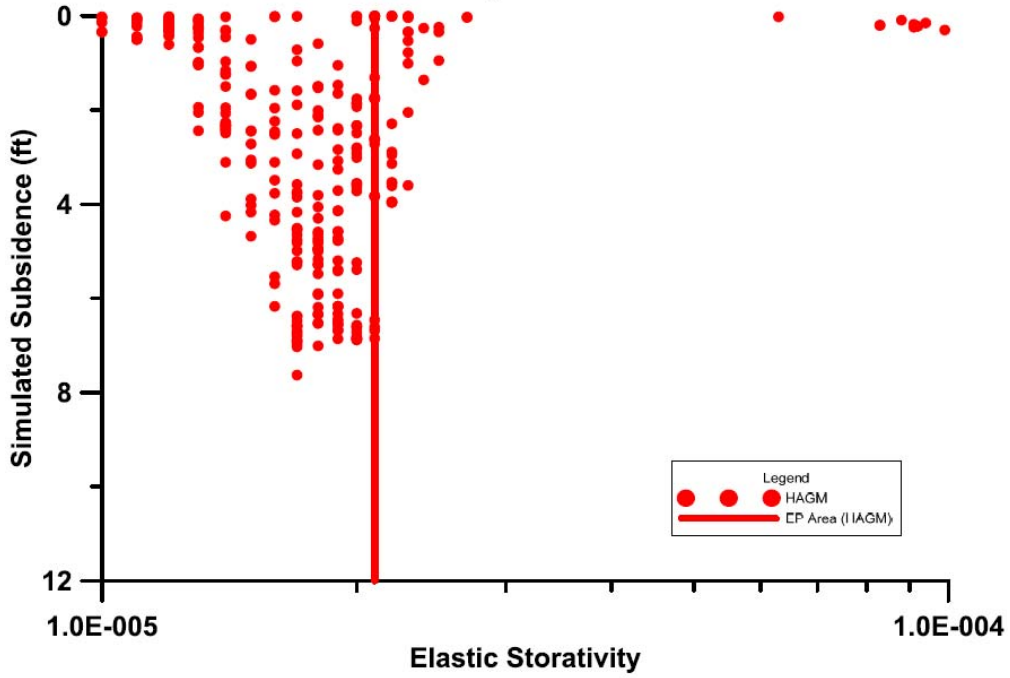
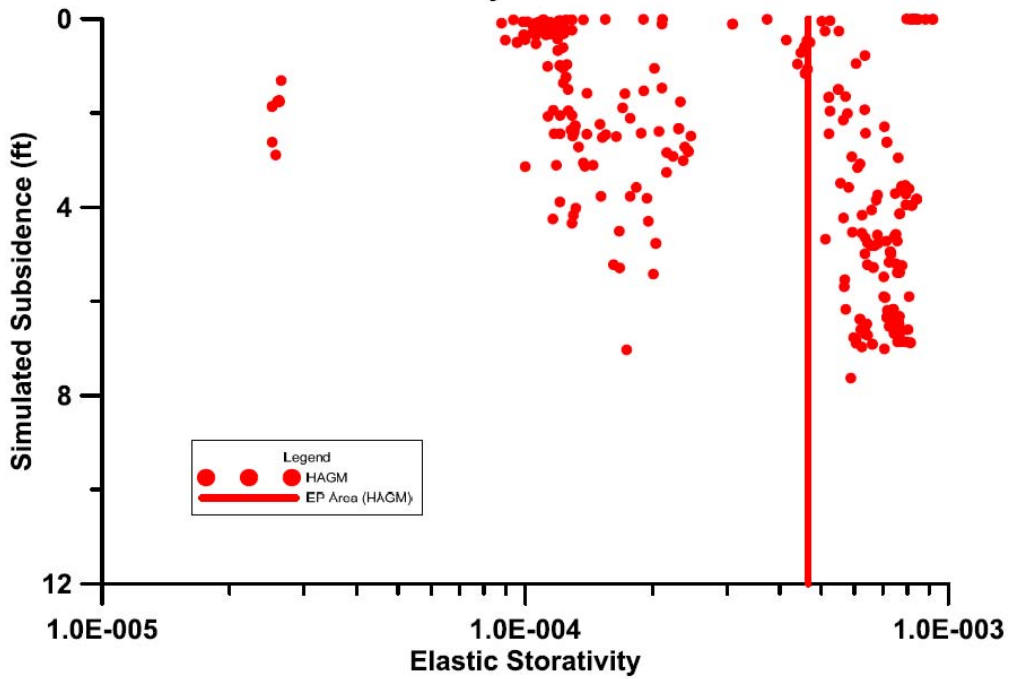


Figure A76
Inelastic Storativity vs. Simulated Subsidence
Layer 4



Appendix B – GMA 14 Resolution Regarding Subsidence Districts

Formations in Fort Bend, Galveston, and Harris Counties

The Groundwater Management Area (GMA) efforts to determine Desired Future Conditions (DFCs) is primarily an aquifer water-level based approach to describe the regional and local desires for the aquifer beneath them. The GMA process only requires Groundwater Conservation Districts (GCDs) to determine the DFCs for the entire GMA, regardless of whether each county is included within a GCD. The Fort Bend Subsidence District (FBSD) and the Harris-Galveston Subsidence District (HGSD), operating in Fort Bend County and Harris and Galveston Counties, respectively, regulate groundwater for the purpose of ending land surface subsidence within their jurisdiction. They are not GCDs and operate considerably different from the typical GCD. Therefore, in an official context these three counties are “unrepresented” but the GCDs within GMA-14 must still determine the DFC for these counties.

Both FBSD and HGSD have participated in an unofficial role to aid the GCDs within GMA-14 with their evaluation of Fort Bend, Galveston and Harris County information. The groundwater pumpage within these three counties even though regulated is still greater than the sum of all other counties within GMA-14. FBSD and HGSD recognize that the projected groundwater pumpage from these three counties will impact the decisions of GMA-14 throughout a large portion of the area. FBSD and HGSD have provided considerable historical and projected groundwater pumpage data and details of regulations to assist GMA-14 in incorporating these counties in the overall GMA-14 DFC. FBSD and HGSD cannot however, present DFCs for these three counties in terms of aquifer water-level changes over time. The FBSD and HGSD regulations do not specifically address water-levels nor do they designate a specific pumping limit, rather the regulations are based on limitations of groundwater as a percentage of total water demand. The percentage of groundwater to total water demand is decreased over time, as total water demand increases.

The goal of both FBSD and HGSD is to end land surface subsidence that is caused by man’s pumpage of groundwater. There is a clearly established link between the over-pumpage of groundwater and land surface subsidence. The DFC within the aquifer beneath Fort Bend, Galveston, and Harris Counties has no easily defined relationship to water-levels. The Desired Future Condition for FBSD and HGSD is the reduction and halting of the compaction of clay layers within the aquifer caused by the over-pumpage of groundwater. Stated more simply, the DFC for these three counties is that future land surface subsidence be avoided. That stated HGSD and FBSD have adopted regulations, most recently in 1999 and 2003 respectively that require the reduction of groundwater pumpage and the conversion to alternate water sources, while balancing with the realistic ability of the permittees to achieve compliance with these regulations.

Within HGSD, from central to southeastern Harris County and all of Galveston County (Regulatory Areas 1 and 2), virtually all permittees have achieved compliance with previous and current HGSD regulations. Subsidence has been halted and water-levels within the aquifer have risen dramatically in these areas. However, in northern and western areas of Harris County (Regulatory Area 3), the HGSD regulations have allowed groundwater pumpage to continue until the required reductions in 2010, 2020, and 2030. With these scheduled reductions in groundwater pumpage, subsidence will slow dramatically and even be halted with water-levels stabilizing and in later years rising.

Within FBSD, from central to northern and eastern Fort Bend County (Regulatory Area A), the regulations call for reductions of groundwater pumpage in 2013/2015, and 2025. Similar to HGSD's Regulatory Area 3, subsidence within FBSD Regulatory Area A will slow dramatically and even be halted with water-levels stabilizing and in later years rising.

In both HGSD and FBSD, because of the percentage based approach to regulations, groundwater pumpage will increase until scheduled reductions in milestone years (ex: 2010, 2013/2015, 2020, 2025, and 2030). In between milestone years, groundwater pumpage will increase with the assumed increase in total water demand from an assumed increase in population. In order to demonstrate the DFC of these three counties using water-level changes, the area of previous groundwater-to-alternative water conversions must be separated from future conversions AND each annual time step must be depicted. If a further separation in to layers of the aquifer is necessary, then it is quite apparent that describing the DFC in terms of water-levels is far too complicated and error prone.

The HGSD and FBSD have submitted to GMA-14 their current regulations and projected groundwater pumpages through the year 2030. This data has been divided into the grid cells/layers relative to the Northern Gulf Coast Groundwater Availability Model (NGCGAM) and utilized by the GCDs in development of their DFCs. For the years beyond 2030, assumptions were made to address groundwater pumping limits.

Groundwater pumpage within GMA-14 from Fort Bend, Galveston, and Harris Counties is regulated by FBSD and HGSD, non GCD governmental agencies (the only GMA with this occurrence) and the missions of HGSD and FBSD are vastly different from GCDs and do not fit well with a water-level designed DFC process). The groundwater pumpage projections developed in recognition of the HGSD and FBSD regulatory plans have been utilized without adjustment by GMA14 in the DFC process. Therefore, the DFCs adopted by GMA-14 are consistent with the HGSD and FBSD regulatory plans.

Appendix C – Tables and Maps of Simulated Well Drawdown Estimates

Table C-1
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 1 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-5429	54	66	6180054.5	19142336	0.15	1	31.85	44.01	76.39	50.60	12.17	44.55	18.75
BAUS-5430	54	66	6180054.5	19142336	0.15	1	31.85	44.01	76.39	50.60	12.17	44.55	18.75
BWLL-5117	53	69	6191012.5	19154344	0.34	1	26.21	41.79	73.96	50.66	15.59	47.76	24.46
BWLL-5481	53	70	6191500	19157906	0.36	1	24.63	38.23	65.42	45.80	13.60	40.79	21.17
BWLL-5006	54	69	6190699	19153424	0.46	1	26.72	40.39	69.45	47.94	13.67	42.73	21.23
BAUS-4159	53	66	6177818.5	19144046	0.47	1	31.10	44.63	78.96	52.11	13.53	47.86	21.00
BAUS-4158	53	66	6177811.5	19144248	0.49	1	31.10	44.63	78.96	52.11	13.53	47.86	21.00
BWLL-5541	52	69	6186065.5	19157628	0.50	1	25.63	41.48	73.87	50.53	15.86	48.25	24.90
BWLL-5541	53	69	6188533	19157786	0.54	1	26.21	41.79	73.96	50.66	15.59	47.76	24.46
BWLL-5543	52	69	6186496.5	19157650	0.56	1	25.63	41.48	73.87	50.53	15.86	48.25	24.90
BAUS-4458	51	67	6175604	19159156	0.63	1	28.44	44.03	78.40	52.82	15.59	49.95	24.38
BWLL-4133	51	67	6175182.5	19158636	0.63	1	28.44	44.03	78.40	52.82	15.59	49.95	24.38
BAUS-5436	51	67	6174074	19157298	0.72	1	28.44	44.03	78.40	52.82	15.59	49.95	24.38
BAUS-5447	51	67	6173795	19157412	0.78	1	28.44	44.03	78.40	52.82	15.59	49.95	24.38
BAUS-4340	53	65	6171277.5	19142192	0.84	1	32.58	44.18	75.26	50.38	11.60	42.67	17.80
BWLL-4363	52	69	6186773	19159558	0.88	1	25.63	41.48	73.87	50.53	15.86	48.25	24.90
BAUS-5426	51	67	6173430.5	19159360	0.98	1	28.44	44.03	78.40	52.82	15.59	49.95	24.38
BAUS-5401	51	67	6172709	19157480	0.99	1	28.44	44.03	78.40	52.82	15.59	49.95	24.38
BAUS-5398	51	66	6171645	19154492	1.25	1	29.85	43.79	76.22	51.46	13.94	46.37	21.61
BAUS-4236	50	67	6173220	19161806	1.31	1	27.61	41.55	71.77	49.18	13.94	44.16	21.57
6517415	55	67	6187339.5	19141354	1.34	1	30.89	42.40	70.98	48.53	11.51	40.10	17.64
BAUS-4485	50	67	6172028.5	19160648	1.34	1	27.61	41.55	71.77	49.18	13.94	44.16	21.57
BAUS-4325	50	67	6172780	19161790	1.36	1	27.61	41.55	71.77	49.18	13.94	44.16	21.57
BAUS-4518	50	68	6174657	19163476	1.42	1	26.11	40.27	69.74	48.06	14.15	43.63	21.94
BAUS-5298	50	67	6172278	19161868	1.44	1	27.61	41.55	71.77	49.18	13.94	44.16	21.57
BAUS-4515	51	66	6170610	19153510	1.50	1	29.85	43.79	76.22	51.46	13.94	46.37	21.61
BAUS-4519	50	68	6175159	19164204	1.52	1	26.11	40.27	69.74	48.06	14.15	43.63	21.94
BAUS-5397	51	66	6169866.5	19155934	1.52	1	29.85	43.79	76.22	51.46	13.94	46.37	21.61
BAUS-0002A	50	68	6175328	19164412	1.54	1	26.11	40.27	69.74	48.06	14.15	43.63	21.94
BAUS-0002B	50	68	6175328	19164412	1.54	1	26.11	40.27	69.74	48.06	14.15	43.63	21.94
BAUS-5400	50	67	6171322	19161498	1.54	1	27.61	41.55	71.77	49.18	13.94	44.16	21.57
BAUS-5402	50	67	6170748.5	19160828	1.56	1	27.61	41.55	71.77	49.18	13.94	44.16	21.57
BWLL-5690	51	69	6184161	19164328	1.65	1	25.03	39.85	69.88	48.20	14.82	44.85	23.17
BAUS-4430	50	66	6168784	19157800	1.73	1	28.84	41.60	70.44	48.44	12.76	41.60	19.59
BAUS-4185	52	66	6170700	19150982	1.73	1	30.53	44.91	79.51	52.93	14.38	48.98	22.40
BAUS-5399	50	66	6168767	19157550	1.73	1	28.84	41.60	70.44	48.44	12.76	41.60	19.59
BWLL-4303	50	68	6177915	19165922	1.75	1	26.11	40.27	69.74	48.06	14.15	43.63	21.94
6509702	52	71	6193335.5	19165170	1.76	1	22.85	34.44	56.81	40.70	11.58	33.96	17.84
BAUS-4429	50	66	6168601	19157996	1.77	1	28.84	41.60	70.44	48.44	12.76	41.60	19.59
BAUS-5297	50	68	6173472	19165068	1.79	1	26.11	40.27	69.74	48.06	14.15	43.63	21.94
BAUS-4129	55	65	6178444	19131512	1.81	1	34.50	43.99	70.09	48.85	9.49	35.59	14.35
BWLL-4992	50	68	6177988.5	19166330	1.83	1	26.11	40.27	69.74	48.06	14.15	43.63	21.94
BWLL-4272	50	68	6177805.5	19166526	1.87	1	26.11	40.27	69.74	48.06	14.15	43.63	21.94
BAUS-0024	56	65	6179473	19131326	1.87	1	35.56	43.85	66.41	47.95	8.29	30.86	12.39
BWLL-5674	51	69	6184132.5	19165744	1.92	1	25.03	39.85	69.88	48.20	14.82	44.85	23.17
BWLL-4161	50	69	6177699	19167028	1.96	1	24.33	37.51	63.98	44.74	13.18	39.65	20.41
BAUS-4299	50	69	6178487	19167158	1.99	1	24.33	37.51	63.98	44.74	13.18	39.65	20.41
BWLL-5082	51	69	6183630	19166128	1.99	1	25.03	39.85	69.88	48.20	14.82	44.85	23.17
BAUS-4138	51	65	6166124	19148388	2.10	1	30.98	42.91	71.99	49.25	11.93	41.01	18.27
6624203	51	65	6166932	19150042	2.15	1	30.98	42.91	71.99	49.25	11.93	41.01	18.27
BWLL-4134	52	71	6197009.5	19166208	2.19	1	22.85	34.44	56.81	40.70	11.58	33.96	17.84
BAUS-4137	51	65	6165560.5	19149382	2.29	1	30.98	42.91	71.99	49.25	11.93	41.01	18.27
BAUS-5120	50	66	6166456	19161362	2.33	1	28.84	41.60	70.44	48.44	12.76	41.60	19.59
BAUS-4552	49	66	6166768	19162486	2.37	1	27.55	38.83	63.65	44.65	11.28	36.10	17.10
BAUS-4235	49	66	6166764.5	19162588	2.38	1	27.55	38.83	63.65	44.65	11.28	36.10	17.10
BAUS-4324	49	66	6166588.5	19162582	2.41	1	27.55	38.83	63.65	44.65	11.28	36.10	17.10
BAUS-4067	50	65	6165176.5	19155240	2.42	1	29.82	40.95	67.12	46.74	11.13	37.30	16.92
BAUS-5146	56	64	6177989	19128236	2.43	1	37.46	44.90	65.55	48.46	7.44	28.09	11.00
BAUS-4288	49	66	6166412.5	19162576	2.44	1	27.55	38.83	63.65	44.65	11.28	36.10	17.10
BAUS-5437	49	68	6171384	19168042	2.48	1	25.00	37.19	62.21	43.67	12.18	37.21	18.67
BAUS-4309	49	66	6166229.5	19162772	2.49	1	27.55	38.83	63.65	44.65	11.28	36.10	17.10
BAUS-4558	49	66	6166226	19162872	2.50	1	27.55	38.83	63.65	44.65	11.28	36.10	17.10

Table C-1
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 2 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4140	50	65	6164582	19154612	2.54	1	29.82	40.95	67.12	46.74	11.13	37.30	16.92
BAUS-5394	50	65	6164439	19155042	2.56	1	29.82	40.95	67.12	46.74	11.13	37.30	16.92
BAUS-5395C	50	65	6164439	19155042	2.56	1	29.82	40.95	67.12	46.74	11.13	37.30	16.92
BAUS-4321	49	66	6165863.5	19163164	2.58	1	27.55	38.83	63.65	44.65	11.28	36.10	17.10
BAUS-4314	49	66	6165765	19163464	2.63	1	27.55	38.83	63.65	44.65	11.28	36.10	17.10
BAUS-4495	49	66	6165427.5	19163046	2.64	1	27.55	38.83	63.65	44.65	11.28	36.10	17.10
BAUS-4541	49	66	6165427.5	19163046	2.64	1	27.55	38.83	63.65	44.65	11.28	36.10	17.10
6624102	51	64	6161925	19145490	2.65	1	31.83	41.81	66.89	46.91	9.98	35.06	15.07
BAUS-5425	51	65	6164243.5	19152214	2.71	1	30.98	42.91	71.99	49.25	11.93	41.01	18.27
BAUS-5344	49	67	6168874	19168294	2.78	1	26.38	38.48	64.18	44.85	12.10	37.80	18.47
BWLL-4987	53	72	6203934.5	19164638	2.85	1	21.42	30.59	48.14	35.32	9.17	26.72	13.90
BAUS-5251	49	66	6163571	19161666	2.86	1	27.55	38.83	63.65	44.65	11.28	36.10	17.10
BWLL-5574	53	72	6204376	19164880	2.95	1	21.42	30.59	48.14	35.32	9.17	26.72	13.90
BWLL-5666	53	72	6204376	19164880	2.95	1	21.42	30.59	48.14	35.32	9.17	26.72	13.90
BWLL-5671	53	72	6203411.5	19166926	3.05	1	21.42	30.59	48.14	35.32	9.17	26.72	13.90
BAUS-4315	50	65	6162008	19152698	3.09	1	29.82	40.95	67.12	46.74	11.13	37.30	16.92
6517418	57	67	6193783.5	19132988	3.16	1	32.38	40.43	60.43	44.33	8.06	28.05	11.95
6616810	48	67	6165870	19168340	3.17	1	24.82	35.05	56.41	40.24	10.23	31.59	15.42
BAUS-4001	50	64	6161187.5	19153480	3.21	1	30.51	39.96	62.81	44.68	9.45	32.30	14.17
BWLL-5144	54	72	6208083.5	19161954	3.32	1	21.16	29.61	46.03	33.87	8.44	24.86	12.71
6616808	48	67	6164696	19168372	3.33	1	24.82	35.05	56.41	40.24	10.23	31.59	15.42
BAUS-5369	50	64	6159339.5	19150220	3.40	1	30.51	39.96	62.81	44.68	9.45	32.30	14.17
6616807	48	67	6164759	19169286	3.44	1	24.82	35.05	56.41	40.24	10.23	31.59	15.42
BAUS-4165	50	64	6159584.5	19151498	3.47	1	30.51	39.96	62.81	44.68	9.45	32.30	14.17
BAUS-4332	56	63	6173628.5	19123240	3.49	1	39.44	46.02	64.51	49.04	6.58	25.07	9.60
BWLL-5283	54	73	6206956.5	19166268	3.50	1	19.14	25.70	38.22	28.83	6.56	19.08	9.60
BAUS-4272	49	65	6159772.5	19161124	3.53	1	28.43	38.45	61.25	43.48	10.02	32.82	15.04
BAUS-0025	48	67	6164912.5	19170116	3.53	1	24.82	35.05	56.41	40.24	10.23	31.59	15.42
6616905	49	70	6181892	19174892	3.54	1	21.68	31.75	51.19	37.02	10.08	29.52	15.34
6517416	57	68	6197967	19136210	3.56	1	30.17	38.33	57.64	42.30	8.16	27.47	12.13
BAUS-4251	48	66	6162705.5	19167810	3.56	1	25.93	35.62	56.50	40.46	9.70	30.57	14.53
BAUS-5354	50	64	6158858.5	19151168	3.56	1	30.51	39.96	62.81	44.68	9.45	32.30	14.17
BAUS-5388	57	63	6178570	19121956	3.62	1	40.64	46.47	62.82	49.06	5.83	22.18	8.42
BAUS-4446	56	63	6172414	19122690	3.65	1	39.44	46.02	64.51	49.04	6.58	25.07	9.60
BWLL-5099	50	71	6188851	19175126	3.66	1	21.58	31.54	50.41	36.76	9.96	28.83	15.18
BWLL-4914	48	69	6175618.5	19175966	3.68	1	21.98	31.59	50.57	36.51	9.62	28.59	14.54
BAUS-4103	48	66	6162497.5	19168714	3.70	1	25.93	35.62	56.50	40.46	9.70	30.57	14.53
BAUS-4482	48	65	6159595	19163650	3.70	1	26.74	35.49	54.89	39.74	8.75	28.15	13.00
BWLL-5083	51	72	6196246	19175092	3.72	1	21.24	30.30	47.29	34.97	9.06	26.05	13.73
BAUS-4046	49	65	6158552	19160778	3.74	1	28.43	38.45	61.25	43.48	10.02	32.82	15.04
6517506	57	70	6206333.5	19142652	3.77	1	24.81	32.16	48.23	35.72	7.35	23.42	10.91
BAUS-4330	56	63	6172527	19121986	3.77	1	39.44	46.02	64.51	49.04	6.58	25.07	9.60
BAUS-4499	50	64	6157484	19151120	3.79	1	30.51	39.96	62.81	44.68	9.45	32.30	14.17
BAUS-5172	49	65	6158516.5	19161790	3.79	1	28.43	38.45	61.25	43.48	10.02	32.82	15.04
BAUS-4197	48	69	6172692.5	19176572	3.89	1	21.98	31.59	50.57	36.51	9.62	28.59	14.54
BAUS-5427	48	65	6158124.5	19162332	3.89	1	26.74	35.49	54.89	39.74	8.75	28.15	13.00
BAUS-4554	50	64	6157482.5	19153652	3.90	1	30.51	39.96	62.81	44.68	9.45	32.30	14.17
BAUS-4244	48	69	6172513	19176666	3.92	1	21.98	31.59	50.57	36.51	9.62	28.59	14.54
BAUS-4245	48	69	6172513	19176666	3.92	1	21.98	31.59	50.57	36.51	9.62	28.59	14.54
BAUS-4381	48	65	6157883	19162274	3.93	1	26.74	35.49	54.89	39.74	8.75	28.15	13.00
BAUS-4161	56	63	6173447	19120904	3.93	1	39.44	46.02	64.51	49.04	6.58	25.07	9.60
BAUS-4377	50	64	6156590	19151494	3.97	1	30.51	39.96	62.81	44.68	9.45	32.30	14.17
BWLL-4902	51	72	6196194.5	19176508	3.98	1	21.24	30.30	47.29	34.97	9.06	26.05	13.73
BAUS-4002	49	64	6156882.5	19158188	3.98	1	29.01	37.63	57.82	41.83	8.63	28.82	12.83
BWLL-5712	52	73	6201356	19174950	4.03	1	19.91	27.38	41.31	31.07	7.46	21.39	11.15
BWLL-4901	51	72	6196531.5	19176924	4.07	1	21.24	30.30	47.29	34.97	9.06	26.05	13.73
BAUS-4106	48	69	6173004	19177696	4.09	1	21.98	31.59	50.57	36.51	9.62	28.59	14.54
BAUS-4326	49	64	6156076.5	19158564	4.14	1	29.01	37.63	57.82	41.83	8.63	28.82	12.83
6624105	49	64	6156073.5	19158552	4.14	1	29.01	37.63	57.82	41.83	8.63	28.82	12.83
BAUS-4130	50	63	6154803.5	19149710	4.17	1	30.94	38.85	58.38	42.65	7.90	27.44	11.71
BWLL-4479	54	73	6211756.5	19165026	4.18	1	19.14	25.70	38.22	28.83	6.56	19.08	9.69
BWLL-5046	48	70	6175780.5	19178808	4.21	1	20.45	28.99	45.38	33.30	8.54	24.93	12.85

Table C-1
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 3 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4440	56	62	6169492.5	19120560	4.22	1	41.08	46.77	62.95	49.30	5.69	21.87	8.23
BWLL-5107	50	72	6193152	19178698	4.31	1	20.62	28.91	44.31	33.11	8.29	23.69	12.49
BAUS-4478	50	63	6153445.5	19148244	4.34	1	30.94	38.85	58.38	42.65	7.90	27.44	11.71
6509803	55	73	6213403	19163354	4.36	1	18.16	24.06	35.54	26.81	5.90	17.38	8.64
BWLL-5036	50	72	6193462	19179040	4.37	1	20.62	28.91	44.31	33.11	8.29	23.69	12.49
BAUS-5365	49	64	6154709.5	19158668	4.40	1	29.01	37.63	57.82	41.83	8.63	28.82	12.83
BWLL-4586	50	72	6193187.5	19179334	4.43	1	20.62	28.91	44.31	33.11	8.29	23.69	12.49
BWLL-4957	50	72	6193187.5	19179334	4.43	1	20.62	28.91	44.31	33.11	8.29	23.69	12.49
BAUS-4231	49	64	6154315	19156072	4.46	1	29.01	37.63	57.82	41.83	8.63	28.82	12.83
BAUS-5178	54	61	6159714	19125378	4.47	1	38.11	43.70	59.32	46.20	5.59	21.21	8.09
BAUS-4433	47	68	6164433	19176176	4.48	1	21.72	30.14	47.04	34.27	8.42	25.32	12.55
BAUS-4555	49	64	6154125	19156470	4.49	1	29.01	37.63	57.82	41.83	8.63	28.82	12.83
BAUS-4323	49	64	6153822	19157574	4.55	1	29.01	37.63	57.82	41.83	8.63	28.82	12.83
BAUS-4215	49	64	6153833	19157270	4.55	1	29.01	37.63	57.82	41.83	8.63	28.82	12.83
BWLL-4273	49	72	6190162.5	19180238	4.60	1	19.67	26.96	40.42	30.57	7.29	20.75	10.90
BAUS-4100	47	67	6159614.5	19173068	4.64	1	22.85	31.28	48.65	35.38	8.43	25.79	12.53
BWLL-4020	50	72	6192689	19180938	4.72	1	20.62	28.91	44.31	33.11	8.29	23.69	12.49
BWLL-4510	54	74	6212934	19168918	4.72	1	17.17	22.30	32.00	24.62	5.13	14.83	7.45
BAUS-5408	57	62	6169281	19117216	4.82	1	42.21	47.32	61.80	49.51	5.11	19.60	7.30
BAUS-4331	54	60	6155456.5	19126140	4.96	1	38.10	42.74	55.70	44.71	4.64	17.60	6.60
BAUS-5307	55	61	6161433.5	19120750	4.97	1	40.14	45.44	60.36	47.75	5.29	20.21	7.60
BAUS-4322	49	63	6151606.5	19155470	4.98	1	29.34	36.61	54.07	40.04	7.28	24.73	10.70
BWLL-5404	49	72	6186798.5	19182242	5.05	1	19.67	26.96	40.42	30.57	7.29	20.75	10.90
BWLL-5720	48	70	6177109.5	19183434	5.07	1	20.45	28.99	45.38	33.30	8.54	24.93	12.85
BWLL-4968	52	74	6207057	19177918	5.08	1	18.79	24.47	34.96	27.12	5.68	16.16	8.32
BAUS-4151	47	64	6152060.5	19165106	5.14	1	25.21	31.73	46.32	34.70	6.52	21.11	9.49
BAUS-4240	47	66	6156685	19173776	5.15	1	23.91	32.00	49.12	35.87	8.09	25.21	11.96
BWLL-0046	50	73	6198713	19182270	5.15	1	19.73	26.41	38.65	29.66	6.68	18.93	9.93
BAUS-5332	46	67	6159231	19176600	5.17	1	20.52	27.28	41.00	30.42	6.76	20.48	9.90
BAUS-4095	46	67	6159387	19177010	5.20	1	20.52	27.28	41.00	30.42	6.76	20.48	9.90
BAUS-4361	48	64	6150553	19160396	5.22	1	27.25	34.87	52.26	38.47	7.62	25.01	11.22
BAUS-4252	46	66	6155967.5	19174154	5.30	1	21.43	27.92	41.42	30.88	6.49	19.99	9.44
BAUS-0023	58	62	6177353.5	19112740	5.37	1	43.03	47.54	60.25	49.39	4.50	17.22	6.35
6616701	46	66	6154947.5	19173422	5.37	1	21.43	27.92	41.42	30.88	6.49	19.99	9.44
BWLL-4175	47	70	6175471.5	19184974	5.38	1	18.87	25.87	39.21	29.26	7.00	20.34	10.39
BAUS-4157	55	60	6157945	19120556	5.39	1	40.00	44.40	56.83	46.21	4.40	16.83	6.22
BAUS-4229	52	60	6150139	19129496	5.45	1	34.07	38.81	51.56	40.84	4.73	17.48	6.77
BAUS-5374	47	64	6149640.5	19162492	5.46	1	25.21	31.73	46.32	34.70	6.52	21.11	9.49
BWLL-4391	50	73	6195988	19184602	5.48	1	19.73	26.41	38.65	29.66	6.68	18.93	9.93
BAUS-5320	46	66	6155757.5	19175638	5.51	1	21.43	27.92	41.42	30.88	6.49	19.99	9.44
BWLL-5619	49	73	6190846.5	19185114	5.51	1	18.98	24.93	35.74	27.75	5.94	16.76	8.76
6616408	46	67	6156879.5	19177938	5.66	1	20.52	27.28	41.00	30.42	6.76	20.48	9.90
BAUS-4533	49	61	6145912	19147068	5.70	1	28.78	33.72	46.02	35.87	4.94	17.24	7.09
BAUS-4441	46	66	6154841	19176140	5.71	1	21.43	27.92	41.42	30.88	6.49	19.99	9.44
6517505	59	70	6212777.5	19134288	5.75	1	24.81	29.75	40.86	31.93	4.95	16.06	7.13
BAUS-4312	47	65	6149991	19168882	5.76	1	24.67	32.05	48.08	35.49	7.37	23.41	10.82
BWLL-4388	47	71	6176538	19187140	5.78	1	17.90	23.98	35.29	26.85	6.07	17.39	8.95
BWLL-4841	55	75	6219268	19169050	5.79	1	13.90	17.70	24.93	19.29	3.80	11.02	5.39
BWLL-4199	48	72	6184208.5	19186706	5.81	1	18.50	24.71	36.11	27.68	6.20	17.60	9.17
BWLL-4019	48	72	6188877	19186572	5.81	1	18.50	24.71	36.11	27.68	6.20	17.60	9.17
BWLL-4198	48	72	6184296.5	19186710	5.82	1	18.50	24.71	36.11	27.68	6.20	17.60	9.17
BWLL-4271	54	75	6216897.5	19173622	5.84	1	15.54	19.68	27.45	21.45	4.15	11.91	5.91
BWLL-4668	46	69	6164915.5	19184902	5.88	1	18.23	24.51	36.65	27.45	6.27	18.42	9.21
BAUS-5321	46	66	6155203.5	19177898	5.88	1	21.43	27.92	41.42	30.88	6.49	19.99	9.44
BAUS-4209	47	64	6148873	19168134	5.90	1	25.21	31.73	46.32	34.70	6.52	21.11	9.49
BWLL-4844	54	75	6219097.5	19171272	5.96	1	15.54	19.68	27.45	21.45	4.15	11.91	5.91
BAUS-5366	59	62	6179431	19109360	6.01	1	43.74	47.66	58.69	49.20	3.92	14.95	5.46
BAUS-4284	46	67	6156156.5	19179906	6.02	1	20.52	27.28	41.00	30.42	6.76	20.48	9.90
BWLL-4146	47	71	6177018	19188474	6.03	1	17.90	23.98	35.29	26.85	6.07	17.39	8.95
6525104	60	65	6195083.5	19113996	6.05	1	39.37	43.68	55.07	45.44	4.31	15.70	6.07
BAUS-4111	49	62	6145119.5	19152104	6.05	1	29.16	35.19	49.96	37.92	6.03	20.79	8.76
6517806	60	67	6203449.5	19120438	6.10	1	34.33	38.91	50.27	40.84	4.58	15.94	6.51

Table C-1
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 4 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4320	46	67	6155152.5	19179796	6.14	1	20.52	27.28	41.00	30.42	6.76	20.48	9.90
BAUS-5210	46	66	6152520	19177072	6.16	1	21.43	27.92	41.42	30.88	6.49	19.99	9.44
BWLL-5048	50	74	6201355	19187026	6.16	1	19.04	24.30	33.84	26.73	5.27	14.81	7.69
BWLL-5244	47	71	6176659	19189290	6.18	1	17.90	23.98	35.29	26.85	6.07	17.39	8.95
BAUS-4219	47	63	6146183.5	19164496	6.18	1	25.35	30.96	43.81	33.44	5.61	18.46	8.08
BWLL-4997	48	73	6191791	19188702	6.19	1	17.93	23.02	32.22	25.36	5.09	14.29	7.43
BAUS-4179	51	60	6142840	19136634	6.33	1	32.15	36.75	48.88	38.72	4.60	16.73	6.58
BWLL-4481	51	75	6207214	19185620	6.34	1	18.40	22.79	30.75	24.71	4.39	12.36	6.31
BAUS-4501	47	63	6144274	19161188	6.42	1	25.35	30.96	43.81	33.44	5.61	18.46	8.08
BAUS-4546	45	66	6152776	19179814	6.46	1	19.71	24.98	35.84	27.25	5.27	16.14	7.55
BAUS-4096	45	66	6152178.5	19179288	6.48	1	19.71	24.98	35.84	27.25	5.27	16.14	7.55
BWLL-4362	53	59	6146703.5	19124416	6.50	1	35.64	39.51	50.15	41.09	3.87	14.52	5.45
BAUS-4194	45	66	6152336.5	19179800	6.52	1	19.71	24.98	35.84	27.25	5.27	16.14	7.55
BWLL-5633	46	72	6178922	19191884	6.67	1	15.67	19.77	27.22	21.58	4.10	11.55	5.91
BWLL-5316	48	73	6188437.5	19191416	6.73	1	17.93	23.02	32.22	25.36	5.09	14.29	7.43
BWLL-0050	54	76	6221764	19175320	6.78	1	13.42	16.73	22.88	18.06	3.31	9.46	4.64
6517615	59	73	6225327	19143954	6.79	1	13.12	16.30	22.93	17.61	3.18	9.81	4.49
6517612	59	73	6225327	19143954	6.79	1	13.12	16.30	22.93	17.61	3.18	9.81	4.49
BAUS-4058	55	59	6152213	19115596	6.80	1	39.34	42.95	53.17	44.37	3.60	13.83	5.03
BAUS-4317	53	59	6144949.5	19124152	6.81	1	35.64	39.51	50.15	41.09	3.87	14.52	5.45
BWLL-5218	47	73	6186841.5	19191764	6.83	1	16.77	21.01	28.67	22.90	4.24	11.90	6.13
BWLL-0014B	54	76	6222610.5	19174580	6.85	1	13.42	16.73	22.88	18.06	3.31	9.46	4.64
BAUS-4456	53	59	6145351.5	19122748	6.89	1	35.64	39.51	50.15	41.09	3.87	14.52	5.45
BAUS-4329	53	59	6145263	19122744	6.90	1	35.64	39.51	50.15	41.09	3.87	14.52	5.45
BWLL-4529	50	75	6206447	19189744	6.98	1	18.57	22.70	30.12	24.49	4.13	11.55	5.92
BWLL-4524	50	75	6206447	19189744	6.98	1	18.57	22.70	30.12	24.49	4.13	11.55	5.92
6623602	49	60	6138788.5	19144204	6.99	1	28.52	32.56	42.76	34.24	4.04	14.24	5.73
BWLL-5229	48	73	6190403.5	19193006	7.01	1	17.93	23.02	32.22	25.36	5.09	14.29	7.43
BWLL-5228	48	73	6190403.5	19193006	7.01	1	17.93	23.02	32.22	25.36	5.09	14.29	7.43
BWLL-5230	48	73	6190403.5	19193006	7.01	1	17.93	23.02	32.22	25.36	5.09	14.29	7.43
BWLL-5231	48	73	6190403.5	19193006	7.01	1	17.93	23.02	32.22	25.36	5.09	14.29	7.43
BWLL-5234	48	73	6190403.5	19193006	7.01	1	17.93	23.02	32.22	25.36	5.09	14.29	7.43
BWLL-5235	48	73	6190403.5	19193006	7.01	1	17.93	23.02	32.22	25.36	5.09	14.29	7.43
BWLL-5236	48	73	6190403.5	19193006	7.01	1	17.93	23.02	32.22	25.36	5.09	14.29	7.43
BWLL-5278	48	73	6190403.5	19193006	7.01	1	17.93	23.02	32.22	25.36	5.09	14.29	7.43
BWLL-0056	48	73	6190403.5	19193006	7.01	1	17.93	23.02	32.22	25.36	5.09	14.29	7.43
BWLL-4098	46	72	6180351	19193656	7.02	1	15.67	19.77	27.22	21.58	4.10	11.55	5.91
BAUS-4254	48	61	6139071	19148754	7.02	1	26.85	31.30	42.12	33.18	4.45	15.27	6.33
BAUS-4202	45	65	6145386.5	19174694	7.03	1	19.79	24.57	34.63	26.59	4.78	14.84	6.81
6525106	61	65	6198306	19109812	7.05	1	40.03	43.65	53.18	45.04	3.62	13.15	5.01
6616305	46	71	6175255.5	19193866	7.06	1	16.24	21.09	30.04	23.28	4.84	13.80	7.04
BWLL-0001D	54	76	6224553	19173702	7.08	1	13.42	16.73	22.88	18.06	3.31	9.46	4.64
BWLL-5560	50	76	6207148	19189986	7.08	1	18.11	21.31	27.01	22.59	3.20	8.91	4.49
BWLL-5583	50	76	6207148	19189986	7.08	1	18.11	21.31	27.01	22.59	3.20	8.91	4.49
BWLL-5705	50	76	6207148	19189986	7.08	1	18.11	21.31	27.01	22.59	3.20	8.91	4.49
BAUS-4287	48	61	6139321	19151700	7.09	1	26.85	31.30	42.12	33.18	4.45	15.27	6.33
BWLL-5093	50	76	6206153.5	19190542	7.10	1	18.11	21.31	27.01	22.59	3.20	8.91	4.49
BWLL-4001	50	76	6206776	19190364	7.11	1	18.11	21.31	27.01	22.59	3.20	8.91	4.49
BWLL-5523	49	75	6202579.5	19192032	7.13	1	18.27	21.99	28.61	23.56	3.71	10.34	5.29
BWLL-4387	46	71	6173820.5	19194232	7.15	1	16.24	21.09	30.04	23.28	4.84	13.80	7.04
BWLL-5260	49	75	6202931	19192046	7.15	1	18.27	21.99	28.61	23.56	3.71	10.34	5.29
BWLL-4427	47	73	6189667.5	19193892	7.18	1	16.77	21.01	28.67	22.90	4.24	11.90	6.13
BWLL-5047	49	75	6203183.5	19192358	7.22	1	18.27	21.99	28.61	23.56	3.71	10.34	5.29
BAUS-4164	54	58	6147398	19117150	7.23	1	36.61	39.69	48.27	40.87	3.09	11.66	4.26
BAUS-4369	49	60	6137283	19144440	7.28	1	28.52	32.56	42.76	34.24	4.04	14.24	5.73
BWLL-4753	54	77	6223802.5	19177320	7.31	1	10.84	13.45	18.28	14.44	2.61	7.44	3.60
BWLL-4655	49	75	6202275.5	19193136	7.32	1	18.27	21.99	28.61	23.56	3.71	10.34	5.29
BAUS-4313	48	60	6137047.5	19146152	7.34	1	26.64	30.29	39.29	31.77	3.65	12.65	5.13
BWLL-4599	49	75	6202890.5	19193158	7.35	1	18.27	21.99	28.61	23.56	3.71	10.34	5.29
BWLL-4656	49	75	6201913	19193426	7.35	1	18.27	21.99	28.61	23.56	3.71	10.34	5.29
BAUS-5288	54	58	6148317	19114972	7.39	1	36.61	39.69	48.27	40.87	3.09	11.66	4.26
BAUS-4078	48	61	6137790.5	19152660	7.42	1	26.85	31.30	42.12	33.18	4.45	15.27	6.33

Table C-1
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 5 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BWLL-4660	49	75	6202868	19193764	7.46	1	18.27	21.99	28.61	23.56	3.71	10.34	5.29
BWLL-4227	53	77	6222451.5	19180512	7.46	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4113	53	77	6222902.5	19180224	7.50	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4304	53	77	6222433	19181016	7.52	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4181	53	77	6222891	19180528	7.53	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-5210	49	75	6202498.5	19194258	7.53	1	18.27	21.99	28.61	23.56	3.71	10.34	5.29
BWLL-4297	45	71	6169373.5	19195592	7.54	1	14.50	18.23	25.03	19.83	3.73	10.54	5.34
BWLL-4405	54	77	6224743	19178064	7.54	1	10.84	13.45	18.28	14.44	2.61	7.44	3.60
BAUS-4066	47	62	6138023	19158642	7.55	1	25.14	29.86	40.89	31.87	4.71	15.75	6.73
BWLL-4265	53	77	6222608.5	19181024	7.55	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4570	53	77	6223437	19180042	7.55	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BAUS-4075	47	62	6138002	19159248	7.56	1	25.14	29.86	40.89	31.87	4.71	15.75	6.73
BAUS-4297	46	72	6178346	19196654	7.57	1	15.67	19.77	27.22	21.58	4.10	11.55	5.91
BWLL-4590	49	75	6202934	19194374	7.58	1	18.27	21.99	28.61	23.56	3.71	10.34	5.29
BAUS-4230	47	61	6136978	19153238	7.59	1	24.76	28.63	37.88	30.23	3.88	13.12	5.47
BWLL-4127	53	77	6223052	19180938	7.60	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4299	54	77	6225373.5	19177684	7.60	1	10.84	13.45	18.28	14.44	2.61	7.44	3.60
BWLL-4114	53	77	6222864.5	19181236	7.61	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-5339	53	77	6222956.5	19181138	7.61	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4128	53	77	6223876.5	19180058	7.62	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4017	53	77	6224063.5	19179760	7.62	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4014	53	77	6223972	19179858	7.62	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
6510715	57	76	6231432	19161984	7.63	1	7.27	9.73	14.53	10.69	2.46	7.26	3.42
BWLL-4264	53	77	6223319	19180848	7.63	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4262	54	77	6225736	19177392	7.63	1	10.84	13.45	18.28	14.44	2.61	7.44	3.60
6517614	60	73	6228549	19139770	7.65	1	11.95	14.58	20.14	15.62	2.63	8.19	3.68
BWLL-4308	53	77	6224144	19179966	7.65	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BAUS-4472	48	60	6135298.5	19145788	7.67	1	26.64	30.29	39.29	31.77	3.65	12.65	5.13
BWLL-4614	49	75	6202556.5	19195070	7.68	1	18.27	21.99	28.61	23.56	3.71	10.34	5.29
BWLL-4180	53	77	6224041	19180368	7.68	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4294	53	77	6223671	19180860	7.68	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BAUS-5154	47	62	6137316	19158718	7.69	1	25.14	29.86	40.89	31.87	4.71	15.75	6.73
BWLL-4058	53	77	6224133	19180270	7.69	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4266	54	77	6224686.5	19179582	7.69	1	10.84	13.45	18.28	14.44	2.61	7.44	3.60
BWLL-4179	53	77	6224030	19180672	7.72	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4034	54	77	6224862.5	19179588	7.72	1	10.84	13.45	18.28	14.44	2.61	7.44	3.60
BWLL-5165	49	76	6202725	19195278	7.73	1	18.11	20.99	26.10	22.14	2.88	7.98	4.02
BWLL-4225	54	77	6224847	19179992	7.76	1	10.84	13.45	18.28	14.44	2.61	7.44	3.60
BWLL-4279	53	77	6224477	19180486	7.76	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4380	53	77	6223831.5	19181272	7.76	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4566	53	77	6223831.5	19181272	7.76	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4797	55	77	6227917.5	19175550	7.81	1	8.53	10.95	15.51	11.87	2.42	6.98	3.34
BWLL-4916	53	77	6224271	19181288	7.82	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-5324	47	73	6186384	19197114	7.83	1	16.77	21.01	28.67	22.90	4.24	11.90	6.13
BWLL-4990	52	77	6218864.5	19187062	7.83	1	15.05	17.78	22.73	18.82	2.73	7.68	3.77
BWLL-4018	54	77	6225195	19180106	7.83	1	10.84	13.45	18.28	14.44	2.61	7.44	3.60
BWLL-4359	53	77	6224450.5	19181194	7.84	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4226	54	77	6225096	19180408	7.85	1	10.84	13.45	18.28	14.44	2.61	7.44	3.60
BWLL-4016	53	77	6224813.5	19180902	7.86	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4059	54	77	6225271.5	19180414	7.88	1	10.84	13.45	18.28	14.44	2.61	7.44	3.60
BWLL-4060	54	77	6225271.5	19180414	7.88	1	10.84	13.45	18.28	14.44	2.61	7.44	3.60
BWLL-0014A	55	77	6229109.5	19174278	7.90	1	8.53	10.95	15.51	11.87	2.42	6.98	3.34
BAUS-5159	47	61	6136060	19156852	7.91	1	24.76	28.63	37.88	30.23	3.88	13.12	5.47
BAUS-4356	49	59	6133777	19141382	7.94	1	28.31	31.62	40.05	32.93	3.31	11.74	4.62
BWLL-4088	54	77	6225898	19180134	7.94	1	10.84	13.45	18.28	14.44	2.61	7.44	3.60
BWLL-4447	53	77	6225241.5	19181222	7.96	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4126	53	77	6225329.5	19181226	7.98	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4407	53	77	6225604.5	19180932	7.98	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4282	54	77	6226062.5	19180444	8.00	1	10.84	13.45	18.28	14.44	2.61	7.44	3.60
6525105	62	65	6201528	19105630	8.04	1	40.59	43.63	51.59	44.71	3.04	11.00	4.12
BWLL-4228	53	77	6225853	19181346	8.07	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78
BWLL-4012	53	77	6226028.5	19181354	8.10	1	13.18	15.92	20.92	16.96	2.73	7.73	3.78

Table C-1
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 6 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4394	44	64	6139451.5	19175804	8.13	1	17.14	20.40	27.33	21.69	3.27	10.20	4.56
6518103	58	76	6234654	19157800	8.16	1	5.40	7.54	11.79	8.37	2.14	6.39	2.96
6518406	60	74	6232732	19142992	8.17	1	8.76	11.00	15.65	11.86	2.23	6.88	3.10
BAUS-5433	45	63	6137554	19171998	8.17	1	19.77	23.40	31.43	24.88	3.63	11.66	5.11
BWLL-4482	48	76	6202617.5	19198212	8.26	1	17.58	20.08	24.46	21.04	2.49	6.88	3.45
BAUS-5362	44	64	6139628	19178494	8.34	1	17.14	20.40	27.33	21.69	3.27	10.20	4.56
BAUS-4308	44	64	6137869	19175750	8.39	1	17.14	20.40	27.33	21.69	3.27	10.20	4.56
6615902	45	63	6136149	19171854	8.40	1	19.77	23.40	31.43	24.88	3.63	11.66	5.11
6509106	46	74	6188481	19200322	8.41	1	15.18	17.91	22.77	19.03	2.74	7.60	3.85
BWLL-5718	56	77	6233042.5	19172732	8.46	1	6.33	8.54	12.77	9.38	2.22	6.44	3.05
BWLL-4263	54	78	6229601	19179968	8.51	1	7.87	9.91	13.68	10.65	2.04	5.80	2.77
BAUS-4228	48	58	6129578	19140528	8.74	1	26.43	28.89	35.11	29.79	2.46	8.69	3.37
BAUS-4544	45	62	6133072	19169406	8.82	1	19.76	22.87	29.91	24.10	3.11	10.15	4.34
BWLL-4969	45	73	6182724.5	19203464	8.91	1	13.76	16.36	21.01	17.43	2.61	7.26	3.67
6518404	61	74	6235954	19138808	9.01	1	7.81	9.64	13.52	10.33	1.84	5.72	2.52
BAUS-4319	46	60	6129618	19154706	9.01	1	22.40	25.11	31.57	26.14	2.71	9.17	3.74
6518403	61	74	6235954	19138808	9.01	1	7.81	9.64	13.52	10.33	1.84	5.72	2.52
6525209	63	66	6208933	19104668	9.03	1	38.58	41.17	47.82	42.05	2.60	9.24	3.48
6525218	63	66	6208933	19104668	9.03	1	38.58	41.17	47.82	42.05	2.60	9.24	3.48
6525219	63	66	6208933	19104668	9.03	1	38.58	41.17	47.82	42.05	2.60	9.24	3.48
6525220	63	65	6204749.5	19101448	9.04	1	41.00	43.54	50.16	44.38	2.53	9.16	3.37
6525221	63	65	6204749.5	19101448	9.04	1	41.00	43.54	50.16	44.38	2.53	9.16	3.37
6525210	63	65	6204749.5	19101448	9.04	1	41.00	43.54	50.16	44.38	2.53	9.16	3.37
BAUS-4072	45	62	6131531.5	19168138	9.04	1	19.76	22.87	29.91	24.10	3.11	10.15	4.34
BAUS-4131	48	58	6128001.5	19140272	9.04	1	26.43	28.89	35.11	29.79	2.46	8.69	3.37
6525202	63	67	6213116	19107890	9.08	1	35.63	38.23	44.74	39.13	2.60	9.11	3.50
6525203	63	67	6213116	19107890	9.08	1	35.63	38.23	44.74	39.13	2.60	9.11	3.50
BAUS-4291	45	61	6130616.5	19166588	9.14	1	19.77	22.40	28.48	23.41	2.63	8.70	3.63
BWLL-5331	46	74	6188675.5	19204286	9.16	1	15.18	17.91	22.77	19.03	2.74	7.60	3.85
BAUS-4217	45	61	6130444.5	19166480	9.17	1	19.77	22.40	28.48	23.41	2.63	8.70	3.63
BAUS-4305	45	61	6130444.5	19166480	9.17	1	19.77	22.40	28.48	23.41	2.63	8.70	3.63
BAUS-4218	45	61	6130444.5	19166480	9.17	1	19.77	22.40	28.48	23.41	2.63	8.70	3.63
BAUS-4195	45	61	6130275.5	19166272	9.19	1	19.77	22.40	28.48	23.41	2.63	8.70	3.63
BWLL-4511	53	79	6228988.5	19186932	9.19	1	7.35	9.02	12.05	9.59	1.67	4.71	2.24
BAUS-5306	45	61	6130250.5	19166582	9.21	1	19.77	22.40	28.48	23.41	2.63	8.70	3.63
BAUS-5377	45	61	6130250.5	19166582	9.21	1	19.77	22.40	28.48	23.41	2.63	8.70	3.63
BAUS-4532	48	58	6127012.5	19140844	9.22	1	26.43	28.89	35.11	29.79	2.46	8.69	3.37
6525301	63	68	6217299	19111112	9.23	1	32.28	34.81	41.02	35.71	2.53	8.74	3.43
BAUS-5181	45	61	6130085.5	19166670	9.24	1	19.77	22.40	28.48	23.41	2.63	8.70	3.63
BAUS-4463	45	61	6129853.5	19165750	9.25	1	19.77	22.40	28.48	23.41	2.63	8.70	3.63
BWLL-5038	52	79	6226942.5	19189894	9.27	1	10.15	11.82	14.80	12.37	1.67	4.65	2.22
BAUS-5371	45	61	6129745	19166062	9.28	1	19.77	22.40	28.48	23.41	2.63	8.70	3.63
BWLL-4560	52	79	6225465	19191764	9.33	1	10.15	11.82	14.80	12.37	1.67	4.65	2.22
BWLL-5368	53	79	6229497	19187458	9.33	1	7.35	9.02	12.05	9.59	1.67	4.71	2.24
BAUS-5439	45	61	6129458.5	19166208	9.34	1	19.77	22.40	28.48	23.41	2.63	8.70	3.63
BAUS-4166	44	62	6129924.5	19168790	9.36	1	16.71	19.08	24.37	19.98	2.37	7.67	3.27
BWLL-5377	52	79	6225996	19191682	9.38	1	10.15	11.82	14.80	12.37	1.67	4.65	2.22
BWLL-4212	46	75	6189681.5	19205640	9.41	1	15.19	17.33	21.12	18.17	2.15	5.93	2.98
BAUS-4363	46	60	6127131	19155328	9.50	1	22.40	25.11	31.57	26.14	2.71	9.17	3.74
BAUS-4037	48	58	6125454	19142614	9.51	1	26.43	28.89	35.11	29.79	2.46	8.69	3.37
BWLL-4239	55	79	6237373	19176916	9.53	1	2.07	3.60	6.44	4.13	1.52	4.36	2.05
BWLL-4562	52	79	6227130.5	19191926	9.57	1	10.15	11.82	14.80	12.37	1.67	4.65	2.22
BWLL-4898	53	79	6232263	19186448	9.62	1	7.35	9.02	12.05	9.59	1.67	4.71	2.24
BWLL-5566	52	79	6227068	19192974	9.70	1	10.15	11.82	14.80	12.37	1.67	4.65	2.22
6623205	45	60	6126611.5	19158036	9.71	1	19.96	22.18	27.41	23.00	2.22	7.45	3.04
BWLL-5656	53	79	6232524.5	19187068	9.73	1	7.35	9.02	12.05	9.59	1.67	4.71	2.24
BWLL-5063	51	79	6224348	19195772	9.76	1	12.53	14.14	16.97	14.65	1.60	4.44	2.12
BWLL-5602	52	79	6228469	19192130	9.78	1	10.15	11.82	14.80	12.37	1.67	4.65	2.22
BWLL-5148	50	79	6221156.5	19198794	9.85	1	14.45	15.92	18.50	16.38	1.47	4.05	1.93
BAUS-5364	48	57	6123778	19139626	9.85	1	26.27	28.30	33.48	29.01	2.03	7.20	2.73
BWLL-5655	53	79	6233317.5	19187106	9.85	1	7.35	9.02	12.05	9.59	1.67	4.71	2.24
BWLL-5657	53	79	6233273	19187104	9.85	1	7.35	9.02	12.05	9.59	1.67	4.71	2.24

Table C-1
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 7 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BWLL-5658	53	79	6233273	19187104	9.85	1	7.35	9.02	12.05	9.59	1.67	4.71	2.24
6510813	58	78	6243020.5	19164244	9.86	1	-0.19	1.22	3.97	1.73	1.41	4.16	1.91
6510814	58	78	6243020.5	19164244	9.86	1	-0.19	1.22	3.97	1.73	1.41	4.16	1.91
BWLL-4662	50	79	6221947	19198822	9.94	1	14.45	15.92	18.50	16.38	1.47	4.05	1.93
BWLL-4276	50	79	6221947	19198822	9.94	1	14.45	15.92	18.50	16.38	1.47	4.05	1.93
BWLL-5605	43	73	6173644.5	19209052	9.95	1	10.01	11.29	13.56	11.78	1.29	3.55	1.77
BAUS-4189	43	62	6127509.5	19172454	9.99	1	13.27	14.96	18.67	15.57	1.68	5.40	2.30

Table C-2
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 1 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-5429	54	66	6180054.5	19142336	0.15	1	43.19	52.65	77.22	57.74	9.46	34.04	14.55
BAUS-5430	54	66	6180054.5	19142336	0.15	1	43.19	52.65	77.22	57.74	9.46	34.04	14.55
BWLL-5117	53	69	6191012.5	19154344	0.34	1	38.92	50.75	74.91	57.34	11.83	35.99	18.41
BWLL-5481	53	70	6191500	19157906	0.36	1	37.99	48.31	69.16	53.94	10.32	31.17	15.95
BWLL-5006	54	69	6190699	19153424	0.46	1	39.23	49.27	70.69	54.75	10.04	31.46	15.51
BAUS-4159	53	66	6177818.5	19144046	0.47	1	42.29	53.21	80.24	59.19	10.92	37.95	16.9
BAUS-4158	53	66	6177811.5	19144248	0.49	1	42.29	53.21	80.24	59.19	10.92	37.95	16.9
BWLL-5541	52	69	6186065.5	19157628	0.5	1	38.65	51.57	77.57	58.78	12.91	38.92	20.13
BWLL-5541	53	69	6188533	19157786	0.54	1	38.92	50.75	74.91	57.34	11.83	35.99	18.41
BWLL-5543	52	69	6186496.5	19157650	0.56	1	38.65	51.57	77.57	58.78	12.91	38.92	20.13
BAUS-4458	51	67	6175604	19159156	0.63	1	39.87	53.04	81.27	60.33	13.17	41.4	20.45
BWLL-4133	51	67	6175182.5	19158636	0.63	1	39.87	53.04	81.27	60.33	13.17	41.4	20.45
BAUS-5436	51	67	6174074	19157298	0.72	1	39.87	53.04	81.27	60.33	13.17	41.4	20.45
BAUS-5447	51	67	6173795	19157412	0.78	1	39.87	53.04	81.27	60.33	13.17	41.4	20.45
BAUS-4340	53	65	6171277.5	19142192	0.84	1	43.58	53.13	78.3	58.23	9.55	34.72	14.65
BWLL-4363	52	69	6186773	19159558	0.88	1	38.65	51.57	77.57	58.78	12.91	38.92	20.13
BAUS-5426	51	67	6173430.5	19159360	0.98	1	39.87	53.04	81.27	60.33	13.17	41.4	20.45
BAUS-5401	51	67	6172709	19157480	0.99	1	39.87	53.04	81.27	60.33	13.17	41.4	20.45
BAUS-5398	51	66	6171645	19154492	1.25	1	40.91	52.79	79.78	59.27	11.89	38.87	18.36
BAUS-4236	50	67	6173220	19161806	1.31	1	39.08	51.21	77.11	57.78	12.13	38.02	18.7
6517415	55	67	6187339.5	19141354	1.34	1	42.48	51.04	72.03	55.59	8.56	29.55	13.11
BAUS-4485	50	67	6172028.5	19160648	1.34	1	39.08	51.21	77.11	57.78	12.13	38.02	18.7
BAUS-4325	50	67	6172780	19161790	1.36	1	39.08	51.21	77.11	57.78	12.13	38.02	18.7
BAUS-4518	50	68	6174657	19163476	1.42	1	38.04	50.4	75.87	57.11	12.36	37.83	19.07
BAUS-5298	50	67	6172278	19161868	1.44	1	39.08	51.21	77.11	57.78	12.13	38.02	18.7
BAUS-4515	51	66	6170610	19153510	1.5	1	40.91	52.79	79.78	59.27	11.89	38.87	18.36
BAUS-4519	50	68	6175159	19164204	1.52	1	38.04	50.4	75.87	57.11	12.36	37.83	19.07
BAUS-5397	51	66	6169866.5	19155934	1.52	1	40.91	52.79	79.78	59.27	11.89	38.87	18.36
BAUS-0002A	50	68	6175328	19164412	1.54	1	38.04	50.4	75.87	57.11	12.36	37.83	19.07
BAUS-0002B	50	68	6175328	19164412	1.54	1	38.04	50.4	75.87	57.11	12.36	37.83	19.07
BAUS-5400	50	67	6171322	19161498	1.54	1	39.08	51.21	77.11	57.78	12.13	38.02	18.7
BAUS-5402	50	67	6170748.5	19160828	1.56	1	39.08	51.21	77.11	57.78	12.13	38.02	18.7
BWLL-5690	51	69	6184161	19164328	1.65	1	38.06	50.75	76.22	57.75	12.69	38.16	19.69
BAUS-4430	50	66	6168784	19157800	1.73	1	39.94	51.1	76	57.07	11.16	36.06	17.13
BAUS-4185	52	66	6170700	19150982	1.73	1	41.55	53.49	81.41	60.05	11.93	39.86	18.5
BAUS-5399	50	66	6168767	19157550	1.73	1	39.94	51.1	76	57.07	11.16	36.06	17.13
BWLL-4303	50	68	6177915	19165922	1.75	1	38.04	50.4	75.87	57.11	12.36	37.83	19.07
6509702	52	71	6193335.5	19165170	1.76	1	37.82	47.56	66.82	52.78	9.74	29	14.96
BAUS-4429	50	66	6168601	19157996	1.77	1	39.94	51.1	76	57.07	11.16	36.06	17.13
BAUS-5297	50	68	6173472	19165068	1.79	1	38.04	50.4	75.87	57.11	12.36	37.83	19.07
BAUS-4129	55	65	6178444	19131512	1.81	1	45.79	53.16	73.11	56.96	7.37	27.32	11.17
BWLL-4992	50	68	6177988.5	19166330	1.83	1	38.04	50.4	75.87	57.11	12.36	37.83	19.07
BWLL-4272	50	68	6177805.5	19166526	1.87	1	38.04	50.4	75.87	57.11	12.36	37.83	19.07
BAUS-0024	56	65	6179473	19131326	1.87	1	46.71	53.08	70.2	56.28	6.37	23.49	9.57
BWLL-5674	51	69	6184132.5	19165744	1.92	1	38.06	50.75	76.22	57.75	12.69	38.16	19.69
BWLL-4161	50	69	6177699	19167028	1.96	1	36.97	48.7	72.29	55.04	11.73	35.32	18.07
BAUS-4299	50	69	6178487	19167158	1.99	1	36.97	48.7	72.29	55.04	11.73	35.32	18.07
BWLL-5082	51	69	6183630	19166128	1.99	1	38.06	50.75	76.22	57.75	12.69	38.16	19.69
BAUS-4138	51	65	6166124	19148388	2.1	1	41.84	52.15	76.88	57.64	10.31	35.05	15.8
6624203	51	65	6166932	19150042	2.15	1	41.84	52.15	76.88	57.64	10.31	35.05	15.8
BWLL-4134	52	71	6197009.5	19166208	2.19	1	37.82	47.56	66.82	52.78	9.74	29	14.96
BAUS-4137	51	65	6165560.5	19149382	2.29	1	41.84	52.15	76.88	57.64	10.31	35.05	15.8
BAUS-5120	50	66	6166456	19161362	2.33	1	39.94	51.1	76	57.07	11.16	36.06	17.13
BAUS-4552	49	66	6166768	19162486	2.37	1	38.74	48.85	71.15	54.11	10.1	32.41	15.36
BAUS-4235	49	66	6166764.5	19162588	2.38	1	38.74	48.85	71.15	54.11	10.1	32.41	15.36
BAUS-4324	49	66	6166588.5	19162582	2.41	1	38.74	48.85	71.15	54.11	10.1	32.41	15.36
BAUS-4067	50	65	6165176.5	19155240	2.42	1	40.66	50.48	73.43	55.62	9.82	32.77	14.96
BAUS-5146	56	64	6177989	19128236	2.43	1	48.85	54.68	70.71	57.54	5.83	21.86	8.69
BAUS-4288	49	66	6166412.5	19162576	2.44	1	38.74	48.85	71.15	54.11	10.1	32.41	15.36
BAUS-5437	49	68	6171384	19168042	2.48	1	37.05	48.05	70.74	53.86	11	33.69	16.81
BAUS-4309	49	66	6166229.5	19162772	2.49	1	38.74	48.85	71.15	54.11	10.1	32.41	15.36
BAUS-4558	49	66	6166226	19162872	2.5	1	38.74	48.85	71.15	54.11	10.1	32.41	15.36

Table C-2
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 2 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4140	50	65	6164582	19154612	2.54	1	40.66	50.48	73.43	55.62	9.82	32.77	14.96
BAUS-5394	50	65	6164439	19155042	2.56	1	40.66	50.48	73.43	55.62	9.82	32.77	14.96
BAUS-5395C	50	65	6164439	19155042	2.56	1	40.66	50.48	73.43	55.62	9.82	32.77	14.96
BAUS-4321	49	66	6165863.5	19163164	2.58	1	38.74	48.85	71.15	54.11	10.1	32.41	15.36
BAUS-4314	49	66	6165765	19163464	2.63	1	38.74	48.85	71.15	54.11	10.1	32.41	15.36
BAUS-4495	49	66	6165427.5	19163046	2.64	1	38.74	48.85	71.15	54.11	10.1	32.41	15.36
BAUS-4541	49	66	6165427.5	19163046	2.64	1	38.74	48.85	71.15	54.11	10.1	32.41	15.36
6624102	51	64	6161925	19145490	2.65	1	42.7	51.41	73.26	55.92	8.71	30.57	13.23
BAUS-5425	51	65	6164243.5	19152214	2.71	1	41.84	52.15	76.88	57.64	10.31	35.05	15.8
BAUS-5344	49	67	6168874	19168294	2.78	1	37.96	48.82	71.89	54.53	10.85	33.93	16.57
BWLL-4987	53	72	6203934.5	19164638	2.85	1	36.43	44.32	60.1	48.42	7.88	23.67	11.99
BAUS-5251	49	66	6163571	19161666	2.86	1	38.74	48.85	71.15	54.11	10.1	32.41	15.36
BWLL-5574	53	72	6204376	19164880	2.95	1	36.43	44.32	60.1	48.42	7.88	23.67	11.99
BWLL-5666	53	72	6204376	19164880	2.95	1	36.43	44.32	60.1	48.42	7.88	23.67	11.99
BWLL-5671	53	72	6203411.5	19166926	3.05	1	36.43	44.32	60.1	48.42	7.88	23.67	11.99
BAUS-4315	50	65	6162008	19152698	3.09	1	40.66	50.48	73.43	55.62	9.82	32.77	14.96
6517418	57	67	6193783.5	19132988	3.16	1	42.22	48.31	63.49	51.35	6.09	21.27	9.13
6616810	48	67	6165870	19168340	3.17	1	36.53	46	66.06	50.81	9.46	29.53	14.27
BAUS-4001	50	64	6161187.5	19153480	3.21	1	41.36	49.75	70.18	54.03	8.39	28.81	12.67
BWLL-5144	54	72	6208083.5	19161954	3.32	1	34.88	41.97	56.46	45.61	7.08	21.57	10.73
6616808	48	67	6164696	19168372	3.33	1	36.53	46	66.06	50.81	9.46	29.53	14.27
BAUS-5369	50	64	6159339.5	19150220	3.4	1	41.36	49.75	70.18	54.03	8.39	28.81	12.67
6616807	48	67	6164759	19169286	3.44	1	36.53	46	66.06	50.81	9.46	29.53	14.27
BAUS-4165	50	64	6159584.5	19151498	3.47	1	41.36	49.75	70.18	54.03	8.39	28.81	12.67
BAUS-4332	56	63	6173628.5	19123240	3.49	1	51.3	56.61	71.49	59.15	5.31	20.2	7.85
BWLL-5283	54	73	6206956.5	19166268	3.5	1	32.99	39.08	51.48	42.12	6.09	18.5	9.13
BAUS-4272	49	65	6159772.5	19161124	3.53	1	39.36	48.37	69.07	52.98	9.01	29.71	13.61
BAUS-0025	48	67	6164912.5	19170116	3.53	1	36.53	46	66.06	50.81	9.46	29.53	14.27
6616905	49	70	6181892	19174892	3.54	1	35.7	45.36	64.48	50.36	9.66	28.78	14.66
6517416	57	68	6197967	19136210	3.56	1	41.19	47.4	62.32	50.53	6.22	21.13	9.35
BAUS-4251	48	66	6162705.5	19167810	3.56	1	37.28	46.19	65.72	50.68	8.91	28.44	13.4
BAUS-5354	50	64	6158858.5	19151168	3.56	1	41.36	49.75	70.18	54.03	8.39	28.81	12.67
BAUS-5388	57	63	6178570	19121956	3.62	1	52.18	56.91	70.01	59.11	4.73	17.83	6.93
BAUS-4446	56	63	6172414	19122690	3.65	1	51.3	56.61	71.49	59.15	5.31	20.2	7.85
BWLL-5099	50	71	6188851	19175126	3.66	1	36.82	46.17	64.42	51.03	9.34	27.6	14.21
BWLL-4914	48	69	6175618.5	19175966	3.68	1	34.9	44.1	62.7	48.78	9.2	27.8	13.88
BAUS-4103	48	66	6162497.5	19168714	3.7	1	37.28	46.19	65.72	50.68	8.91	28.44	13.4
BAUS-4482	48	65	6159595	19163650	3.7	1	37.87	45.91	64.15	49.9	8.04	26.29	12.03
BWLL-5083	51	72	6196246	19175092	3.72	1	37.63	45.95	62.16	50.24	8.32	24.53	12.61
BAUS-4046	49	65	6158552	19160778	3.74	1	39.36	48.37	69.07	52.98	9.01	29.71	13.61
6517506	57	70	6206333.5	19142652	3.77	1	38.35	44.27	57.63	47.22	5.92	19.28	8.87
BAUS-4330	56	63	6172527	19121986	3.77	1	51.3	56.61	71.49	59.15	5.31	20.2	7.85
BAUS-4499	50	64	6157484	19151120	3.79	1	41.36	49.75	70.18	54.03	8.39	28.81	12.67
BAUS-5172	49	65	6158516.5	19161790	3.79	1	39.36	48.37	69.07	52.98	9.01	29.71	13.61
BAUS-4197	48	69	6172692.5	19176572	3.89	1	34.9	44.1	62.7	48.78	9.2	27.8	13.88
BAUS-5427	48	65	6158124.5	19162332	3.89	1	37.87	45.91	64.15	49.9	8.04	26.29	12.03
BAUS-4554	50	64	6157482.5	19153652	3.9	1	41.36	49.75	70.18	54.03	8.39	28.81	12.67
BAUS-4244	48	69	6172513	19176666	3.92	1	34.9	44.1	62.7	48.78	9.2	27.8	13.88
BAUS-4245	48	69	6172513	19176666	3.92	1	34.9	44.1	62.7	48.78	9.2	27.8	13.88
BAUS-4381	48	65	6157883	19162274	3.93	1	37.87	45.91	64.15	49.9	8.04	26.29	12.03
BAUS-4161	56	63	6173447	19120904	3.93	1	51.3	56.61	71.49	59.15	5.31	20.2	7.85
BAUS-4377	50	64	6156590	19151494	3.97	1	41.36	49.75	70.18	54.03	8.39	28.81	12.67
BWLL-4902	51	72	6196194.5	19176508	3.98	1	37.63	45.95	62.16	50.24	8.32	24.53	12.61
BAUS-4002	49	64	6156882.5	19158188	3.98	1	39.99	47.77	66.35	51.66	7.79	26.36	11.68
BWLL-5712	52	73	6201356	19174950	4.03	1	38.3	45.19	58.7	48.64	6.88	20.39	10.34
BWLL-4901	51	72	6196531.5	19176924	4.07	1	37.63	45.95	62.16	50.24	8.32	24.53	12.61
BAUS-4106	48	69	6173004	19177696	4.09	1	34.9	44.1	62.7	48.78	9.2	27.8	13.88
BAUS-4326	49	64	6156076.5	19158564	4.14	1	39.99	47.77	66.35	51.66	7.79	26.36	11.68
6624105	49	64	6156073.5	19158552	4.14	1	39.99	47.77	66.35	51.66	7.79	26.36	11.68
BAUS-4130	50	63	6154803.5	19149710	4.17	1	41.86	48.88	66.58	52.35	7.02	24.73	10.5
BWLL-4479	54	73	6211756.5	19165026	4.18	1	32.99	39.08	51.48	42.12	6.09	18.5	9.13
BWLL-5046	48	70	6175780.5	19178808	4.21	1	34.36	42.87	59.75	47.14	8.51	25.39	12.77

Table C-2
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 3 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4440	56	62	6169492.5	19120560	4.22	1	53.94	58.66	72.06	60.84	4.72	18.12	6.9
BWLL-5107	50	72	6193152	19178698	4.31	1	36.98	44.95	60.39	48.97	7.97	23.41	11.99
BAUS-4478	50	63	6153445.5	19148244	4.34	1	41.86	48.88	66.58	52.35	7.02	24.73	10.5
6509803	55	73	6213403	19163354	4.36	1	28.89	34.5	46.12	37.26	5.61	17.23	8.37
BWLL-5036	50	72	6193462	19179040	4.37	1	36.98	44.95	60.39	48.97	7.97	23.41	11.99
BAUS-5365	49	64	6154709.5	19158668	4.4	1	39.99	47.77	66.35	51.66	7.79	26.36	11.68
BWLL-4586	50	72	6193187.5	19179334	4.43	1	36.98	44.95	60.39	48.97	7.97	23.41	11.99
BWLL-4957	50	72	6193187.5	19179334	4.43	1	36.98	44.95	60.39	48.97	7.97	23.41	11.99
BAUS-4231	49	64	6154315	19156072	4.46	1	39.99	47.77	66.35	51.66	7.79	26.36	11.68
BAUS-5178	54	61	6159714	19125378	4.47	1	50.4	55.12	68.62	57.3	4.72	18.22	6.9
BAUS-4433	47	68	6164433	19176176	4.48	1	34.07	42.25	59.14	46.26	8.18	25.07	12.19
BAUS-4555	49	64	6154125	19156470	4.49	1	39.99	47.77	66.35	51.66	7.79	26.36	11.68
BAUS-4323	49	64	6153822	19157574	4.55	1	39.99	47.77	66.35	51.66	7.79	26.36	11.68
BAUS-4215	49	64	6153833	19157270	4.55	1	39.99	47.77	66.35	51.66	7.79	26.36	11.68
BWLL-4273	49	72	6190162.5	19180238	4.6	1	35.49	42.83	57.01	46.43	7.33	21.52	10.93
BAUS-4100	47	67	6159614.5	19173068	4.64	1	34.7	42.78	59.84	46.7	8.08	25.13	12
BWLL-4020	50	72	6192689	19180938	4.72	1	36.98	44.95	60.39	48.97	7.97	23.41	11.99
BWLL-4510	54	74	6212934	19168918	4.72	1	32.69	37.91	48.48	40.42	5.21	15.78	7.73
BAUS-5408	57	62	6169281	19117216	4.82	1	54.55	58.8	70.8	60.73	4.26	16.25	6.18
BAUS-4331	54	60	6155456.5	19126140	4.96	1	50.33	54.32	65.8	56.09	3.99	15.47	5.76
BAUS-5307	55	61	6161433.5	19120750	4.97	1	53.2	57.65	70.44	59.68	4.45	17.24	6.48
BAUS-4322	49	63	6151606.5	19155470	4.98	1	40.48	47.05	63.27	50.24	6.57	22.79	9.76
BWLL-5404	49	72	6186798.5	19182242	5.05	1	35.49	42.83	57.01	46.43	7.33	21.52	10.93
BWLL-5720	48	70	6177109.5	19183434	5.07	1	34.36	42.87	59.75	47.14	8.51	25.39	12.77
BWLL-4968	52	74	6207057	19177918	5.08	1	36.91	42.54	53.58	45.25	5.62	16.66	8.33
BAUS-4151	47	64	6152060.5	19165106	5.14	1	36.62	42.77	57.05	45.65	6.15	20.43	9.02
BAUS-4240	47	66	6156685	19173776	5.15	1	35.46	43.13	59.85	46.85	7.67	24.39	11.39
BWLL-0046	50	73	6198713	19182270	5.15	1	37.43	44.09	56.95	47.34	6.66	19.52	9.91
BAUS-5332	46	67	6159231	19176600	5.17	1	32.71	39.6	54.13	42.82	6.9	21.42	10.12
BAUS-4095	46	67	6159387	19177010	5.2	1	32.71	39.6	54.13	42.82	6.9	21.42	10.12
BAUS-4361	48	64	6150553	19160396	5.22	1	38.38	45.4	61.88	48.8	7.02	23.51	10.42
BAUS-4252	46	66	6155967.5	19174154	5.3	1	33.32	39.83	53.88	42.84	6.51	20.56	9.52
BAUS-0023	58	62	6177353.5	19112740	5.37	1	54.98	58.78	69.36	60.45	3.8	14.38	5.46
6616701	46	66	6154947.5	19173422	5.37	1	33.32	39.83	53.88	42.84	6.51	20.56	9.52
BWLL-4175	47	70	6175471.5	19184974	5.38	1	32.72	40.01	54.46	43.51	7.29	21.74	10.79
BAUS-4157	55	60	6157945	19120556	5.39	1	52.52	56.33	67.3	57.98	3.8	14.78	5.46
BAUS-4229	52	60	6150139	19129496	5.45	1	45.9	50.03	61.58	51.87	4.12	15.67	5.97
BAUS-5374	47	64	6149640.5	19162492	5.46	1	36.62	42.77	57.05	45.65	6.15	20.43	9.02
BWLL-4391	50	73	6195988	19184602	5.48	1	37.43	44.09	56.95	47.34	6.66	19.52	9.91
BAUS-5320	46	66	6155757.5	19175638	5.51	1	33.32	39.83	53.88	42.84	6.51	20.56	9.52
BWLL-5619	49	73	6190846.5	19185114	5.51	1	36.4	42.59	54.5	45.53	6.19	18.1	9.13
6616408	46	67	6156879.5	19177938	5.66	1	32.71	39.6	54.13	42.82	6.9	21.42	10.12
BAUS-4533	49	61	6145912	19147068	5.7	1	40.5	44.99	56.68	47.02	4.49	16.18	6.53
BAUS-4441	46	66	6154841	19176140	5.71	1	33.32	39.83	53.88	42.84	6.51	20.56	9.52
6517505	59	70	6212777.5	19134288	5.75	1	37.04	41.48	51.81	43.56	4.44	14.77	6.52
BAUS-4312	47	65	6149991	19168882	5.76	1	35.96	42.92	58.56	46.24	6.96	22.61	10.28
BWLL-4388	47	71	6176538	19187140	5.78	1	32.5	39	51.7	42.05	6.5	19.2	9.55
BWLL-4841	55	75	6219268	19169050	5.79	1	29.27	33.44	42.01	35.36	4.17	12.74	6.09
BWLL-4199	48	72	6184208.5	19186706	5.81	1	33.94	40.48	53.11	43.58	6.54	19.17	9.63
BWLL-4019	48	72	6188877	19186572	5.81	1	33.94	40.48	53.11	43.58	6.54	19.17	9.63
BWLL-4198	48	72	6184296.5	19186710	5.82	1	33.94	40.48	53.11	43.58	6.54	19.17	9.63
BWLL-4271	54	75	6216897.5	19173622	5.84	1	32.17	36.61	45.58	38.67	4.44	13.41	6.5
BWLL-4668	46	69	6164915.5	19184902	5.88	1	31.31	37.98	51.37	41.08	6.67	20.05	9.76
BAUS-5321	46	66	6155203.5	19177898	5.88	1	33.32	39.83	53.88	42.84	6.51	20.56	9.52
BAUS-4209	47	64	6148873	19168134	5.9	1	36.62	42.77	57.05	45.65	6.15	20.43	9.02
BWLL-4844	54	75	6219097.5	19171272	5.96	1	32.17	36.61	45.58	38.67	4.44	13.41	6.5
BAUS-5366	59	62	6179431	19109360	6.01	1	55.96	59.33	68.64	60.75	3.37	12.68	4.8
BAUS-4284	46	67	6156156.5	19179906	6.02	1	32.71	39.6	54.13	42.82	6.9	21.42	10.12
BWLL-4146	47	71	6177018	19188474	6.03	1	32.5	39	51.7	42.05	6.5	19.2	9.55
6525104	60	65	6195083.5	19113996	6.05	1	50.38	54.07	63.77	55.7	3.69	13.39	5.32
BAUS-4111	49	62	6145119.5	19152104	6.05	1	40.46	45.9	59.76	48.46	5.44	19.3	8
6517806	60	67	6203449.5	19120438	6.1	1	45.7	49.64	59.55	51.42	3.94	13.85	5.72

Table C-2
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 4 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4320	46	67	6155152.5	19179796	6.14	1	32.71	39.6	54.13	42.82	6.9	21.42	10.12
BAUS-5210	46	66	6152520	19177072	6.16	1	33.32	39.83	53.88	42.84	6.51	20.56	9.52
BWLL-5048	50	74	6201355	19187026	6.16	1	37.59	43.11	53.75	45.7	5.53	16.16	8.11
BWLL-5244	47	71	6176659	19189290	6.18	1	32.5	39	51.7	42.05	6.5	19.2	9.55
BAUS-4219	47	63	6146183.5	19164496	6.18	1	36.9	42.19	54.85	44.6	5.29	17.95	7.7
BWLL-4997	48	73	6191791	19188702	6.19	1	34.78	40.33	50.97	42.87	5.55	16.19	8.08
BAUS-4179	51	60	6142840	19136634	6.33	1	44.11	48.18	59.38	50	4.07	15.27	5.89
BWLL-4481	51	75	6207214	19185620	6.34	1	37.92	42.62	51.74	44.77	4.7	13.82	6.84
BAUS-4501	47	63	6144274	19161188	6.42	1	36.9	42.19	54.85	44.6	5.29	17.95	7.7
BAUS-4546	45	66	6152776	19179814	6.46	1	31.47	36.94	48.72	39.34	5.47	17.24	7.87
BAUS-4096	45	66	6152178.5	19179288	6.48	1	31.47	36.94	48.72	39.34	5.47	17.24	7.87
BWLL-4362	53	59	6146703.5	19124416	6.5	1	47.84	51.26	61.02	52.71	3.42	13.18	4.87
BAUS-4194	45	66	6152336.5	19179800	6.52	1	31.47	36.94	48.72	39.34	5.47	17.24	7.87
BWLL-5633	46	72	6178922	19191884	6.67	1	30.9	35.67	44.85	37.73	4.77	13.95	6.83
BWLL-5316	48	73	6188437.5	19191416	6.73	1	34.78	40.33	50.97	42.87	5.55	16.19	8.08
BWLL-0050	54	76	6221764	19175320	6.78	1	31.33	35.17	42.9	36.88	3.83	11.56	5.55
6517615	59	73	6225327	19143954	6.79	1	28.41	32.03	40.01	33.65	3.62	11.6	5.24
6517612	59	73	6225327	19143954	6.79	1	28.41	32.03	40.01	33.65	3.62	11.6	5.24
BAUS-4058	55	59	6152213	19115596	6.8	1	51.31	54.52	63.81	55.85	3.21	12.5	4.54
BAUS-4317	53	59	6144949.5	19124152	6.81	1	47.84	51.26	61.02	52.71	3.42	13.18	4.87
BWLL-5218	47	73	6186841.5	19191764	6.83	1	33.62	38.45	47.7	40.56	4.83	14.08	6.94
BWLL-0014B	54	76	6222610.5	19174580	6.85	1	31.33	35.17	42.9	36.88	3.83	11.56	5.55
BAUS-4456	53	59	6145351.5	19122748	6.89	1	47.84	51.26	61.02	52.71	3.42	13.18	4.87
BAUS-4329	53	59	6145263	19122744	6.9	1	47.84	51.26	61.02	52.71	3.42	13.18	4.87
BWLL-4529	50	75	6206447	19189744	6.98	1	38.3	42.86	51.63	44.9	4.56	13.33	6.6
BWLL-4524	50	75	6206447	19189744	6.98	1	38.3	42.86	51.63	44.9	4.56	13.33	6.6
6623602	49	60	6138788.5	19144204	6.99	1	40.84	44.55	54.38	46.16	3.71	13.54	5.32
BWLL-5229	48	73	6190403.5	19193006	7.01	1	34.78	40.33	50.97	42.87	5.55	16.19	8.08
BWLL-5228	48	73	6190403.5	19193006	7.01	1	34.78	40.33	50.97	42.87	5.55	16.19	8.08
BWLL-5230	48	73	6190403.5	19193006	7.01	1	34.78	40.33	50.97	42.87	5.55	16.19	8.08
BWLL-5231	48	73	6190403.5	19193006	7.01	1	34.78	40.33	50.97	42.87	5.55	16.19	8.08
BWLL-5234	48	73	6190403.5	19193006	7.01	1	34.78	40.33	50.97	42.87	5.55	16.19	8.08
BWLL-5235	48	73	6190403.5	19193006	7.01	1	34.78	40.33	50.97	42.87	5.55	16.19	8.08
BWLL-5236	48	73	6190403.5	19193006	7.01	1	34.78	40.33	50.97	42.87	5.55	16.19	8.08
BWLL-5278	48	73	6190403.5	19193006	7.01	1	34.78	40.33	50.97	42.87	5.55	16.19	8.08
BWLL-0056	48	73	6190403.5	19193006	7.01	1	34.78	40.33	50.97	42.87	5.55	16.19	8.08
BWLL-4098	46	72	6180351	19193656	7.02	1	30.9	35.67	44.85	37.73	4.77	13.95	6.83
BAUS-4254	48	61	6139071	19148754	7.02	1	38.78	42.91	53.46	44.73	4.13	14.69	5.95
BAUS-4202	45	65	6145386.5	19174694	7.03	1	31.94	36.93	47.94	39.08	4.98	16	7.14
6525106	61	65	6198306	19109812	7.05	1	51.09	54.31	62.7	55.66	3.21	11.61	4.57
6616305	46	71	6175255.5	19193866	7.06	1	30.57	36.04	46.7	38.48	5.47	16.13	7.91
BWLL-0001D	54	76	6224553	19173702	7.08	1	31.33	35.17	42.9	36.88	3.83	11.56	5.55
BWLL-5560	50	76	6207148	19189986	7.08	1	39.23	42.97	50.16	44.56	3.74	10.93	5.33
BWLL-5583	50	76	6207148	19189986	7.08	1	39.23	42.97	50.16	44.56	3.74	10.93	5.33
BWLL-5705	50	76	6207148	19189986	7.08	1	39.23	42.97	50.16	44.56	3.74	10.93	5.33
BAUS-4287	48	61	6139321	19151700	7.09	1	38.78	42.91	53.46	44.73	4.13	14.69	5.95
BWLL-5093	50	76	6206153.5	19190542	7.1	1	39.23	42.97	50.16	44.56	3.74	10.93	5.33
BWLL-4001	50	76	6206776	19190364	7.11	1	39.23	42.97	50.16	44.56	3.74	10.93	5.33
BWLL-5523	49	75	6202579.5	19192032	7.13	1	38.61	42.88	51.02	44.73	4.26	12.41	6.11
BWLL-4387	46	71	6173820.5	19194232	7.15	1	30.57	36.04	46.7	38.48	5.47	16.13	7.91
BWLL-5260	49	75	6202931	19192046	7.15	1	38.61	42.88	51.02	44.73	4.26	12.41	6.11
BWLL-4427	47	73	6189667.5	19193892	7.18	1	33.62	38.45	47.7	40.56	4.83	14.08	6.94
BWLL-5047	49	75	6203183.5	19192358	7.22	1	38.61	42.88	51.02	44.73	4.26	12.41	6.11
BAUS-4164	54	58	6147398	19117150	7.23	1	48.51	51.3	59.34	52.41	2.78	10.82	3.89
BAUS-4369	49	60	6137283	19144440	7.28	1	40.84	44.55	54.38	46.16	3.71	13.54	5.32
BWLL-4753	54	77	6223802.5	19177320	7.31	1	29.95	33.23	39.82	34.63	3.28	9.87	4.68
BWLL-4655	49	75	6202275.5	19193136	7.32	1	38.61	42.88	51.02	44.73	4.26	12.41	6.11
BAUS-4313	48	60	6137047.5	19146152	7.34	1	39.26	42.69	51.62	44.14	3.43	12.36	4.88
BWLL-4599	49	75	6202890.5	19193158	7.35	1	38.61	42.88	51.02	44.73	4.26	12.41	6.11
BWLL-4656	49	75	6201913	19193426	7.35	1	38.61	42.88	51.02	44.73	4.26	12.41	6.11
BAUS-5288	54	58	6148317	19114972	7.39	1	48.51	51.3	59.34	52.41	2.78	10.82	3.89
BAUS-4078	48	61	6137790.5	19152660	7.42	1	38.78	42.91	53.46	44.73	4.13	14.69	5.95

Table C-2
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 5 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BWLL-4660	49	75	6202868	19193764	7.46	1	38.61	42.88	51.02	44.73	4.26	12.41	6.11
BWLL-4227	53	77	6222451.5	19180512	7.46	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4113	53	77	6222902.5	19180224	7.5	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4304	53	77	6222433	19181016	7.52	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4181	53	77	6222891	19180528	7.53	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-5210	49	75	6202498.5	19194258	7.53	1	38.61	42.88	51.02	44.73	4.26	12.41	6.11
BWLL-4297	45	71	6169373.5	19195592	7.54	1	28.5	33.04	41.83	34.96	4.54	13.33	6.45
BWLL-4405	54	77	6224743	19178064	7.54	1	29.95	33.23	39.82	34.63	3.28	9.87	4.68
BAUS-4066	47	62	6138023	19158642	7.55	1	36.97	41.43	52.41	43.4	4.46	15.44	6.44
BWLL-4265	53	77	6222608.5	19181024	7.55	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4570	53	77	6223437	19180042	7.55	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BAUS-4075	47	62	6138002	19159248	7.56	1	36.97	41.43	52.41	43.4	4.46	15.44	6.44
BAUS-4297	46	72	6178346	19196654	7.57	1	30.9	35.67	44.85	37.73	4.77	13.95	6.83
BWLL-4590	49	75	6202934	19194374	7.58	1	38.61	42.88	51.02	44.73	4.26	12.41	6.11
BAUS-4230	47	61	6136978	19153238	7.59	1	37.08	40.8	50.15	42.39	3.72	13.07	5.3
BWLL-4127	53	77	6223052	19180938	7.6	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4299	54	77	6225373.5	19177684	7.6	1	29.95	33.23	39.82	34.63	3.28	9.87	4.68
BWLL-4114	53	77	6222864.5	19181236	7.61	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-5339	53	77	6222956.5	19181138	7.61	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4128	53	77	6223876.5	19180058	7.62	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4017	53	77	6224063.5	19179760	7.62	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4014	53	77	6223972	19179858	7.62	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
6510715	57	76	6231432	19161984	7.63	1	22.15	25.4	32.21	26.82	3.25	10.06	4.66
BWLL-4264	53	77	6223319	19180848	7.63	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4262	54	77	6225736	19177392	7.63	1	29.95	33.23	39.82	34.63	3.28	9.87	4.68
6517614	60	73	6228549	19139770	7.65	1	27.78	31	38.2	32.4	3.23	10.42	4.62
BWLL-4308	53	77	6224144	19179966	7.65	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BAUS-4472	48	60	6135298.5	19145788	7.67	1	39.26	42.69	51.62	44.14	3.43	12.36	4.88
BWLL-4614	49	75	6202556.5	19195070	7.68	1	38.61	42.88	51.02	44.73	4.26	12.41	6.11
BWLL-4180	53	77	6224041	19180368	7.68	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4294	53	77	6223671	19180860	7.68	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BAUS-5154	47	62	6137316	19158718	7.69	1	36.97	41.43	52.41	43.4	4.46	15.44	6.44
BWLL-4058	53	77	6224133	19180270	7.69	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4266	54	77	6224686.5	19179582	7.69	1	29.95	33.23	39.82	34.63	3.28	9.87	4.68
BWLL-4179	53	77	6224030	19180672	7.72	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4034	54	77	6224862.5	19179588	7.72	1	29.95	33.23	39.82	34.63	3.28	9.87	4.68
BWLL-5165	49	76	6202725	19195278	7.73	1	39.96	43.46	50.13	44.9	3.5	10.17	4.94
BWLL-4225	54	77	6224847	19179992	7.76	1	29.95	33.23	39.82	34.63	3.28	9.87	4.68
BWLL-4279	53	77	6224477	19180486	7.76	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4380	53	77	6223831.5	19181272	7.76	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4566	53	77	6223831.5	19181272	7.76	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4797	55	77	6227917.5	19175550	7.81	1	26	29.2	35.73	30.57	3.2	9.72	4.57
BWLL-4916	53	77	6224271	19181288	7.82	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-5324	47	73	6186384	19197114	7.83	1	33.62	38.45	47.7	40.56	4.83	14.08	6.94
BWLL-4990	52	77	6218864.5	19187062	7.83	1	35.53	38.81	45.25	40.19	3.28	9.72	4.67
BWLL-4018	54	77	6225195	19180106	7.83	1	29.95	33.23	39.82	34.63	3.28	9.87	4.68
BWLL-4359	53	77	6224450.5	19181194	7.84	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4226	54	77	6225096	19180408	7.85	1	29.95	33.23	39.82	34.63	3.28	9.87	4.68
BWLL-4016	53	77	6224813.5	19180902	7.86	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4059	54	77	6225271.5	19180414	7.88	1	29.95	33.23	39.82	34.63	3.28	9.87	4.68
BWLL-4060	54	77	6225271.5	19180414	7.88	1	29.95	33.23	39.82	34.63	3.28	9.87	4.68
BWLL-0014A	55	77	6229109.5	19174278	7.9	1	26	29.2	35.73	30.57	3.2	9.72	4.57
BAUS-5159	47	61	6136060	19156852	7.91	1	37.08	40.8	50.15	42.39	3.72	13.07	5.3
BAUS-4356	49	59	6133777	19141382	7.94	1	41.4	44.47	52.72	45.74	3.07	11.32	4.34
BWLL-4088	54	77	6225898	19180134	7.94	1	29.95	33.23	39.82	34.63	3.28	9.87	4.68
BWLL-4447	53	77	6225241.5	19181222	7.96	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4126	53	77	6225329.5	19181226	7.98	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4407	53	77	6225604.5	19180932	7.98	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4282	54	77	6226062.5	19180444	8	1	29.95	33.23	39.82	34.63	3.28	9.87	4.68
6525105	62	65	6201528	19105630	8.04	1	51.68	54.49	61.82	55.62	2.81	10.14	3.95
BWLL-4228	53	77	6225853	19181346	8.07	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71
BWLL-4012	53	77	6226028.5	19181354	8.1	1	33.09	36.39	42.94	37.8	3.3	9.85	4.71

Table C-2
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 6 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4394	44	64	6139451.5	19175804	8.13	1	30.28	33.93	42.2	35.39	3.65	11.92	5.11
6518103	58	76	6234654	19157800	8.16	1	19.45	22.46	28.83	23.74	3	9.37	4.29
6518406	60	74	6232732	19142992	8.17	1	24.02	27.05	33.71	28.33	3.02	9.69	4.31
BAUS-5433	45	63	6137554	19171998	8.17	1	33.17	37.03	46.05	38.63	3.85	12.88	5.45
BWLL-4482	48	76	6202617.5	19198212	8.26	1	39.84	43	49.01	44.25	3.17	9.17	4.42
BAUS-5362	44	64	6139628	19178494	8.34	1	30.28	33.93	42.2	35.39	3.65	11.92	5.11
BAUS-4308	44	64	6137869	19175750	8.39	1	30.28	33.93	42.2	35.39	3.65	11.92	5.11
6615902	45	63	6136149	19171854	8.4	1	33.17	37.03	46.05	38.63	3.85	12.88	5.45
6509106	46	74	6188481	19200322	8.41	1	33.24	36.69	43.24	38.06	3.45	9.99	4.82
BWLL-5718	56	77	6233042.5	19172732	8.46	1	22.06	25.11	31.41	26.41	3.05	9.34	4.35
BWLL-4263	54	78	6229601	19179968	8.51	1	27.34	30.06	35.51	31.17	2.72	8.17	3.83
BAUS-4228	48	58	6129578	19140528	8.74	1	40.96	43.33	49.64	44.22	2.36	8.68	3.26
BAUS-4544	45	62	6133072	19169406	8.82	1	33.05	36.35	44.25	37.67	3.3	11.2	4.62
BWLL-4969	45	73	6182724.5	19203464	8.91	1	29.63	32.97	39.31	34.27	3.34	9.69	4.64
6518404	61	74	6235954	19138808	9.01	1	22.31	24.99	30.97	26.09	2.68	8.66	3.78
BAUS-4319	46	60	6129618	19154706	9.01	1	35.85	38.6	45.52	39.67	2.74	9.67	3.82
6518403	61	74	6235954	19138808	9.01	1	22.31	24.99	30.97	26.09	2.68	8.66	3.78
6525209	63	66	6208933	19104668	9.03	1	50.22	52.78	59.32	53.78	2.56	9.1	3.56
6525218	63	66	6208933	19104668	9.03	1	50.22	52.78	59.32	53.78	2.56	9.1	3.56
6525219	63	66	6208933	19104668	9.03	1	50.22	52.78	59.32	53.78	2.56	9.1	3.56
6525220	63	65	6204749.5	19101448	9.04	1	51.94	54.42	60.87	55.38	2.48	8.92	3.44
6525221	63	65	6204749.5	19101448	9.04	1	51.94	54.42	60.87	55.38	2.48	8.92	3.44
6525210	63	65	6204749.5	19101448	9.04	1	51.94	54.42	60.87	55.38	2.48	8.92	3.44
BAUS-4072	45	62	6131531.5	19168138	9.04	1	33.05	36.35	44.25	37.67	3.3	11.2	4.62
BAUS-4131	48	58	6128001.5	19140272	9.04	1	40.96	43.33	49.64	44.22	2.36	8.68	3.26
6525202	63	67	6213116	19107890	9.08	1	48.25	50.85	57.4	51.87	2.6	9.14	3.62
6525203	63	67	6213116	19107890	9.08	1	48.25	50.85	57.4	51.87	2.6	9.14	3.62
BAUS-4291	45	61	6130616.5	19166588	9.14	1	33.26	36.06	42.91	37.14	2.8	9.65	3.88
BWLL-5331	46	74	6188675.5	19204286	9.16	1	33.24	36.69	43.24	38.06	3.45	9.99	4.82
BAUS-4217	45	61	6130444.5	19166480	9.17	1	33.26	36.06	42.91	37.14	2.8	9.65	3.88
BAUS-4305	45	61	6130444.5	19166480	9.17	1	33.26	36.06	42.91	37.14	2.8	9.65	3.88
BAUS-4218	45	61	6130444.5	19166480	9.17	1	33.26	36.06	42.91	37.14	2.8	9.65	3.88
BAUS-4195	45	61	6130275.5	19166272	9.19	1	33.26	36.06	42.91	37.14	2.8	9.65	3.88
BWLL-4511	53	79	6228988.5	19186932	9.19	1	28.52	30.81	35.35	31.69	2.29	6.83	3.17
BAUS-5306	45	61	6130250.5	19166582	9.21	1	33.26	36.06	42.91	37.14	2.8	9.65	3.88
BAUS-5377	45	61	6130250.5	19166582	9.21	1	33.26	36.06	42.91	37.14	2.8	9.65	3.88
BAUS-4532	48	58	6127012.5	19140844	9.22	1	40.96	43.33	49.64	44.22	2.36	8.68	3.26
6525301	63	68	6217299	19111112	9.23	1	45.77	48.37	54.82	49.39	2.6	9.05	3.63
BAUS-5181	45	61	6130085.5	19166670	9.24	1	33.26	36.06	42.91	37.14	2.8	9.65	3.88
BAUS-4463	45	61	6129853.5	19165750	9.25	1	33.26	36.06	42.91	37.14	2.8	9.65	3.88
BWLL-5038	52	79	6226942.5	19189894	9.27	1	32.09	34.35	38.77	35.2	2.26	6.67	3.11
BAUS-5371	45	61	6129745	19166062	9.28	1	33.26	36.06	42.91	37.14	2.8	9.65	3.88
BWLL-4560	52	79	6225465	19191764	9.33	1	32.09	34.35	38.77	35.2	2.26	6.67	3.11
BWLL-5368	53	79	6229497	19187458	9.33	1	28.52	30.81	35.35	31.69	2.29	6.83	3.17
BAUS-5439	45	61	6129458.5	19166208	9.34	1	33.26	36.06	42.91	37.14	2.8	9.65	3.88
BAUS-4166	44	62	6129924.5	19168790	9.36	1	30.83	33.57	40.09	34.61	2.74	9.26	3.78
BWLL-5377	52	79	6225996	19191682	9.38	1	32.09	34.35	38.77	35.2	2.26	6.67	3.11
BWLL-4212	46	75	6189681.5	19205640	9.41	1	35.05	37.93	43.37	39.02	2.88	8.31	3.96
BAUS-4363	46	60	6127131	19155328	9.5	1	35.85	38.6	45.52	39.67	2.74	9.67	3.82
BAUS-4037	48	58	6125454	19142614	9.51	1	40.96	43.33	49.64	44.22	2.36	8.68	3.26
BWLL-4239	55	79	6237373	19176916	9.53	1	18.49	20.68	25.12	21.53	2.19	6.63	3.04
BWLL-4562	52	79	6227130.5	19191926	9.57	1	32.09	34.35	38.77	35.2	2.26	6.67	3.11
BWLL-4898	53	79	6232263	19186448	9.62	1	28.52	30.81	35.35	31.69	2.29	6.83	3.17
BWLL-5566	52	79	6227068	19192974	9.7	1	32.09	34.35	38.77	35.2	2.26	6.67	3.11
6623205	45	60	6126611.5	19158036	9.71	1	33.94	36.32	42.24	37.2	2.38	8.31	3.26
BWLL-5656	53	79	6232524.5	19187068	9.73	1	28.52	30.81	35.35	31.69	2.29	6.83	3.17
BWLL-5063	51	79	6224348	19195772	9.76	1	35.09	37.27	41.5	38.08	2.18	6.41	2.99
BWLL-5602	52	79	6228469	19192130	9.78	1	32.09	34.35	38.77	35.2	2.26	6.67	3.11
BWLL-5148	50	79	6221156.5	19198794	9.85	1	37.61	39.66	43.59	40.39	2.04	5.97	2.77
BAUS-5364	48	57	6123778	19139626	9.85	1	42.01	43.97	49.26	44.67	1.96	7.25	2.66
BWLL-5655	53	79	6233317.5	19187106	9.85	1	28.52	30.81	35.35	31.69	2.29	6.83	3.17
BWLL-5657	53	79	6233273	19187104	9.85	1	28.52	30.81	35.35	31.69	2.29	6.83	3.17

Table C-2
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 7 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BWLL-5658	53	79	6233273	19187104	9.85	1	28.52	30.81	35.35	31.69	2.29	6.83	3.17
6510813	58	78	6243020.5	19164244	9.86	1	7.93	10.19	14.95	11.09	2.26	7.02	3.16
6510814	58	78	6243020.5	19164244	9.86	1	7.93	10.19	14.95	11.09	2.26	7.02	3.16
BWLL-4662	50	79	6221947	19198822	9.94	1	37.61	39.66	43.59	40.39	2.04	5.97	2.77
BWLL-4276	50	79	6221947	19198822	9.94	1	37.61	39.66	43.59	40.39	2.04	5.97	2.77
BWLL-5605	43	73	6173644.5	19209052	9.95	1	24.74	26.76	30.57	27.44	2.02	5.82	2.7
BAUS-4189	43	62	6127509.5	19172454	9.99	1	28.1	30.31	35.51	31.08	2.21	7.42	2.99

Table C-3
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Evangeline Aquifer (Layer 2) - GAM
Page 1 of 2

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
6517417	55	69	6195706	19147798	1.74	2	27.59	55.95	114.5	73.38	28.36	86.91	45.79
BWLL-5065	50	69	6182473	19168922	2.48	2	25.26	56.76	115.65	76.2	31.5	90.39	50.94
BWLL-4269	50	69	6182649	19168928	2.49	2	25.26	56.76	115.65	76.2	31.5	90.39	50.94
BWLL-5609	50	70	6183010	19170292	2.76	2	24.5	49.65	96.02	64.96	25.14	71.52	40.46
BAUS-0022B	48	68	6169273	19172252	3.37	2	24.18	42.39	78.23	53.07	18.2	54.04	28.88
BAUS-0022A	48	68	6169273	19172252	3.37	2	24.18	42.39	78.23	53.07	18.2	54.04	28.88
BWLL-0001C	51	72	6197378.5	19173006	3.4	2	25.79	43.17	74.61	53.46	17.38	48.82	27.67
6509704	51	72	6197392	19173010	3.4	2	25.79	43.17	74.61	53.46	17.38	48.82	27.67
BWLL-4555	49	71	6182775.5	19177642	4.08	2	22.78	38.75	68.4	48.11	15.98	45.62	25.34
BWLL-0001A	52	73	6202960	19174426	4.1	2	24.05	37.8	62.82	45.77	13.74	38.76	21.71
BWLL-5067	49	71	6184782.5	19178120	4.26	2	22.78	38.75	68.4	48.11	15.98	45.62	25.34
6624805	56	62	6169529	19119842	4.34	2	41.44	49.85	78.18	54.38	8.41	36.74	12.94
BAUS-0005B	56	61	6168258	19118458	4.68	2	43.41	50.31	72.98	53.89	6.9	29.57	10.48
6624801	57	62	6169900.5	19116538	4.91	2	42.47	49.81	73.86	53.67	7.35	31.39	11.2
BWLL-5211	48	71	6180275.5	19183526	5.11	2	21.66	34.34	58.09	41.58	12.67	36.43	19.91
BWLL-4682	47	70	6173949	19185730	5.55	2	21.5	32.99	54.84	39.42	11.5	33.35	17.92
BWLL-5517	49	73	6190934.5	19185634	5.61	2	21.06	31.06	49.42	36.64	10	28.36	15.59
BWLL-00043	54	75	6217397	19172020	5.75	2	17.41	25.23	40.06	29.53	7.83	22.66	12.12
BWLL-4200	48	72	6184472	19186716	5.83	2	20.79	31.19	50.48	37	10.4	29.69	16.21
BWLL-4201	48	72	6184556.5	19186820	5.85	2	20.79	31.19	50.48	37	10.4	29.69	16.21
BAUS-5057	46	66	6154201	19176826	5.88	2	22.44	31.94	51.88	37.07	9.51	29.45	14.64
BWLL-0007	53	75	6216934	19174876	5.98	2	17.74	25.72	40.63	30.1	7.98	22.89	12.36
BWLL-4535	46	69	6165758	19185944	6	2	20.65	30.26	48.93	35.54	9.61	28.28	14.89
6509403	48	73	6189086	19187984	6.07	2	20.13	28.48	43.86	33.03	8.35	23.74	12.9
BWLL-4649	47	71	6177179.5	19188884	6.1	2	20.47	30.41	49.05	35.88	9.94	28.58	15.4
6509404	48	73	6191004	19188382	6.13	2	20.13	28.48	43.86	33.03	8.35	23.74	12.9
BWLL-5646	48	73	6188683.5	19188736	6.22	2	20.13	28.48	43.86	33.03	8.35	23.74	12.9
BWLL-00049	55	75	6222004.5	19168848	6.25	2	14.83	22.28	36.65	26.35	7.45	21.82	11.52
BAUS-0013A	46	64	6147113	19169048	6.28	2	24.63	32.2	49.13	36.08	7.57	24.5	11.45
BAUS-0013B	46	64	6147113	19169048	6.28	2	24.63	32.2	49.13	36.08	7.57	24.5	11.45
BWLL-4937	45	68	6158954	19184286	6.34	2	19.34	26.86	41.91	30.87	7.52	22.57	11.53
BAUS-4034	45	67	6154157	19180572	6.37	2	19.71	27.22	42.57	31.2	7.51	22.86	11.49
BWLL-4147	47	72	6183378	19190220	6.44	2	19.72	28.02	43.48	32.52	8.29	23.75	12.8
BWLL-5314	45	68	6162103.5	19187042	6.48	2	19.34	26.86	41.91	30.87	7.52	22.57	11.53
6615906	46	63	6144477	19165654	6.55	2	26.33	32.78	47.69	36.02	6.45	21.36	9.69
BWLL-4928	45	68	6159076	19185808	6.56	2	19.34	26.86	41.91	30.87	7.52	22.57	11.53
BAUS-0007A	45	67	6154188.5	19182116	6.58	2	19.71	27.22	42.57	31.2	7.51	22.86	11.49
BAUS-0007C	45	67	6154188.5	19182116	6.58	2	19.71	27.22	42.57	31.2	7.51	22.86	11.49
BWLL-0012B	54	76	6222034	19172800	6.58	2	14.85	21.07	32.87	24.38	6.21	18.02	9.52
BWLL-5084	46	71	6178037	19191952	6.68	2	19.03	26.73	41.22	30.86	7.7	22.19	11.83
BWLL-4891	46	71	6176356.5	19192196	6.73	2	19.03	26.73	41.22	30.86	7.7	22.19	11.83
BWLL-4351	48	73	6190630.5	19191596	6.74	2	20.13	28.48	43.86	33.03	8.35	23.74	12.9
BWLL-4166	47	73	6187526	19192294	6.91	2	19.16	25.95	38.49	29.55	6.78	19.33	10.39
BWLL-00058	50	75	6206661	19189554	6.96	2	19.02	25.85	38.36	29.49	6.83	19.34	10.47
BAUS-0003C	45	64	6144379	19171800	6.96	2	22.95	28.87	41.89	31.82	5.92	18.93	8.87
BWLL-4152	46	71	6175947.5	19193802	7.04	2	19.03	26.73	41.22	30.86	7.7	22.19	11.83
BWLL-4302	46	72	6180256	19193856	7.06	2	18.44	24.98	37.16	28.41	6.54	18.71	9.96
BWLL-5713	50	76	6207148	19189986	7.08	2	17.46	22.75	32.44	25.47	5.28	14.97	8
BWLL-5382	50	76	6208567	19189518	7.11	2	17.46	22.75	32.44	25.47	5.28	14.97	8
BWLL-5648	47	72	6182773	19193958	7.12	2	19.72	28.02	43.48	32.52	8.29	23.75	12.8
BWLL-5649	47	72	6182773	19193958	7.12	2	19.72	28.02	43.48	32.52	8.29	23.75	12.8
6616407	45	67	6152008	19184036	7.13	2	19.71	27.22	42.57	31.2	7.51	22.86	11.49
BWLL-4982	45	71	6171283.5	19193838	7.15	2	17.43	23.35	34.56	26.44	5.92	17.13	9.01
BWLL-5004	47	72	6183327	19194068	7.16	2	19.72	28.02	43.48	32.52	8.29	23.75	12.8
BWLL-4998	45	71	6173553.5	19194324	7.18	2	17.43	23.35	34.56	26.44	5.92	17.13	9.01
BWLL-4485	47	72	6183144	19194264	7.19	2	19.72	28.02	43.48	32.52	8.29	23.75	12.8
BWLL-5598	46	72	6176661.5	19194946	7.25	2	18.44	24.98	37.16	28.41	6.54	18.71	9.96
BWLL-5066	46	72	6176694.5	19195044	7.27	2	18.44	24.98	37.16	28.41	6.54	18.71	9.96
BWLL-5623	45	70	6167395	19193756	7.3	2	18.04	24.7	37.53	28.23	6.67	19.49	10.19
BWLL-5706	45	71	6171943	19195126	7.37	2	17.43	23.35	34.56	26.44	5.92	17.13	9.01
BWLL-4685	45	71	6171848	19195276	7.4	2	17.43	23.35	34.56	26.44	5.92	17.13	9.01
BWLL-4940	45	71	6171936	19195278	7.4	2	17.43	23.35	34.56	26.44	5.92	17.13	9.01

Table C-3
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Evangeline Aquifer (Layer 2) - GAM
Page 2 of 2

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BWLL-4941	45	71	6171936	19195278	7.4	2	17.43	23.35	34.56	26.44	5.92	17.13	9.01
BWLL-4164	45	71	6171936	19195278	7.4	2	17.43	23.35	34.56	26.44	5.92	17.13	9.01
BAUS-4296	45	71	6170790	19195340	7.44	2	17.43	23.35	34.56	26.44	5.92	17.13	9.01
BWLL-4096	44	69	6159234.5	19191282	7.44	2	16.82	22.2	32.99	25	5.39	16.18	8.18
BWLL-4557	45	71	6170340	19195626	7.51	2	17.43	23.35	34.56	26.44	5.92	17.13	9.01
BWLL-4188	46	72	6180329.5	19196694	7.59	2	18.44	24.98	37.16	28.41	6.54	18.71	9.96
6615905	45	63	6139754.5	19169318	7.6	2	25.86	30.97	42.55	33.46	5.11	16.69	7.6
6510714	57	76	6231432	19161984	7.63	2	10.34	15.71	26.4	18.53	5.37	16.06	8.19
BWLL-5428	45	72	6174327	19197288	7.72	2	17	22.08	31.57	24.68	5.08	14.58	7.68
BWLL-4842	44	70	6165153	19195544	7.75	2	16.26	21.3	31.07	23.89	5.04	14.81	7.64
BWLL-5068	45	71	6173269	19197352	7.75	2	17.43	23.35	34.56	26.44	5.92	17.13	9.01
BWLL-4404	45	72	6174839.5	19197712	7.79	2	17	22.08	31.57	24.68	5.08	14.58	7.68
BWLL-4145	45	72	6173935.5	19198388	7.94	2	17	22.08	31.57	24.68	5.08	14.58	7.68
BWLL-5045	46	73	6183174	19198316	7.95	2	18.05	23.45	33.45	26.24	5.4	15.4	8.18
BWLL-4434	45	72	6173577	19198578	7.98	2	17	22.08	31.57	24.68	5.08	14.58	7.68
BWLL-5248	44	69	6157248.5	19193780	8.04	2	16.82	22.2	32.99	25	5.39	16.18	8.18
BWLL-4365	45	73	6179715.5	19199102	8.04	2	16.78	21.02	28.86	23.16	4.24	12.08	6.37
BWLL-5255	46	73	6182713	19198906	8.05	2	18.05	23.45	33.45	26.24	5.4	15.4	8.18
BWLL-5143	45	72	6174957.5	19199336	8.1	2	17	22.08	31.57	24.68	5.08	14.58	7.68
BWLL-5217	45	72	6172929.5	19199466	8.16	2	17	22.08	31.57	24.68	5.08	14.58	7.68
BWLL-5017	45	72	6174939	19199842	8.2	2	17	22.08	31.57	24.68	5.08	14.58	7.68
BAUS-4483	44	65	6141571	19180638	8.23	2	18.97	24.03	34.81	26.53	5.06	15.84	7.56
BWLL-4581	45	72	6174000	19199980	8.23	2	17	22.08	31.57	24.68	5.08	14.58	7.68
BWLL-5225	45	72	6172915	19199870	8.23	2	17	22.08	31.57	24.68	5.08	14.58	7.68
BAUS-0003A	45	63	6136187.5	19171654	8.39	2	25.86	30.97	42.55	33.46	5.11	16.69	7.6
BWLL-4908	45	72	6175953.5	19200992	8.4	2	17	22.08	31.57	24.68	5.08	14.58	7.68
6615904	44	63	6136146.5	19171926	8.41	2	22.45	26.42	35.33	28.31	3.97	12.88	5.85
BAUS-4029	43	67	6147313	19190054	8.57	2	13.82	17.71	25.65	19.66	3.88	11.82	5.84
6615901	44	63	6135112	19171600	8.57	2	22.45	26.42	35.33	28.31	3.97	12.88	5.85
BWLL-5026	45	73	6177685.5	19203824	8.93	2	16.78	21.02	28.86	23.16	4.24	12.08	6.37
BAUS-4107	43	65	6139922	19185036	8.97	2	16.11	19.88	27.86	21.69	3.77	11.74	5.58
6509107	46	74	6189158	19203482	9	2	17.87	22.26	30.32	24.46	4.39	12.45	6.59
BWLL-4522	44	73	6176617	19204560	9.07	2	15.44	18.73	24.82	20.34	3.29	9.38	4.9
6623201	46	60	6129544	19156642	9.12	2	25.63	29.39	38.69	31.12	3.76	13.06	5.49
BWLL-5007	43	70	6158884	19201194	9.17	2	14.58	18.4	25.84	20.34	3.82	11.26	5.77
BAUS-4557	43	65	6139605.5	19186544	9.19	2	16.11	19.88	27.86	21.69	3.77	11.74	5.58
BWLL-4709	45	74	6183010.5	19205296	9.26	2	16.77	20.24	26.63	21.95	3.47	9.86	5.18
BWLL-5112	44	73	6176844	19205582	9.27	2	15.44	18.73	24.82	20.34	3.29	9.38	4.9
BWLL-4193	44	73	6175768.5	19206150	9.38	2	15.44	18.73	24.82	20.34	3.29	9.38	4.9
BWLL-4531	47	76	6198845	19205162	9.41	2	18.26	21.69	27.91	23.34	3.42	9.65	5.07
BWLL-4347	53	79	6230849	19186596	9.42	2	4.4	7.55	13.43	9.07	3.14	9.03	4.66
BWLL-4320	44	73	6176800.5	19206796	9.5	2	15.44	18.73	24.82	20.34	3.29	9.38	4.9
BWLL-4994	47	76	6198823	19205770	9.52	2	18.26	21.69	27.91	23.34	3.42	9.65	5.07
BWLL-4439	44	73	6176617.5	19206992	9.53	2	15.44	18.73	24.82	20.34	3.29	9.38	4.9
BWLL-5689	46	75	6190976.5	19207002	9.66	2	17.73	21.25	27.7	22.98	3.53	9.98	5.25
BAUS-4170	42	65	6138874.5	19189860	9.7	2	13.11	15.86	21.64	17.16	2.75	8.53	4.05
BAUS-4174	42	65	6138449	19189440	9.71	2	13.11	15.86	21.64	17.16	2.75	8.53	4.05
6509201	47	76	6200188.5	19206618	9.72	2	18.26	21.69	27.91	23.34	3.42	9.65	5.07
BAUS-4177	42	65	6139117	19190476	9.74	2	13.11	15.86	21.64	17.16	2.75	8.53	4.05
BWLL-5709	44	73	6176275.5	19208486	9.82	2	15.44	18.73	24.82	20.34	3.29	9.38	4.9
BWLL-5329	46	76	6193732	19207914	9.84	2	17.18	20	25.13	21.33	2.82	7.94	4.15
6518209	58	78	6243020.5	19164244	9.86	2	3.15	6.1	11.94	7.53	2.95	8.79	4.39
BAUS-4050	42	64	6132258.5	19182744	9.95	2	13.3	15.78	21.1	16.93	2.48	7.8	3.63

Table C-4
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Evangeline Aquifer (Layer 2) - HAGM
Page 1 of 2

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
6517417	55	69	6195706	19147798	1.74	2	50.78	78.8	136.08	96.05	28.02	85.3	45.27
BWLL-5065	50	69	6182473	19168922	2.48	2	40.57	71.98	129.91	91.25	31.4	89.34	50.67
BWLL-4269	50	69	6182649	19168928	2.49	2	40.57	71.98	129.91	91.25	31.4	89.34	50.67
BWLL-5609	50	70	6183010	19170292	2.76	2	41.03	66.14	111.99	81.34	25.11	70.97	40.32
BAUS-0022B	48	68	6169273	19172252	3.37	2	37.85	55.95	91.42	66.57	18.1	53.57	28.72
BAUS-0022A	48	68	6169273	19172252	3.37	2	37.85	55.95	91.42	66.57	18.1	53.57	28.72
BWLL-0001C	51	72	6197378.5	19173006	3.4	2	57.26	74.71	106.27	85.02	17.45	49.02	27.77
6509704	51	72	6197392	19173010	3.4	2	57.26	74.71	106.27	85.02	17.45	49.02	27.77
BWLL-4555	49	71	6182775.5	19177642	4.08	2	40.35	56.43	86.24	65.79	16.08	45.88	25.44
BWLL-0001A	52	73	6202960	19174426	4.1	2	62.95	76.92	102.5	85.05	13.97	39.55	22.09
BWLL-5067	49	71	6184782.5	19178120	4.26	2	40.35	56.43	86.24	65.79	16.08	45.88	25.44
6624805	56	62	6169529	19119842	4.34	2	67.01	75.08	102.09	79.47	8.07	35.09	12.46
BAUS-0005B	56	61	6168258	19118458	4.68	2	71.06	77.65	99.24	81.12	6.59	28.18	10.07
6624801	57	62	6169900.5	19116538	4.91	2	69.92	76.93	99.78	80.67	7.01	29.86	10.75
BWLL-5211	48	71	6180275.5	19183526	5.11	2	37.18	50.04	74.22	57.33	12.87	37.04	20.16
BWLL-4682	47	70	6173949	19185730	5.55	2	34.9	46.52	68.83	53	11.62	33.93	18.1
BWLL-5517	49	73	6190934.5	19185634	5.61	2	47.51	57.8	76.9	63.5	10.29	29.39	15.99
BWLL-0043	54	75	6217397	19172020	5.75	2	80.44	89.25	106.19	94.16	8.82	25.76	13.72
BWLL-4200	48	72	6184472	19186716	5.83	2	39.96	50.62	70.57	56.52	10.66	30.61	16.56
BWLL-4201	48	72	6184556.5	19186820	5.85	2	39.96	50.62	70.57	56.52	10.66	30.61	16.56
BAUS-5057	46	66	6154201	19176826	5.88	2	36.39	45.87	65.89	50.99	9.48	29.49	14.6
BWLL-0007	53	75	6216934	19174876	5.98	2	74.5	83.24	99.8	88.07	8.73	25.29	13.57
BWLL-4535	46	69	6165758	19185944	6	2	32.77	42.44	61.5	47.72	9.67	28.73	14.95
6509403	48	73	6189086	19187984	6.07	2	43.59	52.27	68.51	56.95	8.69	24.93	13.37
BWLL-4649	47	71	6177179.5	19188884	6.1	2	34.05	44.21	63.52	49.78	10.16	29.47	15.73
6509404	48	73	6191004	19188382	6.13	2	43.59	52.27	68.51	56.95	8.69	24.93	13.37
BWLL-5646	48	73	6188683.5	19188736	6.22	2	43.59	52.27	68.51	56.95	8.69	24.93	13.37
BWLL-0049	55	75	6222004.5	19168848	6.25	2	65.75	74.37	91.2	79.15	8.62	25.46	13.41
BAUS-0013A	46	64	6147113	19169048	6.28	2	43.69	51.27	68.43	55.24	7.57	24.74	11.55
BAUS-0013B	46	64	6147113	19169048	6.28	2	43.69	51.27	68.43	55.24	7.57	24.74	11.55
BWLL-4937	45	68	6158954	19184286	6.34	2	31.31	38.89	54.1	42.89	7.58	22.79	11.58
BAUS-4034	45	67	6154157	19180572	6.37	2	31.8	39.35	54.81	43.32	7.55	23.01	11.52
BWLL-4147	47	72	6183378	19190220	6.44	2	35.85	44.47	60.76	49.09	8.62	24.9	13.24
BWLL-5314	45	68	6162103.5	19187042	6.48	2	31.31	38.89	54.1	42.89	7.58	22.79	11.58
6615906	46	63	6144477	19165654	6.55	2	50.67	57.16	72.35	60.49	6.49	21.68	9.82
BWLL-4928	45	68	6159076	19185808	6.56	2	31.31	38.89	54.1	42.89	7.58	22.79	11.58
BAUS-0007A	45	67	6154188.5	19182116	6.58	2	31.8	39.35	54.81	43.32	7.55	23.01	11.52
BAUS-0007C	45	67	6154188.5	19182116	6.58	2	31.8	39.35	54.81	43.32	7.55	23.01	11.52
BWLL-0012B	54	76	6222034	19172800	6.58	2	87.69	95.23	109.77	99.33	7.54	22.08	11.64
BWLL-5084	46	71	6178037	19191952	6.68	2	30.72	38.67	53.93	42.87	7.95	23.22	12.16
BWLL-4891	46	71	6176356.5	19192196	6.73	2	30.72	38.67	53.93	42.87	7.95	23.22	12.16
BWLL-4351	48	73	6190630.5	19191596	6.74	2	43.59	52.27	68.51	56.95	8.69	24.93	13.37
BWLL-4166	47	73	6187526	19192294	6.91	2	39.69	46.85	60.34	50.59	7.17	20.66	10.9
BWLL-0058	50	75	6206661	19189554	6.96	2	59.71	66.98	80.58	70.85	7.27	20.87	11.14
BAUS-0003C	45	64	6144379	19171800	6.96	2	44.02	50.01	63.49	53.04	5.99	19.48	9.02
BWLL-4152	46	71	6175947.5	19193802	7.04	2	30.72	38.67	53.93	42.87	7.95	23.22	12.16
BWLL-4302	46	72	6180256	19193856	7.06	2	32.13	39	52.07	42.54	6.87	19.94	10.41
BWLL-5713	50	76	6207148	19189986	7.08	2	65.73	71.51	82.37	74.48	5.78	16.64	8.75
BWLL-5382	50	76	6208567	19189518	7.11	2	65.73	71.51	82.37	74.48	5.78	16.64	8.75
BWLL-5648	47	72	6182773	19193958	7.12	2	35.85	44.47	60.76	49.09	8.62	24.9	13.24
BWLL-5649	47	72	6182773	19193958	7.12	2	35.85	44.47	60.76	49.09	8.62	24.9	13.24
6616407	45	67	6152008	19184036	7.13	2	31.8	39.35	54.81	43.32	7.55	23.01	11.52
BWLL-4982	45	71	6171283.5	19193838	7.15	2	27.66	33.83	45.75	36.96	6.17	18.09	9.3
BWLL-5004	47	72	6183327	19194068	7.16	2	35.85	44.47	60.76	49.09	8.62	24.9	13.24
BWLL-4998	45	71	6173553.5	19194324	7.18	2	27.66	33.83	45.75	36.96	6.17	18.09	9.3
BWLL-4485	47	72	6183144	19194264	7.19	2	35.85	44.47	60.76	49.09	8.62	24.9	13.24
BWLL-5598	46	72	6176661.5	19194946	7.25	2	32.13	39	52.07	42.54	6.87	19.94	10.41
BWLL-5066	46	72	6176694.5	19195044	7.27	2	32.13	39	52.07	42.54	6.87	19.94	10.41
BWLL-5623	45	70	6167395	19193756	7.3	2	28.02	34.87	48.25	38.41	6.85	20.23	10.39
BWLL-5706	45	71	6171943	19195126	7.37	2	27.66	33.83	45.75	36.96	6.17	18.09	9.3
BWLL-4685	45	71	6171848	19195276	7.4	2	27.66	33.83	45.75	36.96	6.17	18.09	9.3
BWLL-4940	45	71	6171936	19195278	7.4	2	27.66	33.83	45.75	36.96	6.17	18.09	9.3

Table C-4
Simulated Drawdown and Drawdown Due to Electro Purification Pumping
Evangeline Aquifer (Layer 2) - HAGM
Page 2 of 2

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Drawdown 2008 to 2060 (ft)				Drawdown Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BWLL-4941	45	71	6171936	19195278	7.4	2	27.66	33.83	45.75	36.96	6.17	18.09	9.3
BWLL-4164	45	71	6171936	19195278	7.4	2	27.66	33.83	45.75	36.96	6.17	18.09	9.3
BAUS-4296	45	71	6170790	19195340	7.44	2	27.66	33.83	45.75	36.96	6.17	18.09	9.3
BWLL-4096	44	69	6159234.5	19191282	7.44	2	28.2	33.72	44.62	36.51	5.52	16.42	8.31
BWLL-4557	45	71	6170340	19195626	7.51	2	27.66	33.83	45.75	36.96	6.17	18.09	9.3
BWLL-4188	46	72	6180329.5	19196694	7.59	2	32.13	39	52.07	42.54	6.87	19.94	10.41
6615905	45	63	6139754.5	19169318	7.6	2	56.24	61.46	73.55	64.03	5.22	17.31	7.79
6510714	57	76	6231432	19161984	7.63	2	37.63	44	56.88	47.38	6.37	19.25	9.76
BWLL-5428	45	72	6174327	19197288	7.72	2	28.88	34.28	44.62	36.95	5.4	15.74	8.08
BWLL-4842	44	70	6165153	19195544	7.75	2	25.97	31.17	41.33	33.73	5.2	15.36	7.76
BWLL-5068	45	71	6173269	19197352	7.75	2	27.66	33.83	45.75	36.96	6.17	18.09	9.3
BWLL-4404	45	72	6174839.5	19197712	7.79	2	28.88	34.28	44.62	36.95	5.4	15.74	8.08
BWLL-4145	45	72	6173935.5	19198388	7.94	2	28.88	34.28	44.62	36.95	5.4	15.74	8.08
BWLL-5045	46	73	6183174	19198316	7.95	2	35.26	41.06	52.05	43.97	5.8	16.79	8.71
BWLL-4434	45	72	6173577	19198578	7.98	2	28.88	34.28	44.62	36.95	5.4	15.74	8.08
BWLL-5248	44	69	6157248.5	19193780	8.04	2	28.2	33.72	44.62	36.51	5.52	16.42	8.31
BWLL-4365	45	73	6179715.5	19199102	8.04	2	31.89	36.52	45.3	38.73	4.62	13.41	6.84
BWLL-5255	46	73	6182713	19198906	8.05	2	35.26	41.06	52.05	43.97	5.8	16.79	8.71
BWLL-5143	45	72	6174957.5	19199336	8.1	2	28.88	34.28	44.62	36.95	5.4	15.74	8.08
BWLL-5217	45	72	6172929.5	19199466	8.16	2	28.88	34.28	44.62	36.95	5.4	15.74	8.08
BWLL-5017	45	72	6174939	19199842	8.2	2	28.88	34.28	44.62	36.95	5.4	15.74	8.08
BAUS-4483	44	65	6141571	19180638	8.23	2	34.58	39.71	50.94	42.26	5.13	16.35	7.67
BWLL-4581	45	72	6174000	19199980	8.23	2	28.88	34.28	44.62	36.95	5.4	15.74	8.08
BWLL-5225	45	72	6172915	19199870	8.23	2	28.88	34.28	44.62	36.95	5.4	15.74	8.08
BAUS-0003A	45	63	6136187.5	19171654	8.39	2	56.24	61.46	73.55	64.03	5.22	17.31	7.79
BWLL-4908	45	72	6175953.5	19200992	8.4	2	28.88	34.28	44.62	36.95	5.4	15.74	8.08
6615904	44	63	6136146.5	19171926	8.41	2	49.62	53.79	63.39	55.76	4.17	13.77	6.14
BAUS-4029	43	67	6147313	19190054	8.57	2	24.7	28.63	36.75	30.58	3.93	12.06	5.88
6615901	44	63	6135112	19171600	8.57	2	49.62	53.79	63.39	55.76	4.17	13.77	6.14
BWLL-5026	45	73	6177685.5	19203824	8.93	2	31.89	36.52	45.3	38.73	4.62	13.41	6.84
BAUS-4107	43	65	6139922	19185036	8.97	2	30.24	34.15	42.68	36	3.91	12.44	5.76
6509107	46	74	6189158	19203482	9	2	39.89	44.71	53.81	47.05	4.82	13.92	7.16
BWLL-4522	44	73	6176617	19204560	9.07	2	29.25	32.88	39.79	34.54	3.63	10.54	5.29
6623201	46	60	6129544	19156642	9.12	2	48.41	52.22	61.83	53.99	3.81	13.42	5.58
BWLL-5007	43	70	6158884	19201194	9.17	2	24.69	28.56	36.16	30.45	3.87	11.47	5.76
BAUS-4557	43	65	6139605.5	19186544	9.19	2	30.24	34.15	42.68	36	3.91	12.44	5.76
BWLL-4709	45	74	6183010.5	19205296	9.26	2	36.55	40.44	47.81	42.25	3.9	11.27	5.7
BWLL-5112	44	73	6176844	19205582	9.27	2	29.25	32.88	39.79	34.54	3.63	10.54	5.29
BWLL-4193	44	73	6175768.5	19206150	9.38	2	29.25	32.88	39.79	34.54	3.63	10.54	5.29
BWLL-4531	47	76	6198845	19205162	9.41	2	58.4	62.29	69.59	64.1	3.89	11.19	5.7
BWLL-4347	53	79	6230849	19186596	9.42	2	87.94	91.41	98.08	93.06	3.47	10.14	5.12
BWLL-4320	44	73	6176800.5	19206796	9.5	2	29.25	32.88	39.79	34.54	3.63	10.54	5.29
BWLL-4994	47	76	6198823	19205770	9.52	2	58.4	62.29	69.59	64.1	3.89	11.19	5.7
BWLL-4439	44	73	6176617.5	19206992	9.53	2	29.25	32.88	39.79	34.54	3.63	10.54	5.29
BWLL-5689	46	75	6190976.5	19207002	9.66	2	45.97	49.95	57.44	51.8	3.98	11.47	5.83
BAUS-4170	42	65	6138874.5	19189860	9.7	2	25.24	28.16	34.53	29.49	2.92	9.29	4.25
BAUS-4174	42	65	6138449	19189440	9.71	2	25.24	28.16	34.53	29.49	2.92	9.29	4.25
6509201	47	76	6200188.5	19206618	9.72	2	58.4	62.29	69.59	64.1	3.89	11.19	5.7
BAUS-4177	42	65	6139117	19190476	9.74	2	25.24	28.16	34.53	29.49	2.92	9.29	4.25
BWLL-5709	44	73	6176275.5	19208486	9.82	2	29.25	32.88	39.79	34.54	3.63	10.54	5.29
BWLL-5329	46	76	6193732	19207914	9.84	2	52.15	55.42	61.57	56.89	3.27	9.42	4.73
6518209	58	78	6243020.5	19164244	9.86	2	-13.2	-9.64	-2.33	-7.94	3.55	10.87	5.26
BAUS-4050	42	64	6132258.5	19182744	9.95	2	27.42	30.18	36.31	31.39	2.75	8.89	3.96

Figure C-1
Simulated Drawdown 2008 to 2060 - GAM
Base Case (DFC/MAG Simulation) - Chicot Aquifer Wells (Layer 1)

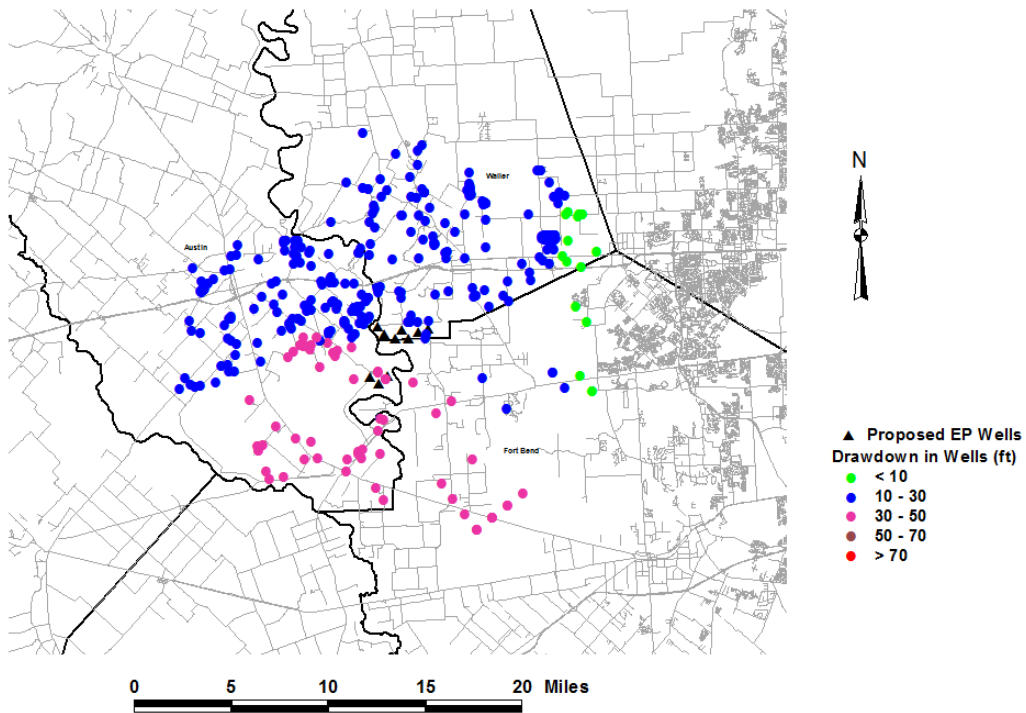


Figure C-2
Simulated Drawdown 2008 to 2060 - HAGM
Base Case (DFC/MAG Simulation) - Chicot Aquifer Wells (Layer 1)

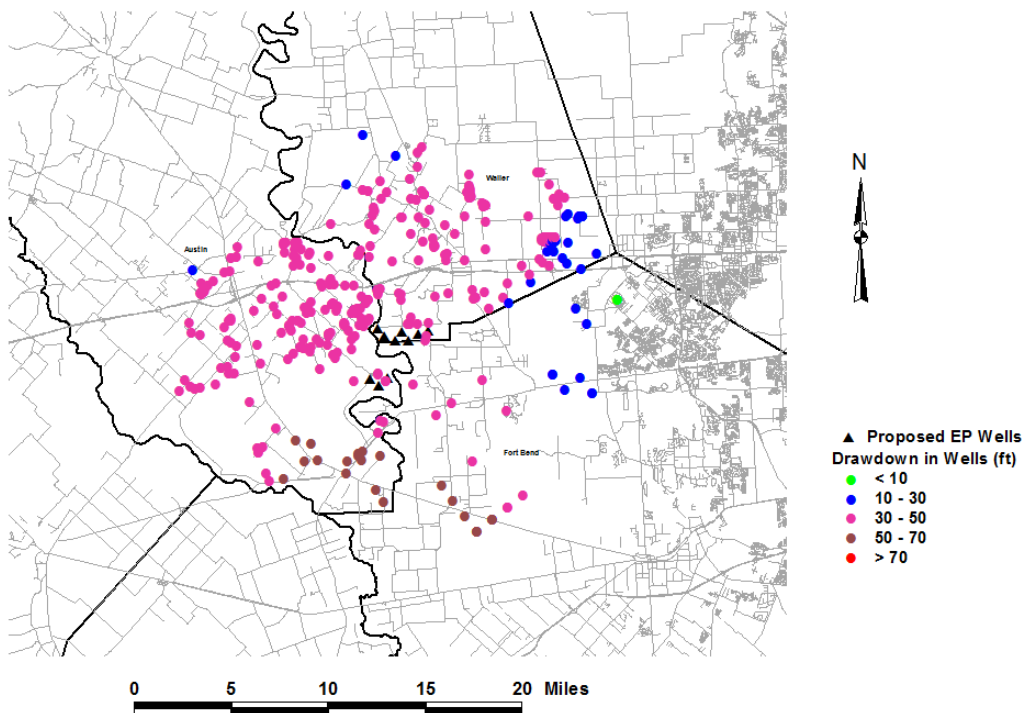


Figure C-3
Simulated Drawdown 2008 to 2060 - GAM
Scenario 3 (EP Pumping = 6 MGD) - Chicot Aquifer Wells (Layer 1)

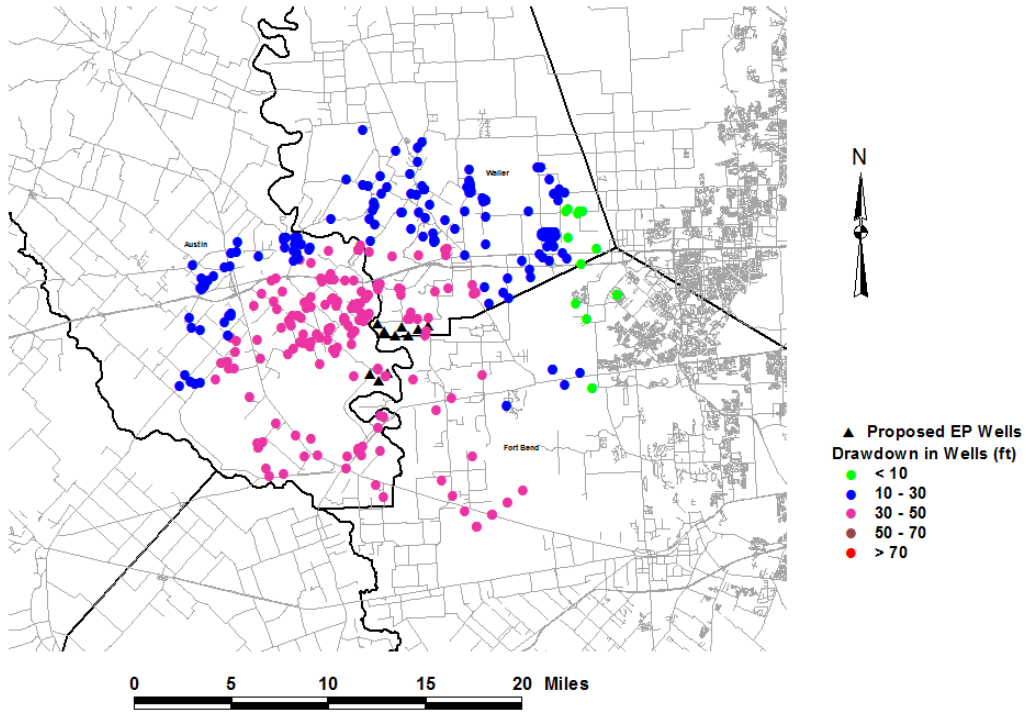


Figure C-4
Simulated Drawdown 2008 to 2060 - HAGM
Scenario 3 (EP Pumping = 6 MGD) - Chicot Aquifer Wells (Layer 1)

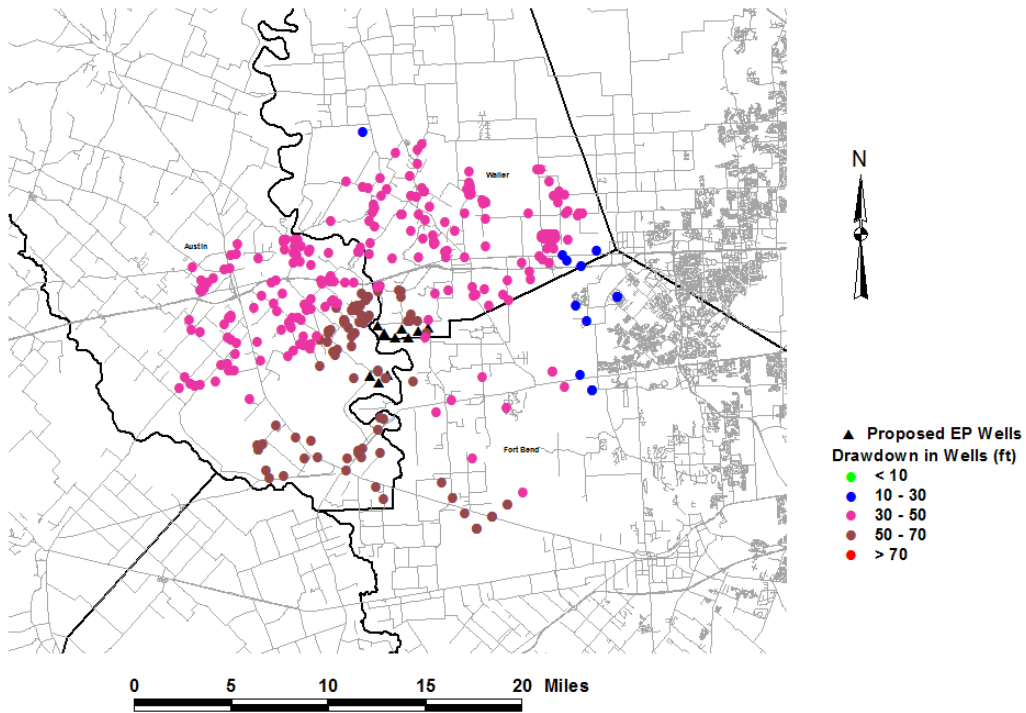


Figure C-5
Simulated Drawdown 2008 to 2060 - GAM
Scenario 10 (EP Pumping = 20 MGD) - Chicot Aquifer Wells (Layer 1)

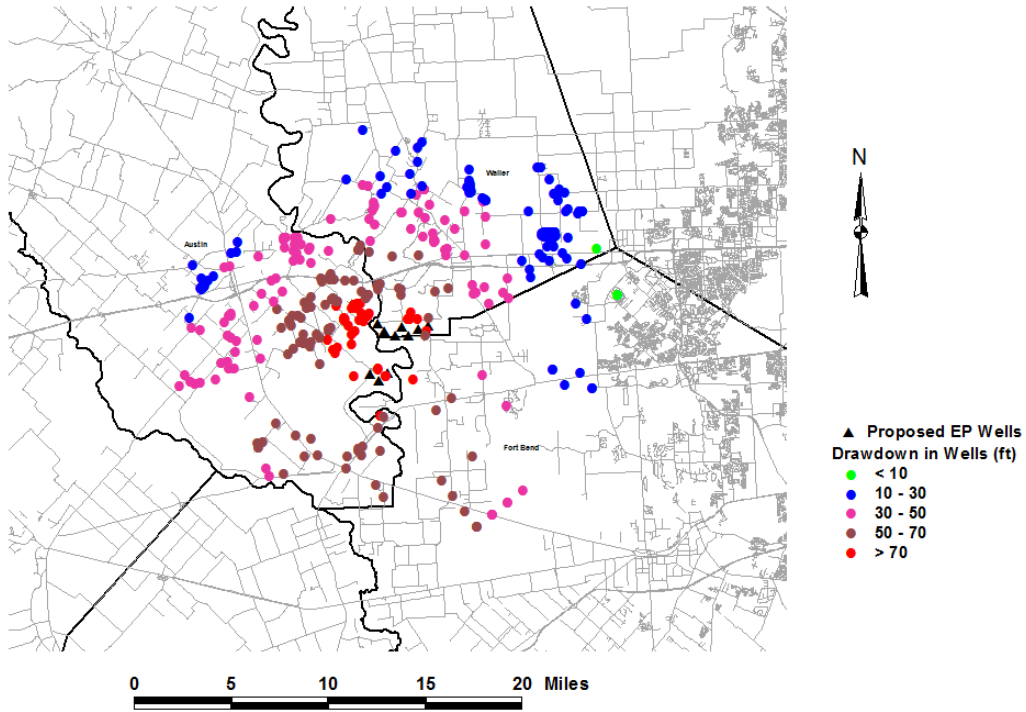


Figure C-6
Simulated Drawdown 2008 to 2060 - HAGM
Scenario 10 (EP Pumping = 20 MGD) - Chicot Aquifer Wells (Layer 1)

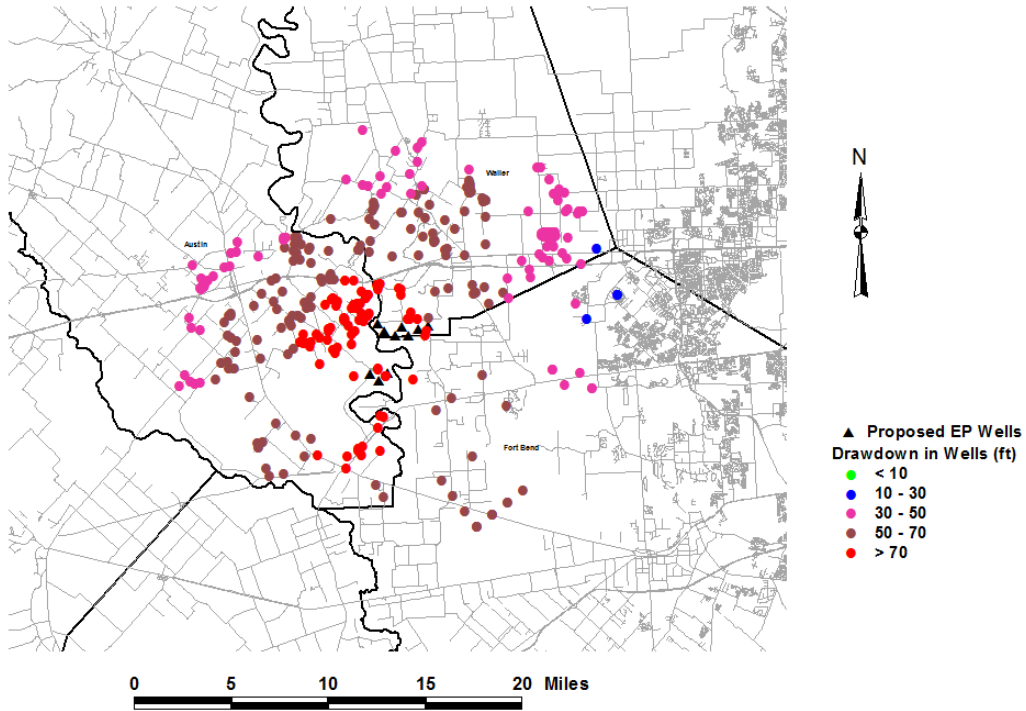


Figure C-7
Simulated Drawdown 2008 to 2060 - GAM
Scenario 31 (EP Pumping = 9.9 MGD) - Chicot Aquifer Wells (Layer 1)

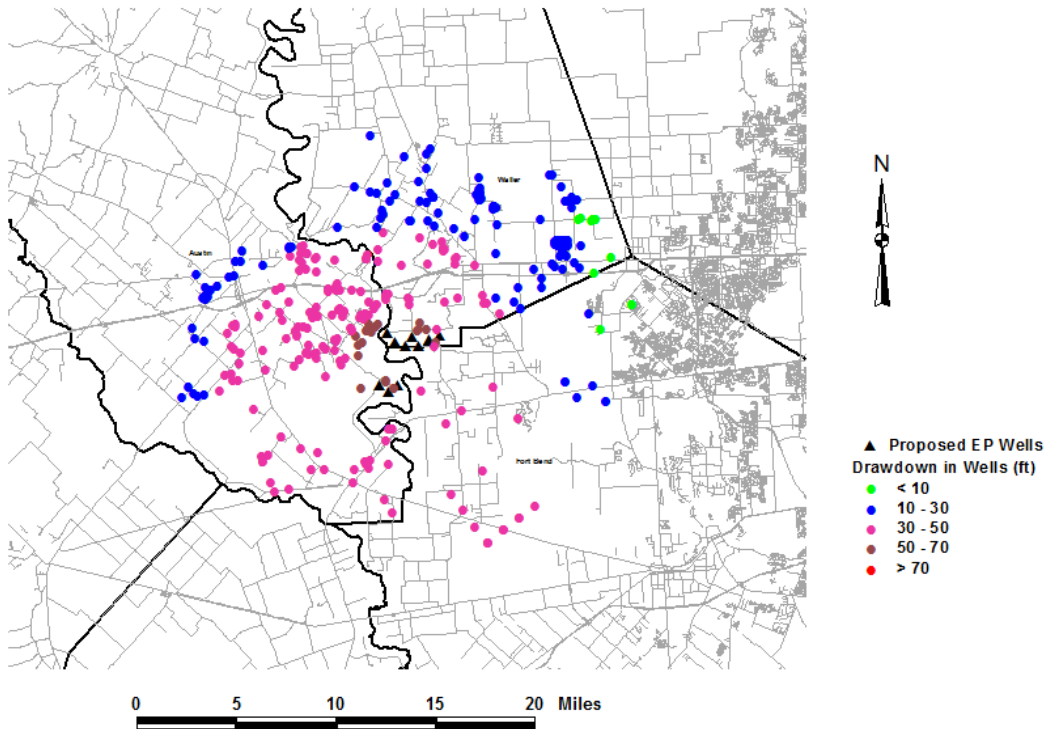


Figure C-8
Simulated Drawdown 2008 to 2060 - HAGM
Scenario 31 (EP Pumping = 9.9 MGD) - Chicot Aquifer Wells (Layer 1)

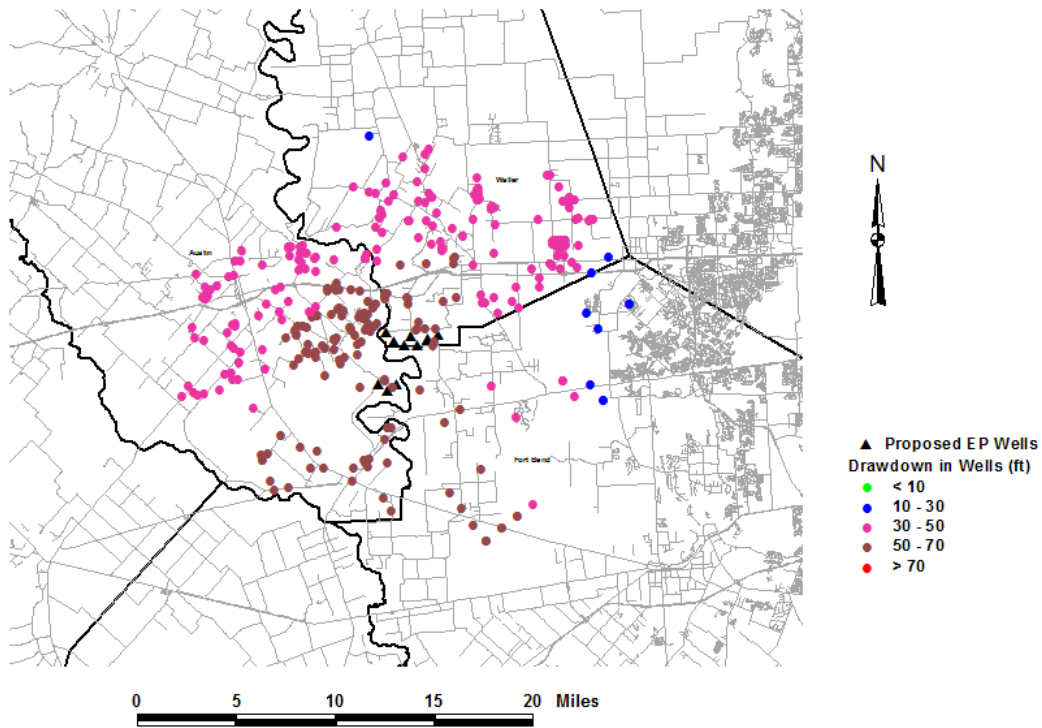


Figure C-9
Simulated Drawdown 2008 to 2060 - GAM
Base Case (DFC/MAG Simulation) - Evangeline Aquifer Wells (Layer 2)

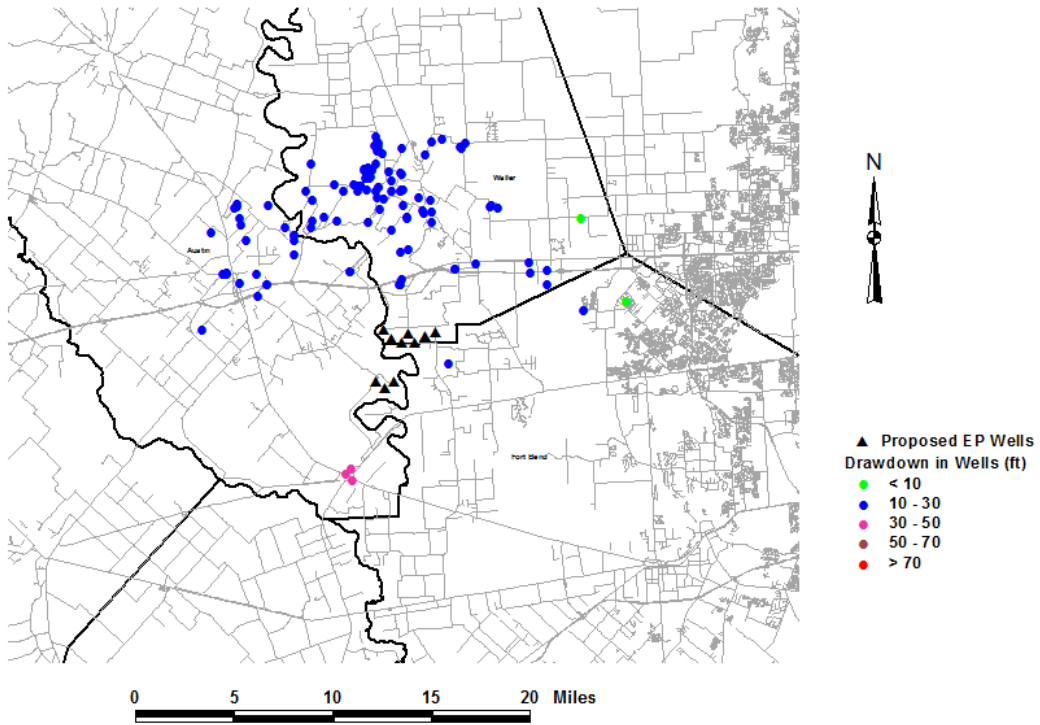


Figure C-10
Simulated Drawdown 2008 to 2060 - HAGM
Base Case (DFC/MAG Simulation) - Evangeline Aquifer Wells (Layer 2)

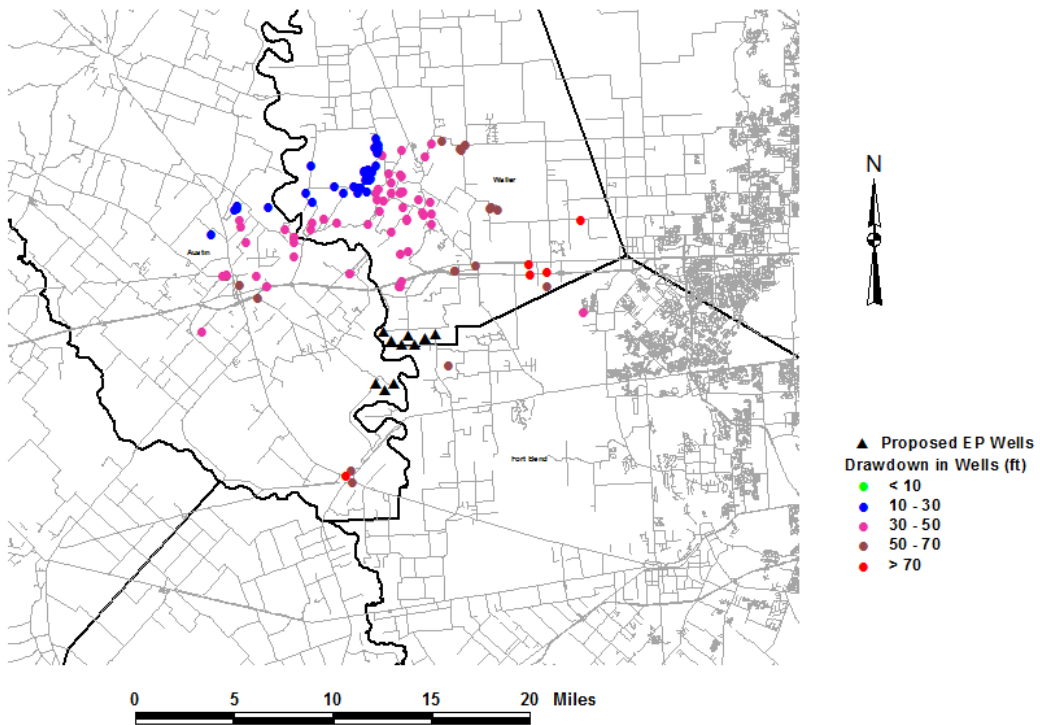


Figure C-11
Simulated Drawdown 2008 to 2060 - GAM
Scenario 3 (EP Pumping = 6 MGD) - Evangeline Aquifer Wells (Layer 2)

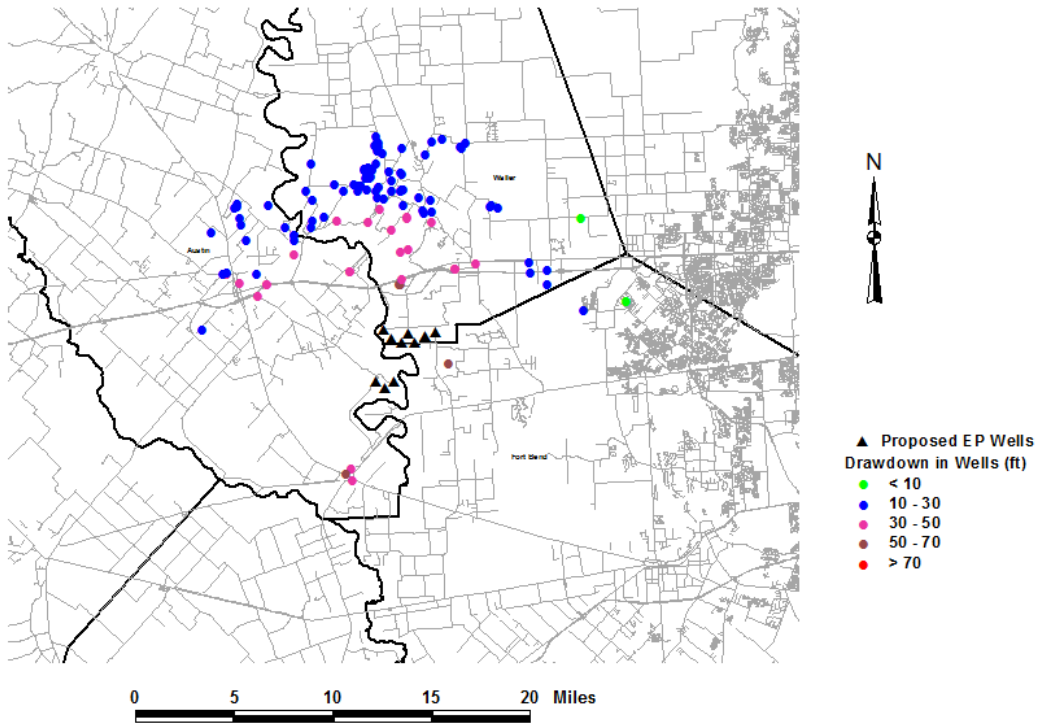


Figure C-12
Simulated Drawdown 2008 to 2060 - HAGM
Scenario 3 (EP Pumping = 6 MGD) - Evangeline Aquifer Wells (Layer 2)

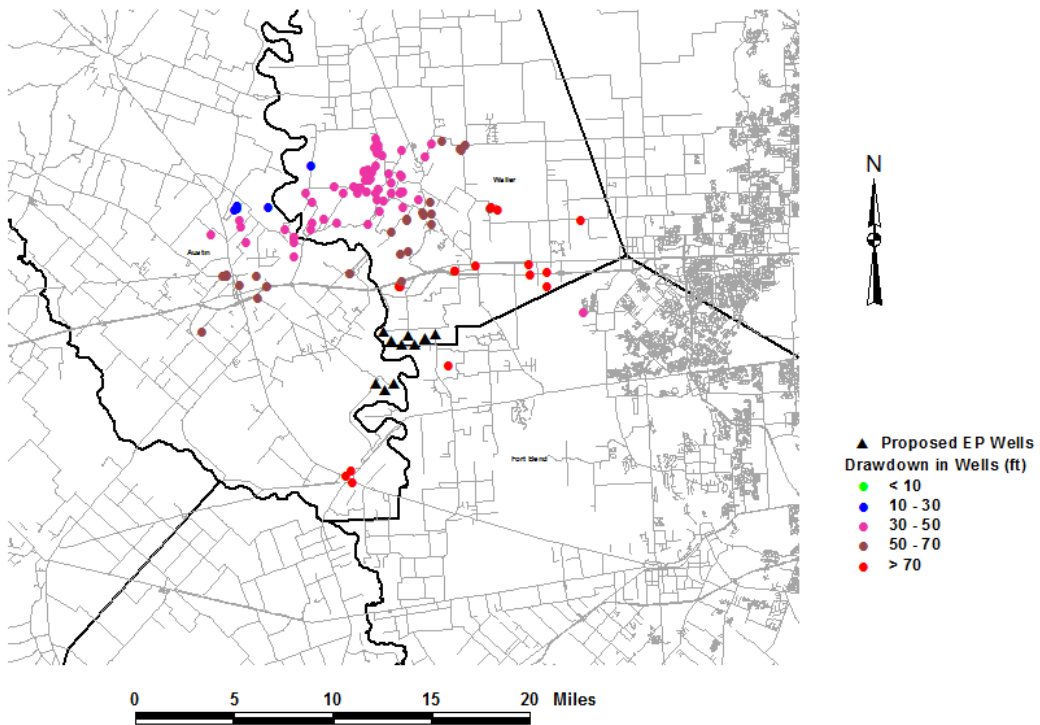


Figure C-13
Simulated Drawdown 2008 to 2060 - GAM
Scenario 10 (EP Pumping = 20 MGD) - Evangeline Aquifer Wells (Layer 2)

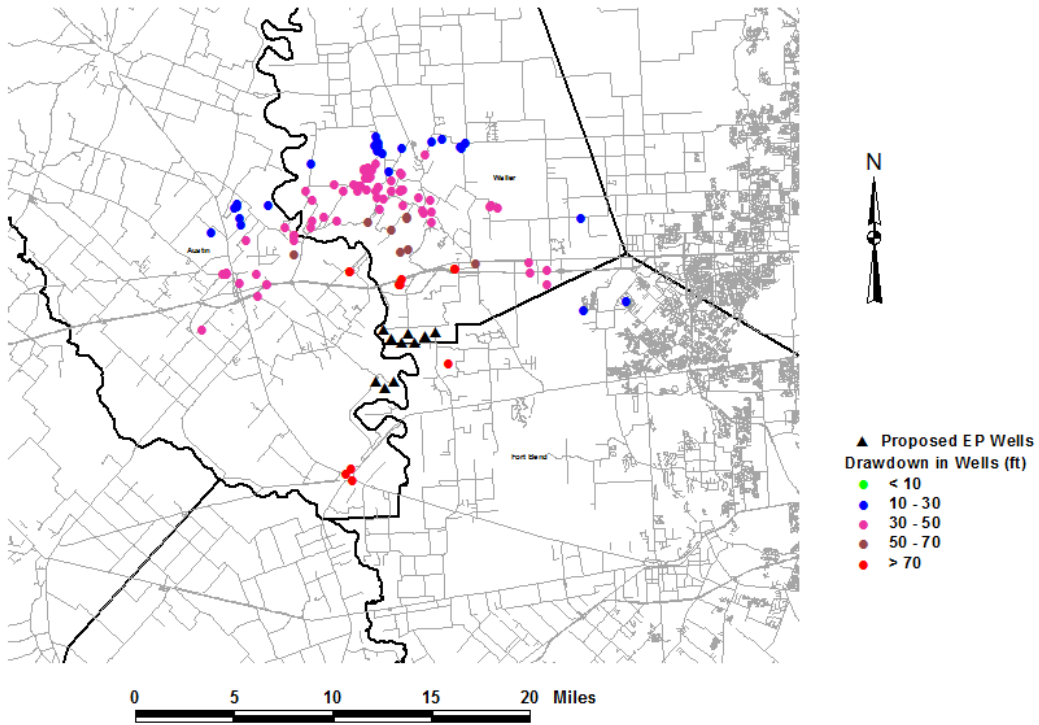


Figure C-14
Simulated Drawdown 2008 to 2060 - HAGM
Scenario 10 (EP Pumping = 20 MGD) - Evangeline Aquifer Wells (Layer 2)

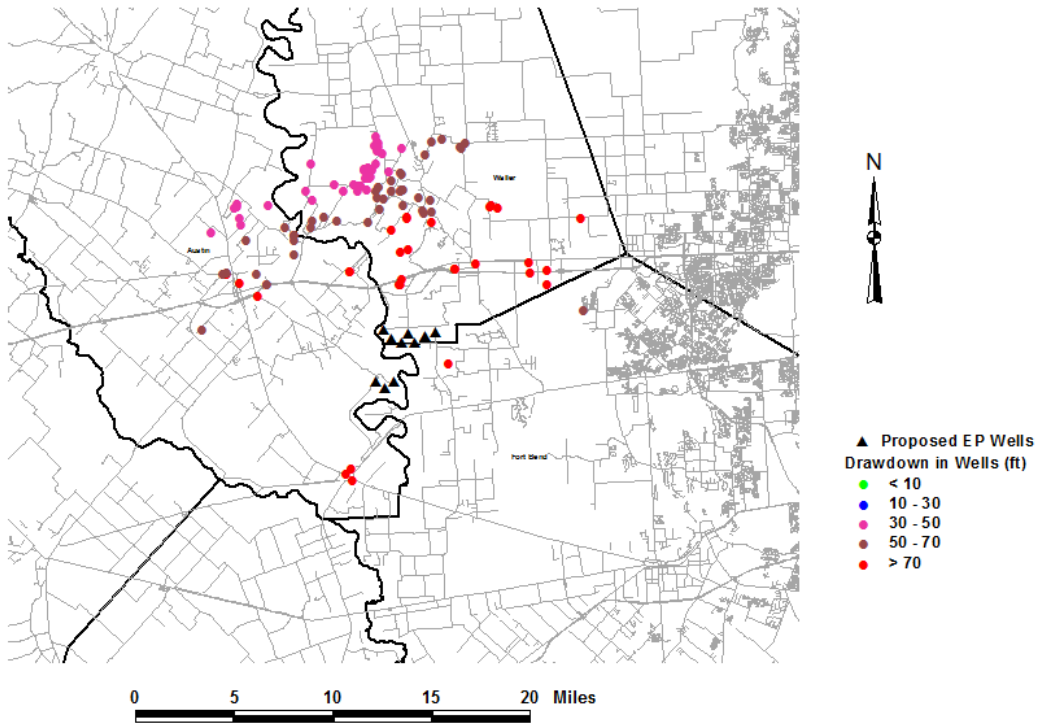


Figure C-15
Simulated Drawdown 2008 to 2060 - GAM
Scenario 31 (EP Pumping = 9.9 MGD) - Evangeline Aquifer Wells (Layer 2)

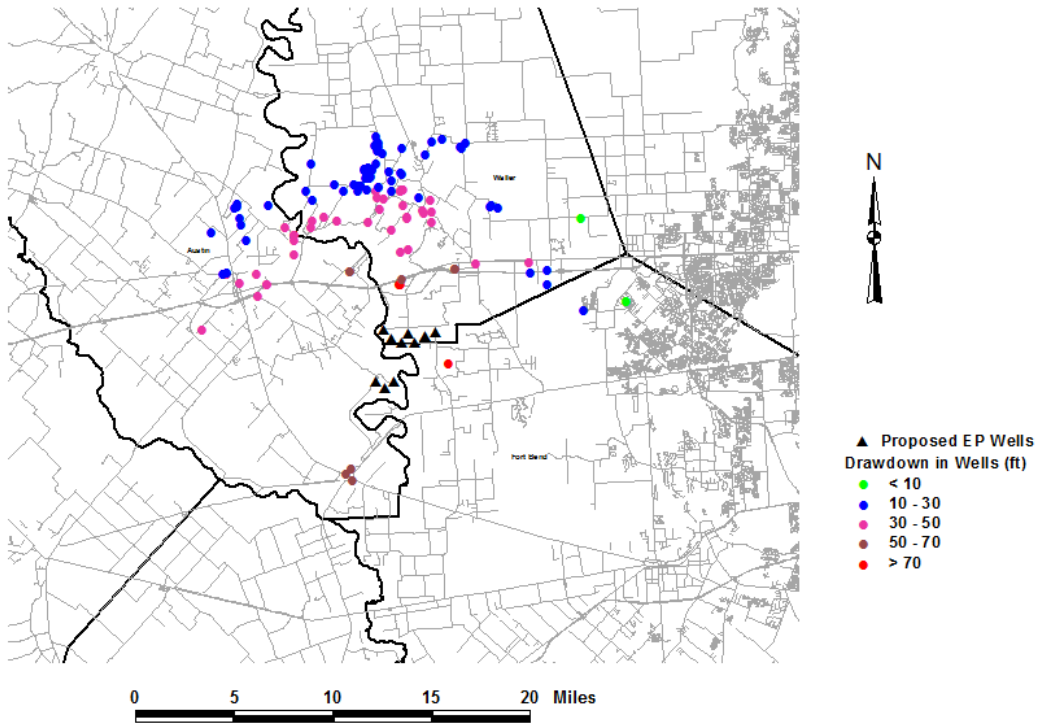


Figure C-16
Simulated Drawdown 2008 to 2060 - HAGM
Scenario 31 (EP Pumping = 9.9 MGD) - Evangeline Aquifer Wells (Layer 2)

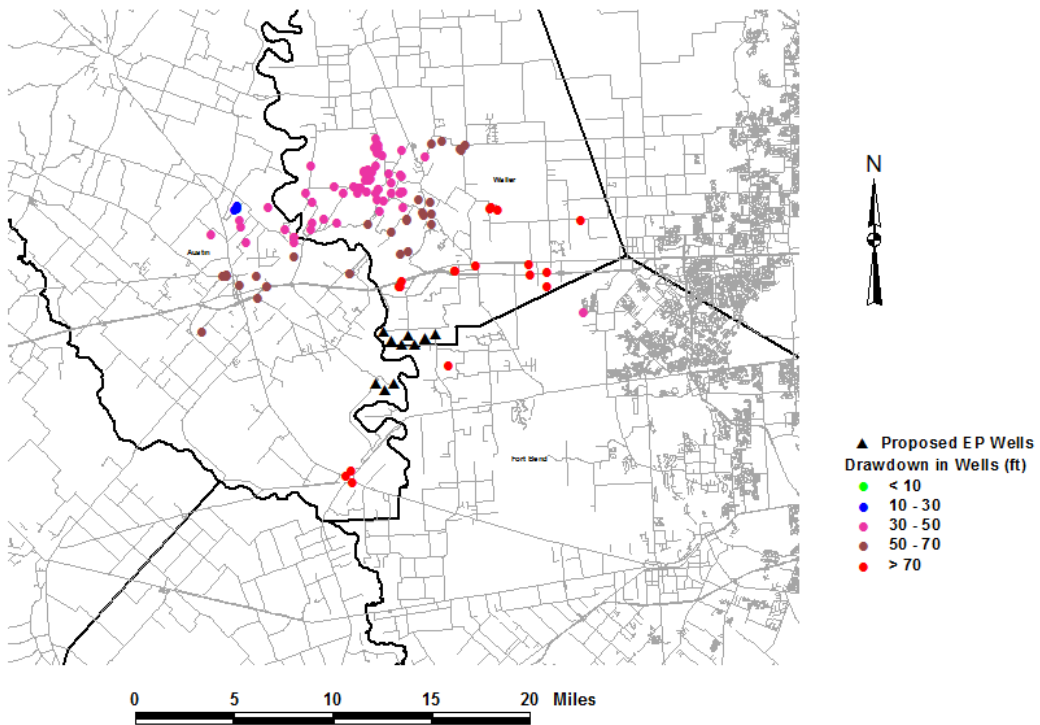


Figure C-17
Simulated Drawdown Attributed to EP Pumping - GAM
Scenario 3 (EP Pumping = 6 MGD) - Chicot Aquifer Wells (Layer 1)

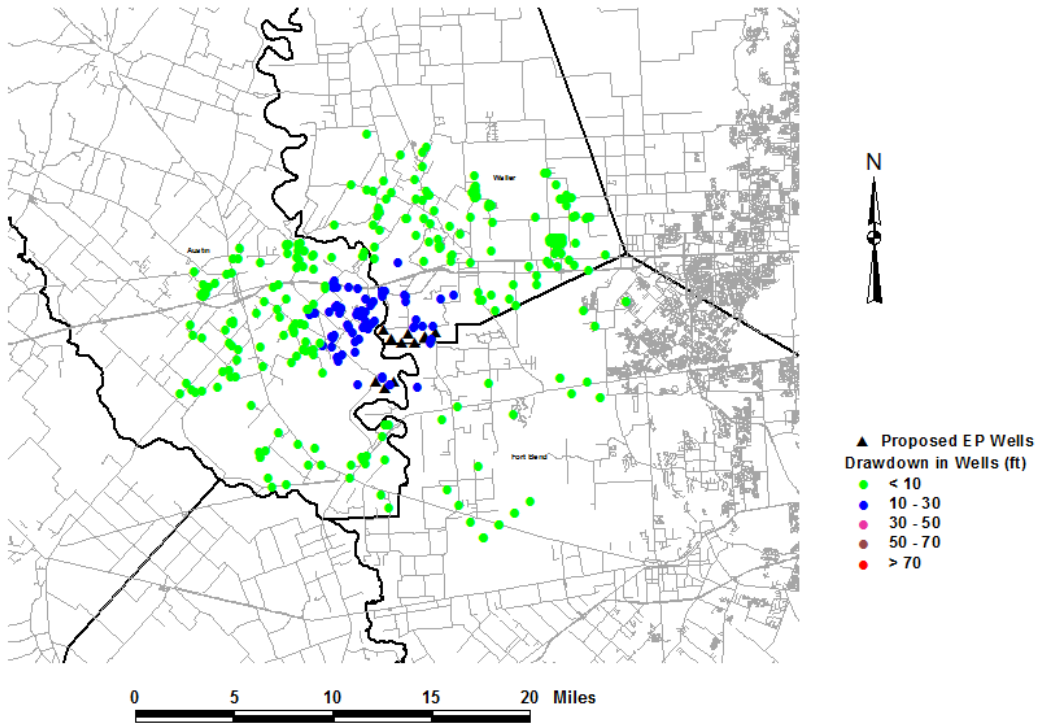


Figure C-18
Simulated Drawdown Attributed to EP Pumping - HAGM
Scenario 3 (EP Pumping = 6 MGD) - Chicot Aquifer Wells (Layer 1)

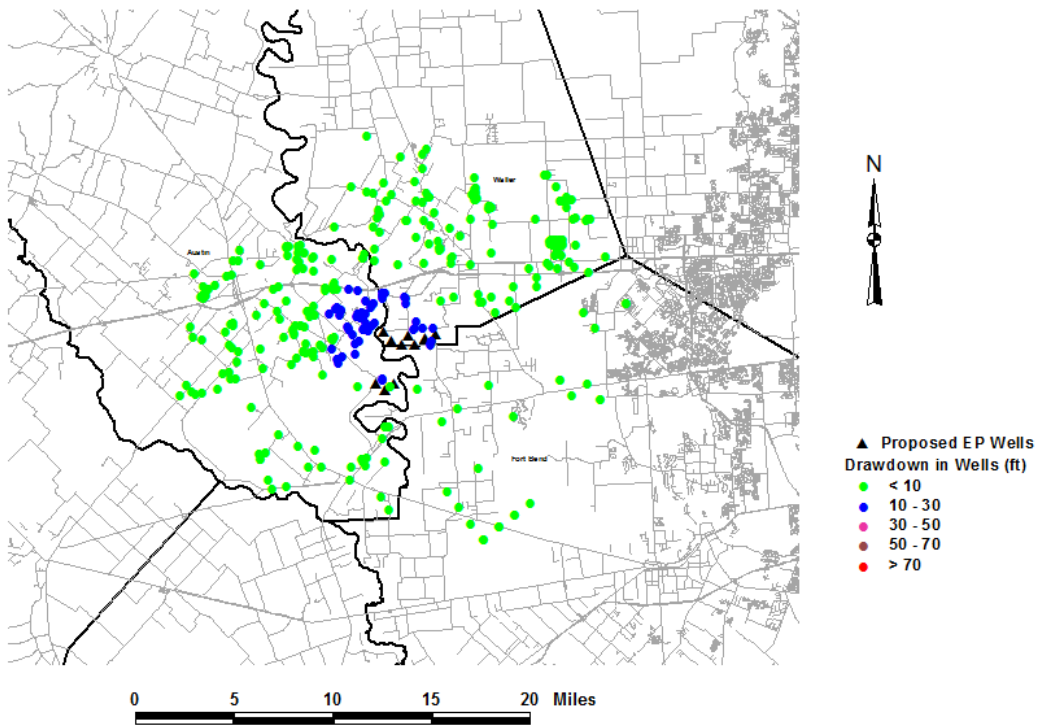


Figure C-19
Simulated Drawdown Attributed to EP Pumping - GAM
Scenario 10 (EP Pumping = 20 MGD) - Chicot Aquifer Wells (Layer 1)

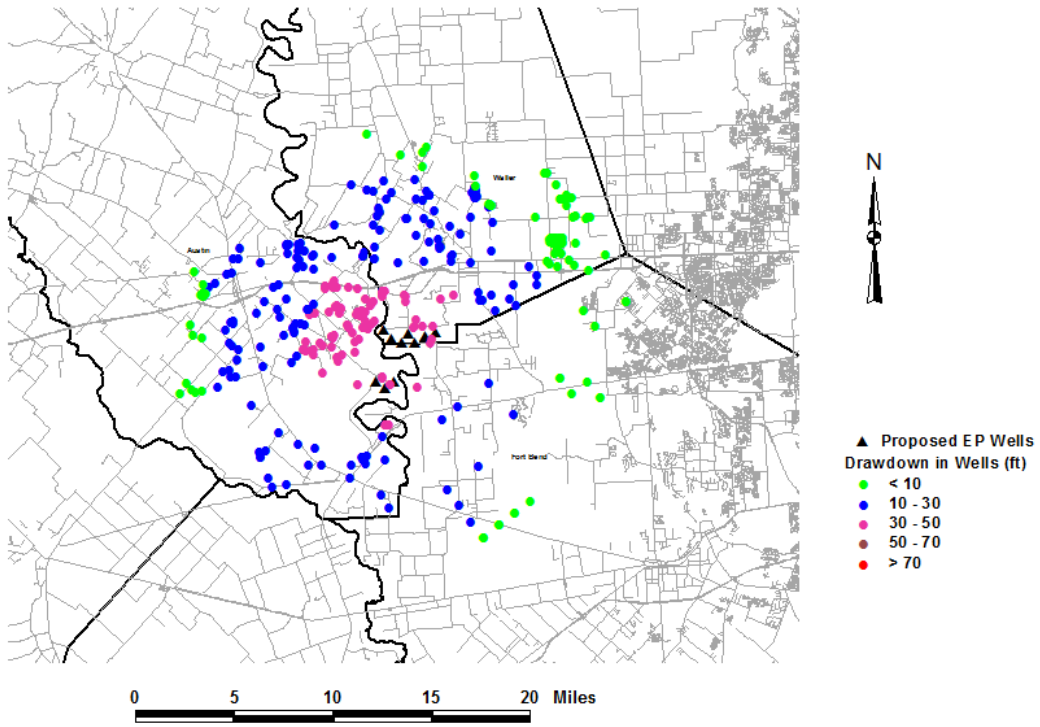


Figure C-20
Simulated Drawdown Attributed to EP Pumping - HAGM
Scenario 10 (EP Pumping = 20 MGD) - Chicot Aquifer Wells (Layer 1)

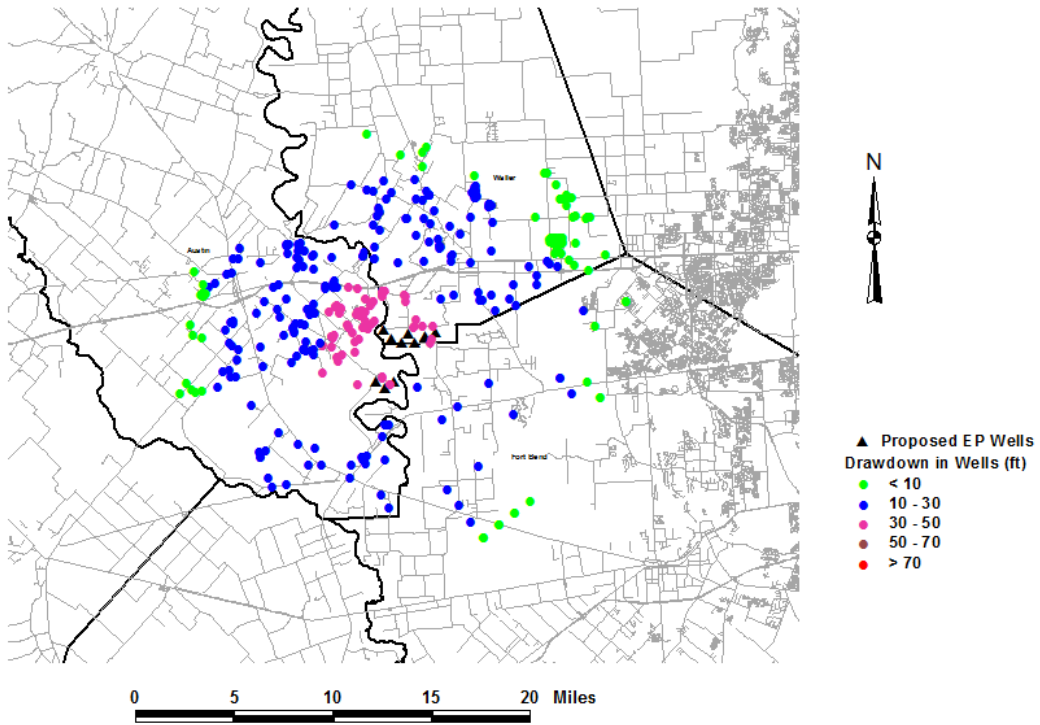


Figure C-21
Simulated Drawdown Attributed to EP Pumping - GAM
Scenario 31 (EP Pumping = 9.9 MGD) - Chicot Aquifer Wells (Layer 1)

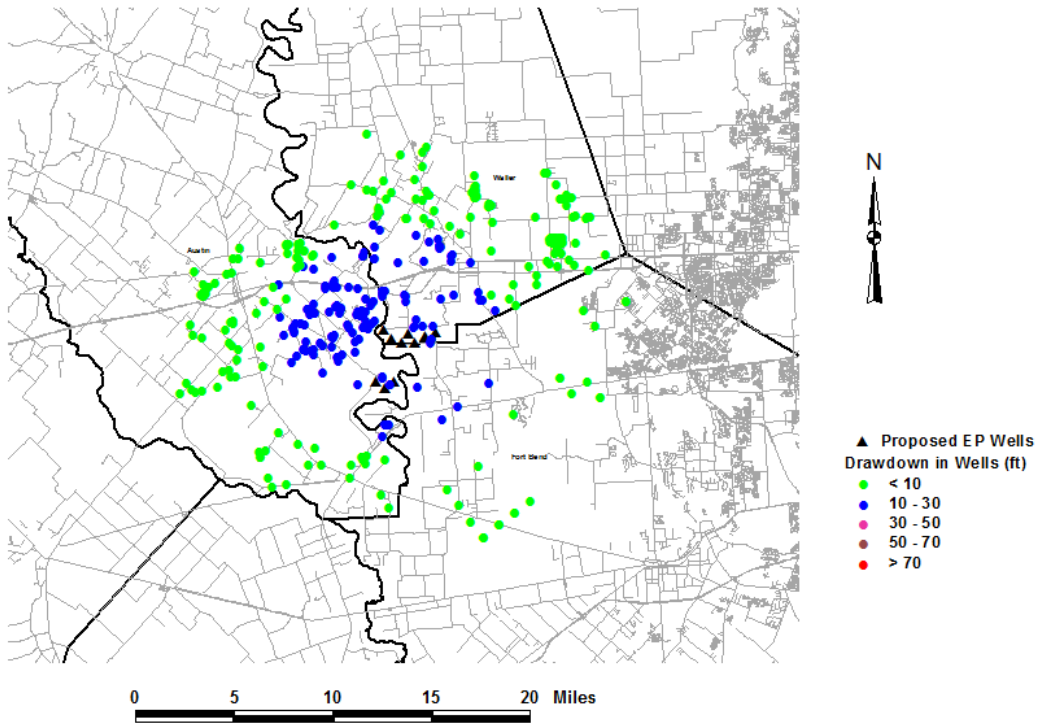


Figure C-22
Simulated Drawdown Attributed to EP Pumping - HAGM
Scenario 31 (EP Pumping = 9.9 MGD) - Chicot Aquifer Wells (Layer 1)

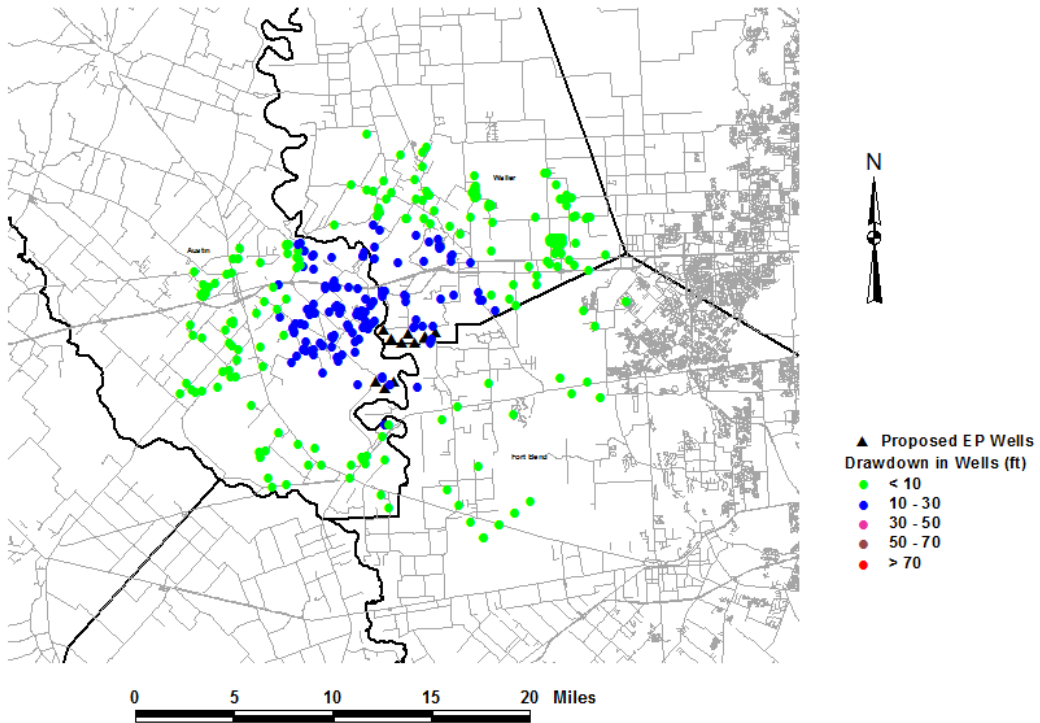


Figure C-23
Simulated Drawdown Attributed to EP Pumping - GAM
Scenario 3 (EP Pumping = 6 MGD) - Evangeline Aquifer Wells (Layer 2)

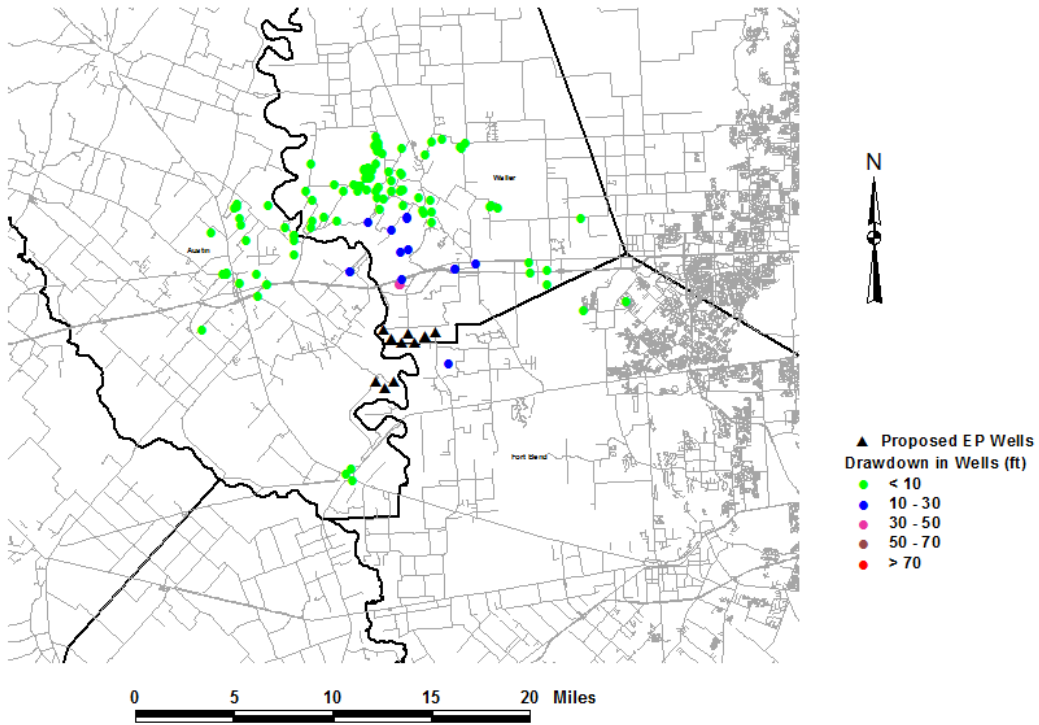


Figure C-24
Simulated Drawdown Attributed to EP Pumping - HAGM
Scenario 3 (EP Pumping = 6 MGD) - Evangeline Aquifer Wells (Layer 2)

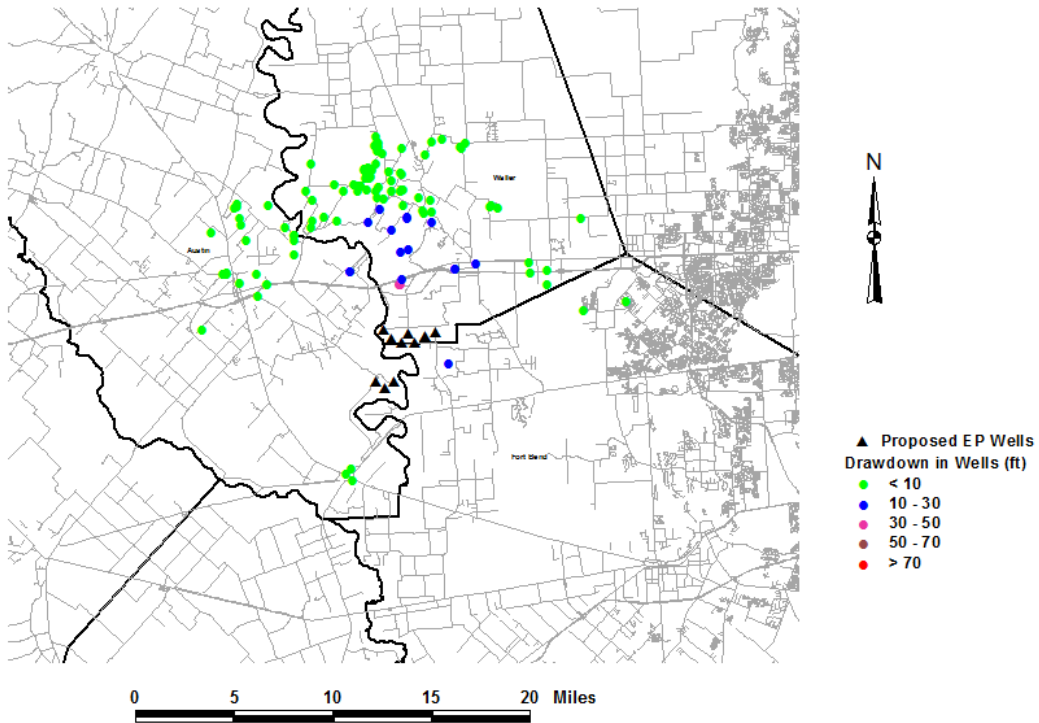


Figure C-25
Simulated Drawdown Attributed to EP Pumping - GAM
Scenario 10 (EP Pumping = 20 MGD) - Evangeline Aquifer Wells (Layer 2)

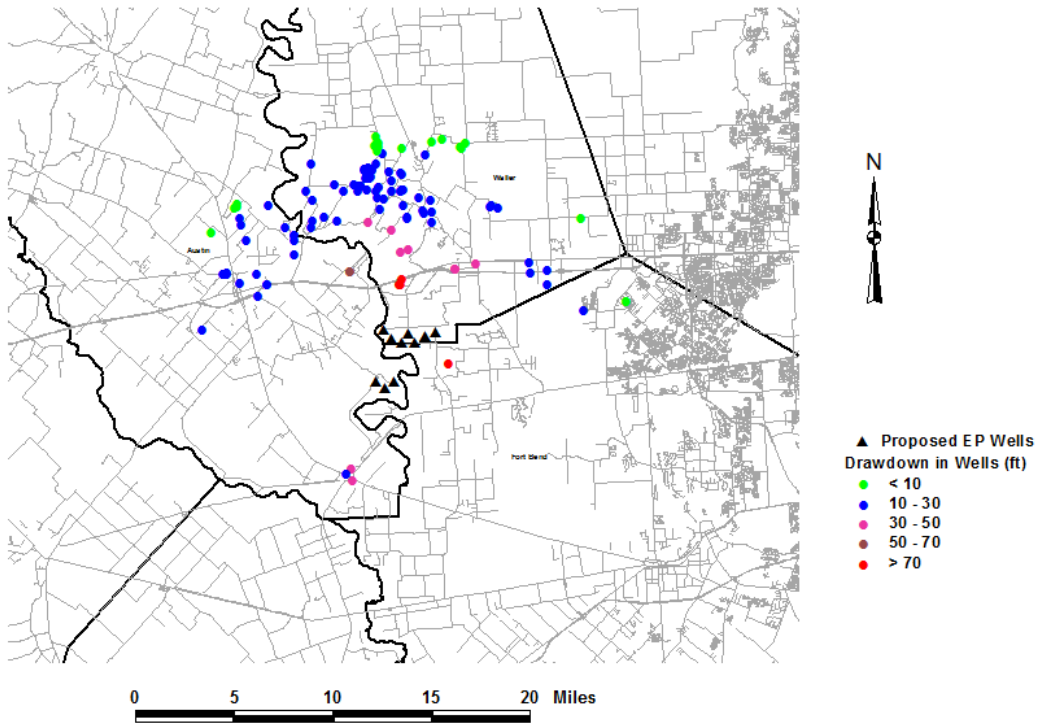


Figure C-26
Simulated Drawdown Attributed to EP Pumping - HAGM
Scenario 10 (EP Pumping = 20 MGD) - Evangeline Aquifer Wells (Layer 2)

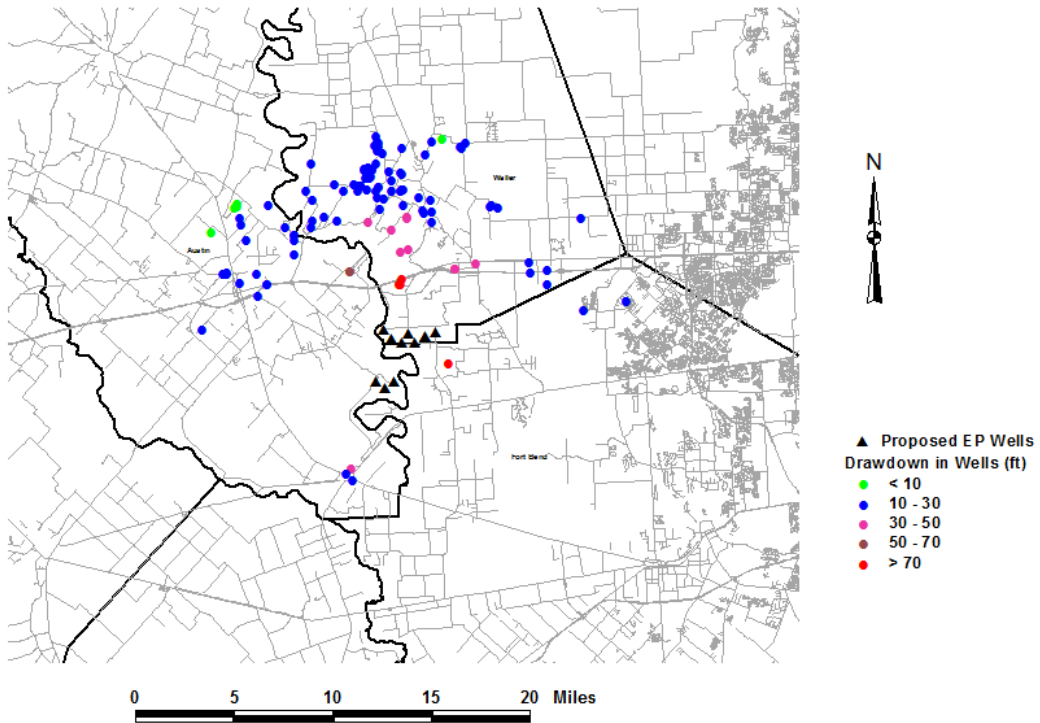


Figure C-27
Simulated Drawdown Attributed to EP Pumping - GAM
Scenario 31 (EP Pumping = 9.9 MGD) - Evangeline Aquifer Wells (Layer 2)

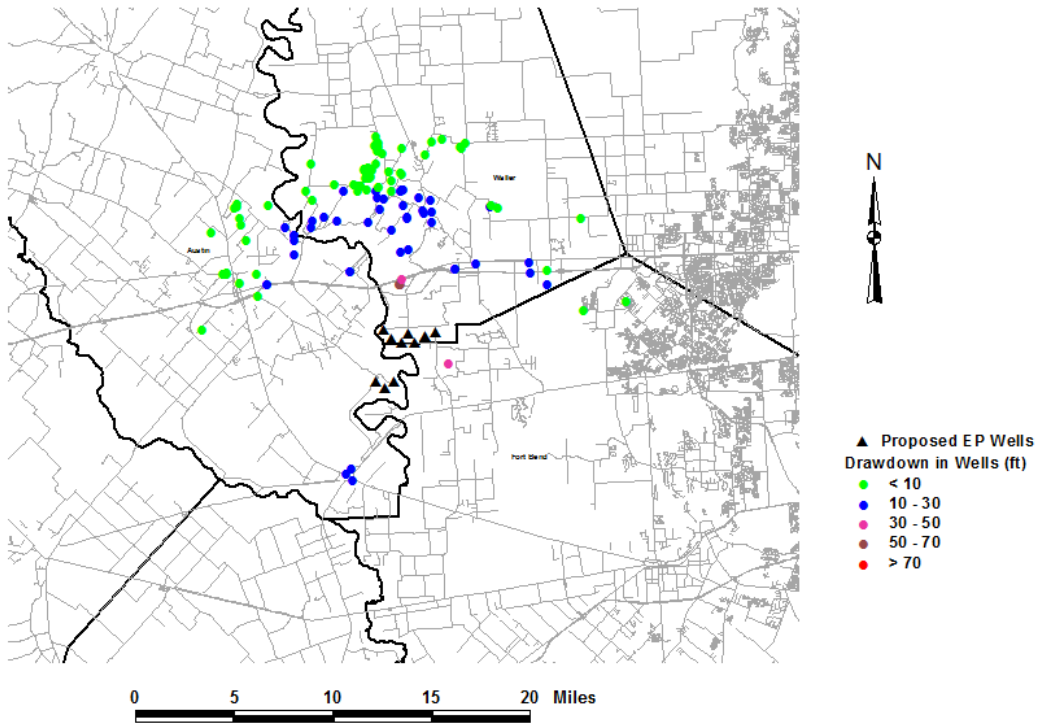
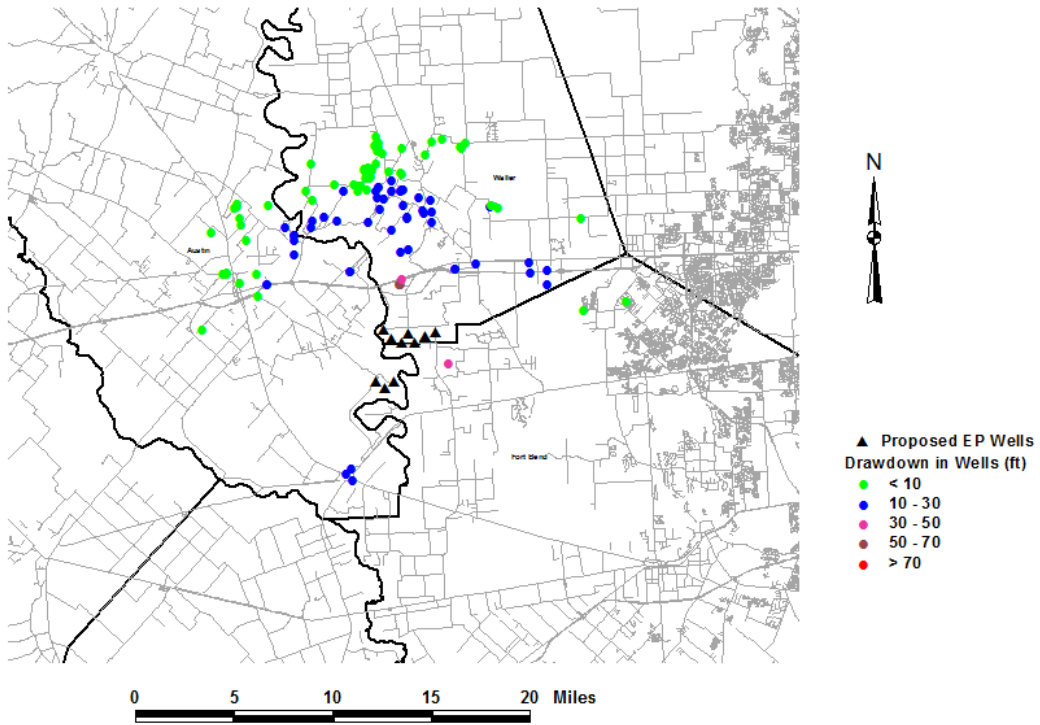


Figure C-28
Simulated Drawdown Attributed to EP Pumping - HAGM
Scenario 31 (EP Pumping = 9.9 MGD) - Evangeline Aquifer Wells (Layer 2)



**Appendix D – Tables and Hydrographs of County-Model Layer Drawdown
Estimates**

Table D-1
Austin County - Total Simulated Drawdown

Scenario	Draw down in 2060 from GAM (ft)				Drawdown in 2060 from HAGM (ft)			
	Chicot	Evangeline	Burkeville	Jasper	Chicot	Evangeline	Burkeville	Jasper
Baseline	17.13	9.94	10.69	20.29	29.00	18.51	18.57	34.79
1	18.20	10.86	11.59	20.71	29.98	19.43	19.47	34.88
2	19.41	11.98	12.69	21.13	31.11	20.54	20.56	34.98
3	20.20	12.61	13.31	21.53	31.86	21.17	21.19	35.07
4	21.24	13.52	14.21	21.94	32.85	22.09	22.09	35.16
5	22.42	14.63	15.30	22.36	33.98	23.20	23.19	35.25
6	23.20	15.27	15.93	22.76	34.74	23.84	23.81	35.34
7	24.22	16.19	16.83	23.17	35.73	24.76	24.72	35.43
8	25.30	17.27	17.89	23.60	36.73	25.82	25.76	35.53
9	26.61	18.62	19.21	24.03	37.95	27.16	27.08	35.62
10	27.69	19.71	20.28	24.46	38.95	28.22	28.13	35.72
11	18.09	10.75	11.48	20.51	29.85	19.30	19.35	34.82
12	19.19	11.76	12.46	20.73	30.85	20.29	20.32	34.84
13	19.88	12.29	12.98	20.93	31.47	20.81	20.83	34.87
14	20.82	13.09	13.77	21.15	32.33	21.60	21.61	34.89
15	21.90	14.09	14.74	21.37	33.33	22.59	22.58	34.92
16	22.58	14.62	15.26	21.58	33.96	23.11	23.09	34.94
17	23.50	15.43	16.05	21.79	34.82	23.90	23.87	34.96
18	23.55	15.32	15.94	21.77	34.52	23.66	23.63	34.92
19	23.82	15.47	16.10	21.77	34.44	23.68	23.65	34.88
20	23.87	15.36	15.99	21.75	34.14	23.43	23.41	34.84
21	26.98	19.19	20.41	47.51	38.03	27.42	27.59	85.83
22	26.12	18.50	20.41	72.20	36.98	26.42	26.87	138.53
23	25.64	18.24	20.74	92.82	36.28	25.89	26.57	184.05
24	24.89	17.58	20.75	117.06	35.36	24.93	25.88	236.05
25	24.22	17.10	20.99	143.70	34.44	24.13	25.36	292.17
26	23.50	16.59	21.13	166.75	33.52	23.32	24.81	341.99
27	22.63	15.90	21.13	191.44	32.47	22.32	24.09	394.63
28	22.14	15.64	21.46	212.07	31.77	21.79	23.79	440.16
29	21.39	14.98	21.48	236.30	30.85	20.83	23.10	492.15
30	20.39	14.06	21.23	259.34	29.71	19.61	22.15	541.94
31	21.62	14.10	14.78	22.21	33.17	22.65	22.64	35.20
32	21.19	13.61	14.27	21.27	32.65	22.11	22.11	34.91

Table D-2
Fort Bend County - Total Simulated Drawdown

Scenario	Drawdown in 2060 from GAM (ft)				Drawdown in 2060 from HAGM (ft)			
	Chicot	Evangeline	Burkeville	Jasper	Chicot	Evangeline	Burkeville	Jasper
Baseline	20.00	24.18	19.97	39.96	27.35	15.37	3.93	56.53
1	20.34	24.80	21.37	40.96	27.74	16.04	5.43	56.67
2	20.67	25.39	22.70	41.93	28.13	16.69	6.84	56.81
3	21.07	26.18	24.49	43.04	28.60	17.55	8.75	56.97
4	21.40	26.80	25.89	44.04	28.99	18.23	10.24	57.11
5	21.72	27.39	27.22	45.01	29.37	18.87	11.66	57.25
6	22.10	28.17	29.00	46.12	29.84	19.73	13.57	57.40
7	22.43	28.78	30.39	47.12	30.24	20.41	15.07	57.54
8	22.83	29.58	32.17	48.17	30.71	21.28	16.94	57.69
9	23.17	30.20	33.52	49.13	31.12	21.95	18.36	57.83
10	23.57	31.00	35.30	50.18	31.59	22.81	20.24	57.98
11	20.21	24.56	20.85	40.38	27.58	15.79	4.89	56.58
12	20.41	24.92	21.67	40.77	27.80	16.19	5.76	56.62
13	20.68	25.47	22.95	41.31	28.10	16.80	7.13	56.68
14	20.88	25.85	23.84	41.74	28.34	17.22	8.09	56.72
15	21.08	26.21	24.66	42.13	28.55	17.61	8.95	56.77
16	21.34	26.76	25.93	42.67	28.86	18.22	10.32	56.82
17	21.53	27.13	26.81	43.10	29.09	18.65	11.27	56.87
18	21.81	27.71	28.17	43.68	29.41	19.28	12.72	56.92
19	22.02	28.11	29.10	44.16	29.66	19.71	13.71	56.97
20	22.29	28.69	30.46	44.74	29.99	20.34	15.15	57.02
21	23.39	30.66	35.00	102.03	31.23	22.19	18.91	131.91
22	23.22	30.35	34.76	152.89	30.87	21.59	17.67	205.98
23	22.98	29.87	34.17	209.96	30.43	20.78	15.93	285.16
24	22.73	29.37	33.62	268.14	29.97	19.96	14.24	367.93
25	22.55	29.04	33.35	320.20	29.60	19.32	12.91	444.87
26	22.37	28.70	33.05	372.06	29.23	18.69	11.58	519.41
27	22.19	28.39	32.80	422.93	28.86	18.08	10.33	593.58
28	21.95	27.90	32.20	479.99	28.42	17.26	8.59	672.78
29	21.69	27.39	31.65	538.18	27.96	16.44	6.90	755.51
30	21.49	27.05	31.39	590.11	27.58	15.81	5.64	830.03
31	21.47	27.19	26.93	44.72	29.06	18.62	11.33	57.18
32	20.93	26.12	24.56	42.02	28.38	17.52	8.89	56.76

**Table D-3
Waller County - Total Simulated Drawdown**

Scenario	Draw down in 2060 from GAM (ft)				Drawdown in 2060 from HAGM (ft)			
	Chicot	Evangeline	Burkeville	Jasper	Chicot	Evangeline	Burkeville	Jasper
Baseline	7.48	7.97	8.58	25.49	26.20	32.10	32.50	50.23
1	8.02	9.02	9.62	25.98	26.77	33.20	33.59	50.31
2	8.48	9.88	10.47	26.43	27.26	34.09	34.48	50.38
3	9.01	10.99	11.55	26.95	27.84	35.24	35.63	50.47
4	9.54	12.04	12.59	27.44	28.41	36.34	36.72	50.55
5	9.99	12.90	13.43	27.89	28.90	37.23	37.61	50.62
6	10.52	14.00	14.51	28.41	29.47	38.38	38.75	50.70
7	11.04	15.05	15.55	28.90	30.04	39.48	39.85	50.78
8	11.34	15.54	16.04	29.32	30.38	39.99	40.36	50.86
9	11.62	15.99	16.49	29.73	30.71	40.47	40.83	50.93
10	11.92	16.49	16.98	30.16	31.05	40.98	41.35	51.00
11	7.35	7.51	8.13	25.44	25.60	31.30	31.70	50.20
12	7.14	6.85	7.49	25.36	24.92	30.29	30.70	50.17
13	7.01	6.45	7.09	25.34	24.32	29.54	29.95	50.15
14	6.87	6.00	6.65	25.30	23.71	28.73	29.15	50.12
15	6.66	5.35	6.02	25.22	23.02	27.72	28.14	50.09
16	6.52	4.95	5.62	25.21	22.42	26.96	27.39	50.06
17	6.37	4.50	5.18	25.16	21.81	26.15	26.59	50.03
18	6.61	4.88	5.55	25.36	22.07	26.56	26.99	50.04
19	6.83	5.22	5.89	25.53	22.32	26.91	27.34	50.05
20	7.07	5.61	6.27	25.73	22.58	27.32	27.75	50.06
21	11.59	15.85	17.01	57.20	30.53	39.98	40.54	95.56
22	11.32	15.41	17.18	82.58	30.08	39.18	39.93	138.42
23	10.99	14.75	17.22	110.20	29.55	38.11	39.06	182.99
24	10.85	14.65	17.66	132.65	29.24	37.67	38.80	222.58
25	10.49	13.96	17.51	154.29	28.71	36.65	37.96	261.76
26	10.16	13.34	17.55	181.34	28.18	35.64	37.15	306.20
27	9.88	12.90	17.72	206.72	27.73	34.84	36.53	349.09
28	9.54	12.24	17.76	234.35	27.20	33.77	35.66	393.65
29	9.40	12.13	18.19	256.81	26.89	33.33	35.40	433.21
30	9.29	12.11	18.82	283.95	26.61	32.95	35.21	477.63
31	9.74	12.72	13.25	27.75	28.57	37.00	37.38	50.58
32	6.63	5.41	6.07	25.19	23.38	28.12	28.54	50.10

**Table D-4
Austin County - Drawdown Attributable to EP Pumping**

Scenario	Drawdown in 2060 from GAM (ft)				Drawdown in 2060 from HAGM (ft)			
	Chicot	Evangeline	Burkeville	Jasper	Chicot	Evangeline	Burkeville	Jasper
Baseline	0	0	0	0	0	0	0	0
1	1.07	0.92	0.90	0.42	0.98	0.92	0.90	0.09
2	2.28	2.04	2.00	0.84	2.11	2.03	1.99	0.19
3	3.07	2.67	2.62	1.24	2.86	2.66	2.62	0.28
4	4.11	3.58	3.52	1.65	3.85	3.58	3.52	0.37
5	5.29	4.69	4.61	2.07	4.98	4.69	4.62	0.46
6	6.07	5.33	5.24	2.47	5.74	5.33	5.24	0.55
7	7.09	6.25	6.14	2.88	6.73	6.25	6.15	0.64
8	8.17	7.33	7.20	3.31	7.73	7.31	7.19	0.74
9	9.48	8.68	8.52	3.74	8.95	8.65	8.51	0.83
10	10.56	9.77	9.59	4.17	9.95	9.71	9.56	0.93
11	0.96	0.81	0.79	0.22	0.85	0.79	0.78	0.03
12	2.06	1.82	1.77	0.44	1.85	1.78	1.75	0.05
13	2.75	2.35	2.29	0.64	2.47	2.30	2.26	0.08
14	3.69	3.15	3.08	0.86	3.33	3.09	3.04	0.10
15	4.77	4.15	4.05	1.08	4.33	4.08	4.01	0.13
16	5.45	4.68	4.57	1.29	4.96	4.60	4.52	0.15
17	6.37	5.49	5.36	1.50	5.82	5.39	5.30	0.17
18	6.42	5.38	5.25	1.48	5.52	5.15	5.06	0.13
19	6.69	5.53	5.41	1.48	5.44	5.17	5.08	0.09
20	6.74	5.42	5.30	1.46	5.14	4.92	4.84	0.05
21	9.85	9.25	9.72	27.22	9.03	8.91	9.02	51.04
22	8.99	8.56	9.72	51.91	7.98	7.91	8.30	103.74
23	8.51	8.30	10.05	72.53	7.28	7.38	8.00	149.26
24	7.76	7.64	10.06	96.77	6.36	6.42	7.31	201.26
25	7.09	7.16	10.30	123.41	5.44	5.62	6.79	257.38
26	6.37	6.65	10.44	146.46	4.52	4.81	6.24	307.20
27	5.50	5.96	10.44	171.15	3.47	3.81	5.52	359.84
28	5.01	5.70	10.77	191.78	2.77	3.28	5.22	405.37
29	4.26	5.04	10.79	216.01	1.85	2.32	4.53	457.36
30	3.26	4.12	10.54	239.05	0.71	1.10	3.58	507.15
31	4.49	4.16	4.09	1.92	4.17	4.14	4.07	0.41
32	4.06	3.67	3.58	0.98	3.65	3.60	3.54	0.12

Table D-5
Fort Bend County - Drawdown Attributable to EP Pumping

Scenario	Draw down in 2060 from GAM (ft)				Drawdown in 2060 from HAGM (ft)			
	Chicot	Evangeline	Burkeville	Jasper	Chicot	Evangeline	Burkeville	Jasper
Baseline	0	0	0	0	0	0	0	0
1	0.34	0.62	1.40	1.00	0.39	0.67	1.50	0.14
2	0.67	1.21	2.73	1.97	0.78	1.32	2.91	0.28
3	1.07	2.00	4.52	3.08	1.25	2.18	4.82	0.44
4	1.40	2.62	5.92	4.08	1.64	2.86	6.31	0.58
5	1.72	3.21	7.25	5.05	2.02	3.50	7.73	0.72
6	2.10	3.99	9.03	6.16	2.49	4.36	9.64	0.87
7	2.43	4.60	10.42	7.16	2.89	5.04	11.14	1.01
8	2.83	5.40	12.20	8.21	3.36	5.91	13.01	1.16
9	3.17	6.02	13.55	9.17	3.77	6.58	14.43	1.30
10	3.57	6.82	15.33	10.22	4.24	7.44	16.31	1.45
11	0.21	0.38	0.88	0.42	0.23	0.42	0.96	0.05
12	0.41	0.74	1.70	0.81	0.45	0.82	1.83	0.09
13	0.68	1.29	2.98	1.35	0.75	1.43	3.20	0.15
14	0.88	1.67	3.87	1.78	0.99	1.85	4.16	0.19
15	1.08	2.03	4.69	2.17	1.20	2.24	5.02	0.24
16	1.34	2.58	5.96	2.71	1.51	2.85	6.39	0.29
17	1.53	2.95	6.84	3.14	1.74	3.28	7.34	0.34
18	1.81	3.53	8.20	3.72	2.06	3.91	8.79	0.39
19	2.02	3.93	9.13	4.20	2.31	4.34	9.78	0.44
20	2.29	4.51	10.49	4.78	2.64	4.97	11.22	0.49
21	3.39	6.48	15.03	62.07	3.88	6.82	14.98	75.38
22	3.22	6.17	14.79	112.93	3.52	6.22	13.74	149.45
23	2.98	5.69	14.20	170.00	3.08	5.41	12.00	228.63
24	2.73	5.19	13.65	228.18	2.62	4.59	10.31	311.40
25	2.55	4.86	13.38	280.24	2.25	3.95	8.98	388.34
26	2.37	4.52	13.08	332.10	1.88	3.32	7.65	462.88
27	2.19	4.21	12.83	382.97	1.51	2.71	6.40	537.05
28	1.95	3.72	12.23	440.03	1.07	1.89	4.66	616.25
29	1.69	3.21	11.68	498.22	0.61	1.07	2.97	698.98
30	1.49	2.87	11.42	550.15	0.23	0.44	1.71	773.50
31	1.47	3.01	6.96	4.76	1.71	3.25	7.40	0.65
32	0.93	1.94	4.59	2.06	1.03	2.15	4.96	0.23

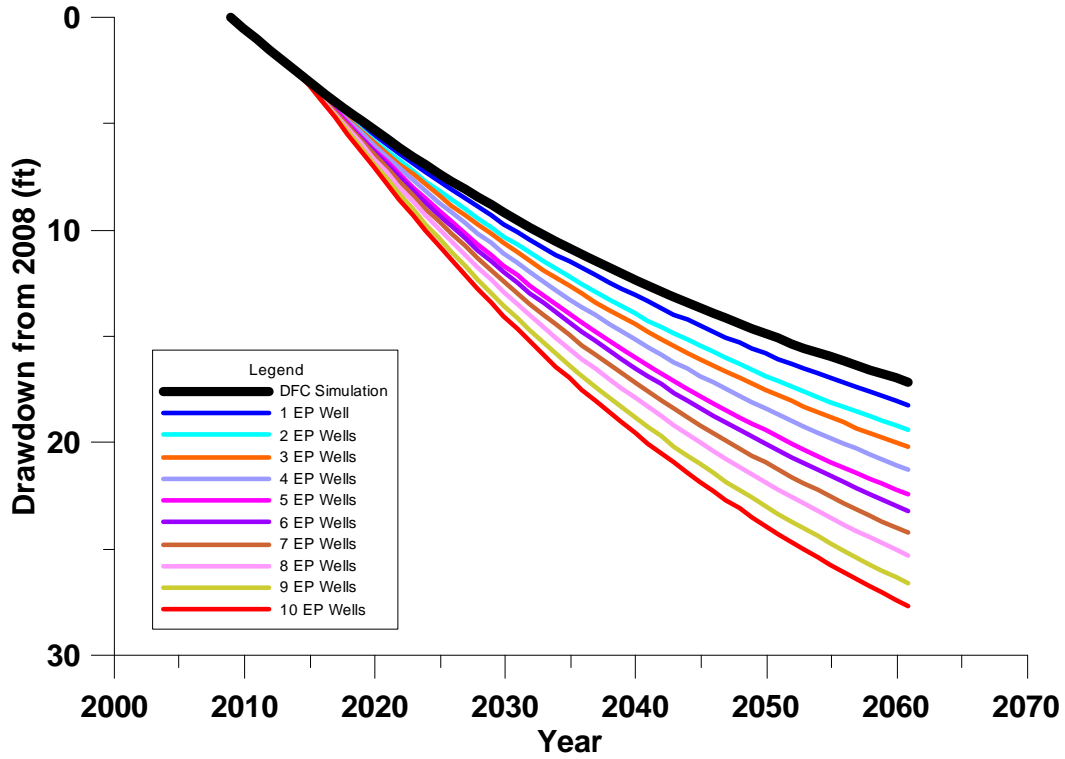
Table D-6
Waller County - Drawdown Attributable to EP Pumping

Scenario	Drawdown in 2060 from GAM (ft)				Drawdown in 2060 from HAGM (ft)			
	Chicot	Evangeline	Burkeville	Jasper	Chicot	Evangeline	Burkeville	Jasper
Baseline	0	0	0	0	0	0	0	0
1	0.54	1.05	1.04	0.49	0.57	1.10	1.09	0.08
2	1.00	1.91	1.89	0.94	1.06	1.99	1.98	0.15
3	1.53	3.02	2.97	1.46	1.64	3.14	3.13	0.24
4	2.06	4.07	4.01	1.95	2.21	4.24	4.22	0.32
5	2.51	4.93	4.85	2.40	2.70	5.13	5.11	0.39
6	3.04	6.03	5.93	2.92	3.27	6.28	6.25	0.47
7	3.56	7.08	6.97	3.41	3.84	7.38	7.35	0.55
8	3.86	7.57	7.46	3.83	4.18	7.89	7.86	0.63
9	4.14	8.02	7.91	4.24	4.51	8.37	8.33	0.70
10	4.44	8.52	8.40	4.67	4.85	8.88	8.85	0.77
11	-0.13	-0.46	-0.45	-0.05	-0.60	-0.80	-0.80	-0.03
12	-0.34	-1.12	-1.09	-0.13	-1.28	-1.81	-1.80	-0.06
13	-0.47	-1.52	-1.49	-0.15	-1.88	-2.56	-2.55	-0.08
14	-0.61	-1.97	-1.93	-0.19	-2.49	-3.37	-3.35	-0.11
15	-0.82	-2.62	-2.56	-0.27	-3.18	-4.38	-4.36	-0.14
16	-0.96	-3.02	-2.96	-0.28	-3.78	-5.14	-5.11	-0.17
17	-1.11	-3.47	-3.40	-0.33	-4.39	-5.95	-5.91	-0.20
18	-0.87	-3.09	-3.03	-0.13	-4.13	-5.54	-5.51	-0.19
19	-0.65	-2.75	-2.69	0.04	-3.88	-5.19	-5.16	-0.18
20	-0.41	-2.36	-2.31	0.24	-3.62	-4.78	-4.75	-0.17
21	4.11	7.88	8.43	31.71	4.33	7.88	8.04	45.33
22	3.84	7.44	8.60	57.09	3.88	7.08	7.43	88.19
23	3.51	6.78	8.64	84.71	3.35	6.01	6.56	132.76
24	3.37	6.68	9.08	107.16	3.04	5.57	6.30	172.35
25	3.01	5.99	8.93	128.80	2.51	4.55	5.46	211.53
26	2.68	5.37	8.97	155.85	1.98	3.54	4.65	255.97
27	2.40	4.93	9.14	181.23	1.53	2.74	4.03	298.86
28	2.06	4.27	9.18	208.86	1.00	1.67	3.16	343.42
29	1.92	4.16	9.61	231.32	0.69	1.23	2.90	382.98
30	1.81	4.14	10.24	258.46	0.41	0.85	2.71	427.40
31	2.26	4.75	4.67	2.26	2.37	4.90	4.88	0.35
32	-0.85	-2.56	-2.51	-0.30	-2.82	-3.98	-3.96	-0.13

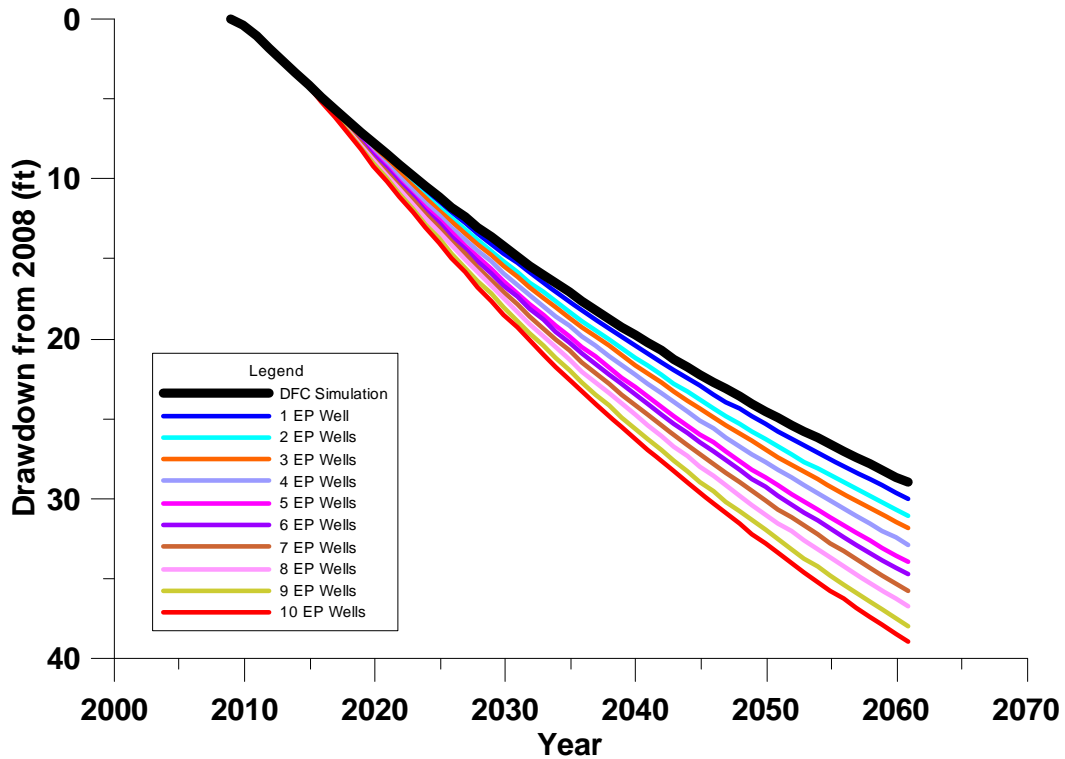
Appendix D - Drawdown Graphs

Figure Number	Aquifer	Location	Scenario	Model	Page Number
D1	Chicot	Austin County	EP Pumping Plus MAG	GAM	1
D2	Chicot	Austin County	EP Pumping Plus MAG	HAGM	1
D3	Evangelina	Austin County	EP Pumping Plus MAG	GAM	2
D4	Evangelina	Austin County	EP Pumping Plus MAG	HAGM	2
D5	Jasper	Austin County	EP Pumping Plus MAG	GAM	3
D6	Jasper	Austin County	EP Pumping Plus MAG	HAGM	3
D7	Chicot	Fort Bend County	EP Pumping Plus MAG	GAM	4
D8	Chicot	Fort Bend County	EP Pumping Plus MAG	HAGM	4
D9	Evangelina	Fort Bend County	EP Pumping Plus MAG	GAM	5
D10	Evangelina	Fort Bend County	EP Pumping Plus MAG	HAGM	5
D11	Jasper	Fort Bend County	EP Pumping Plus MAG	GAM	6
D12	Jasper	Fort Bend County	EP Pumping Plus MAG	HAGM	6
D13	Chicot	Waller County	EP Pumping Plus MAG	GAM	7
D14	Chicot	Waller County	EP Pumping Plus MAG	HAGM	7
D15	Evangelina	Waller County	EP Pumping Plus MAG	GAM	8
D16	Evangelina	Waller County	EP Pumping Plus MAG	HAGM	8
D17	Jasper	Waller County	EP Pumping Plus MAG	GAM	9
D18	Jasper	Waller County	EP Pumping Plus MAG	HAGM	9
D19	Chicot	Austin County	EP Pumping Within MAG	GAM	10
D20	Chicot	Austin County	EP Pumping Within MAG	HAGM	10
D21	Evangelina	Austin County	EP Pumping Within MAG	GAM	11
D22	Evangelina	Austin County	EP Pumping Within MAG	HAGM	11
D23	Jasper	Austin County	EP Pumping Within MAG	GAM	12
D24	Jasper	Austin County	EP Pumping Within MAG	HAGM	12
D25	Chicot	Fort Bend County	EP Pumping Within MAG	GAM	13
D26	Chicot	Fort Bend County	EP Pumping Within MAG	HAGM	13
D27	Evangelina	Fort Bend County	EP Pumping Within MAG	GAM	14
D28	Evangelina	Fort Bend County	EP Pumping Within MAG	HAGM	14
D29	Jasper	Fort Bend County	EP Pumping Within MAG	GAM	15
D30	Jasper	Fort Bend County	EP Pumping Within MAG	HAGM	15
D31	Chicot	Waller County	EP Pumping Within MAG	GAM	16
D32	Chicot	Waller County	EP Pumping Within MAG	HAGM	16
D33	Evangelina	Waller County	EP Pumping Within MAG	GAM	17
D34	Evangelina	Waller County	EP Pumping Within MAG	HAGM	17
D35	Jasper	Waller County	EP Pumping Within MAG	GAM	18
D36	Jasper	Waller County	EP Pumping Within MAG	HAGM	18
D37	Chicot	Austin County	Evangelina/Jasper Scenarios	GAM	19
D38	Chicot	Austin County	Evangelina/Jasper Scenarios	HAGM	19
D39	Evangelina	Austin County	Evangelina/Jasper Scenarios	GAM	20
D40	Evangelina	Austin County	Evangelina/Jasper Scenarios	HAGM	20
D41	Jasper	Austin County	Evangelina/Jasper Scenarios	GAM	21
D42	Jasper	Austin County	Evangelina/Jasper Scenarios	HAGM	21
D43	Chicot	Fort Bend County	Evangelina/Jasper Scenarios	GAM	22
D44	Chicot	Fort Bend County	Evangelina/Jasper Scenarios	HAGM	22
D45	Evangelina	Fort Bend County	Evangelina/Jasper Scenarios	GAM	23
D46	Evangelina	Fort Bend County	Evangelina/Jasper Scenarios	HAGM	23
D47	Jasper	Fort Bend County	Evangelina/Jasper Scenarios	GAM	24
D48	Jasper	Fort Bend County	Evangelina/Jasper Scenarios	HAGM	24
D49	Chicot	Waller County	Evangelina/Jasper Scenarios	GAM	25
D50	Chicot	Waller County	Evangelina/Jasper Scenarios	HAGM	25
D51	Evangelina	Waller County	Evangelina/Jasper Scenarios	GAM	26
D52	Evangelina	Waller County	Evangelina/Jasper Scenarios	HAGM	26
D53	Jasper	Waller County	Evangelina/Jasper Scenarios	GAM	27
D54	Jasper	Waller County	Evangelina/Jasper Scenarios	HAGM	27
D55	Chicot	Austin County	Conversion Schedule	GAM	28
D56	Chicot	Austin County	Conversion Schedule	HAGM	28
D57	Evangelina	Austin County	Conversion Schedule	GAM	29
D58	Evangelina	Austin County	Conversion Schedule	HAGM	29
D59	Jasper	Austin County	Conversion Schedule	GAM	30
D60	Jasper	Austin County	Conversion Schedule	HAGM	30
D61	Chicot	Fort Bend County	Conversion Schedule	GAM	31
D62	Chicot	Fort Bend County	Conversion Schedule	HAGM	31
D63	Evangelina	Fort Bend County	Conversion Schedule	GAM	32
D64	Evangelina	Fort Bend County	Conversion Schedule	HAGM	32
D65	Jasper	Fort Bend County	Conversion Schedule	GAM	33
D66	Jasper	Fort Bend County	Conversion Schedule	HAGM	33
D67	Chicot	Waller County	Conversion Schedule	GAM	34
D68	Chicot	Waller County	Conversion Schedule	HAGM	34
D69	Evangelina	Waller County	Conversion Schedule	GAM	35
D70	Evangelina	Waller County	Conversion Schedule	HAGM	35
D71	Jasper	Waller County	Conversion Schedule	GAM	36
D72	Jasper	Waller County	Conversion Schedule	HAGM	36

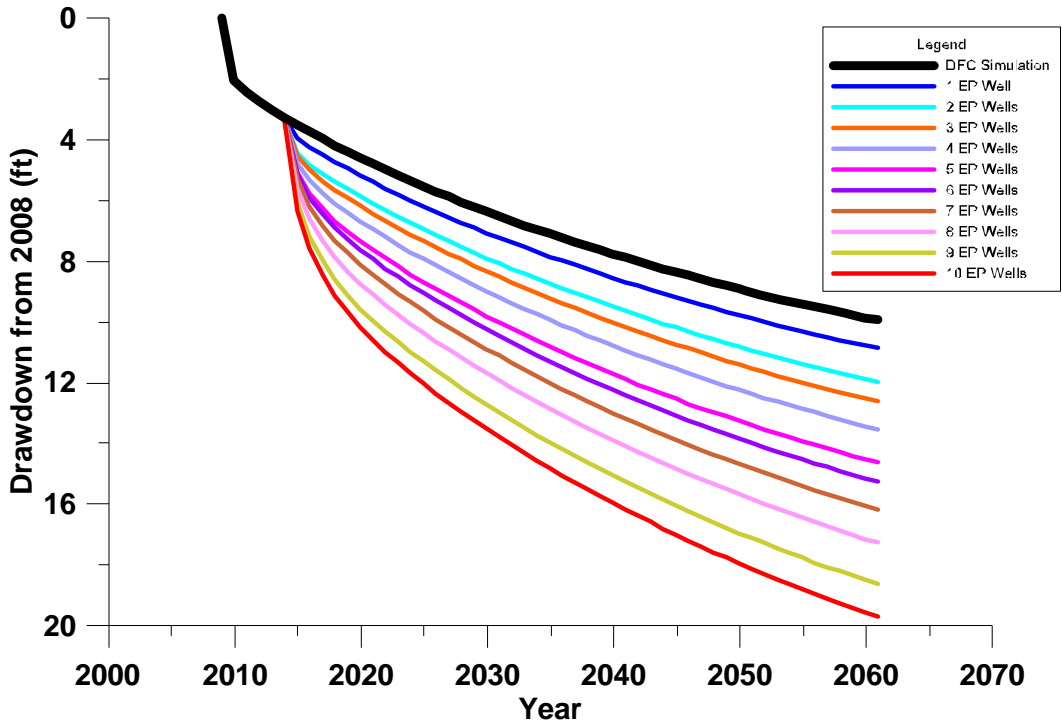
**Figure D-1
Austin County - Chicot
Electro Purification Pumping in Addition to MAG (GAM)**



**Figure D-2
Austin County - Chicot
Electro Purification Pumping in Addition to MAG (HAGM)**



**Figure D-3
Austin County - Evangeline
Electro Purification Pumping in Addition to MAG (GAM)**



**Figure D-4
Austin County - Evangeline
Electro Purification Pumping in Addition to MAG (HAGM)**

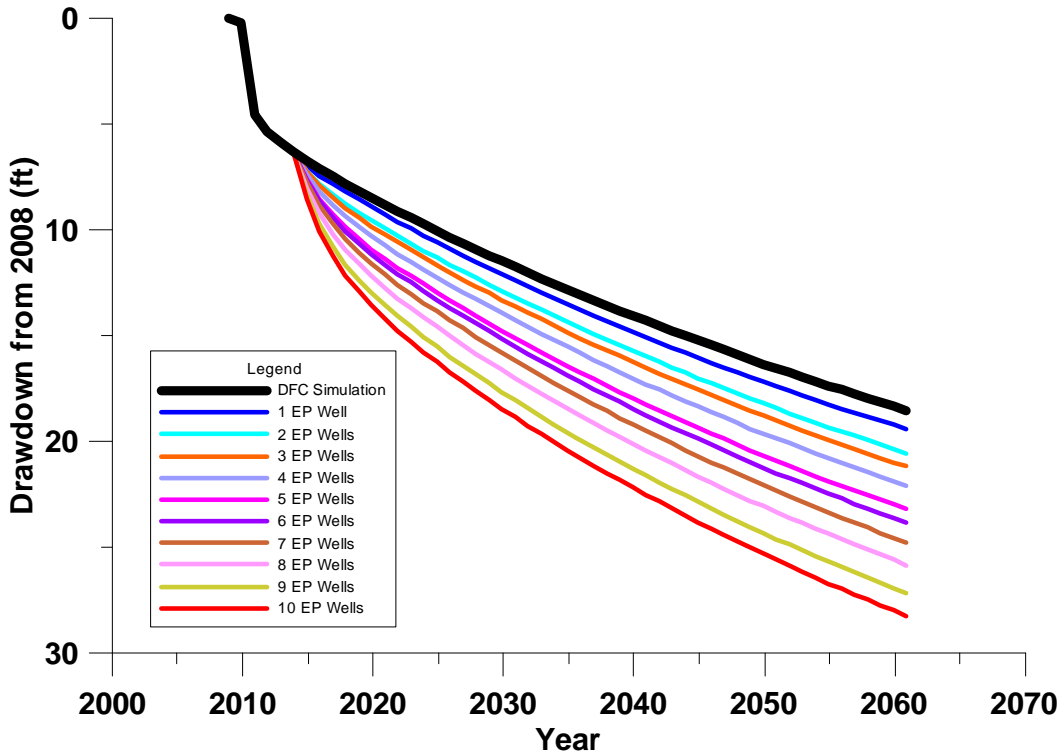


Figure D-5
Austin County - Jasper
Electro Purification Pumping in Addition to MAG (GAM)

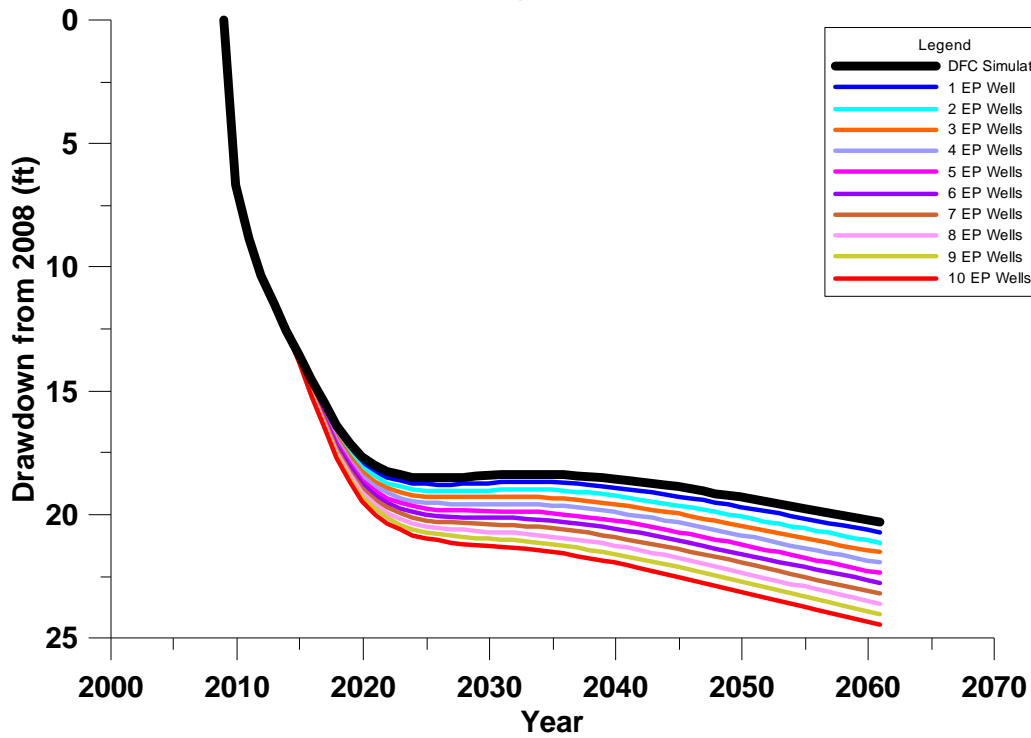


Figure D-6
Austin County - Jasper
Electro Purification Pumping in Addition to MAG (HAGM)

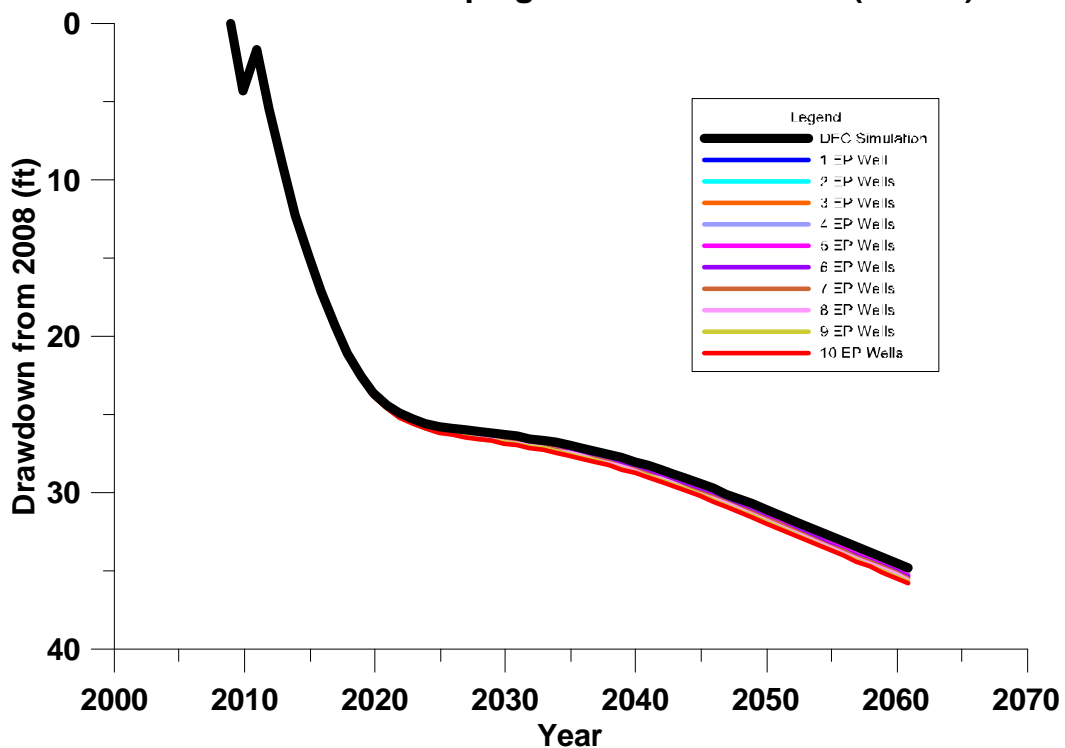


Figure D-7
Fort Bend County - Chicot
Electro Purification Pumping in Addition to MAG (GAM)

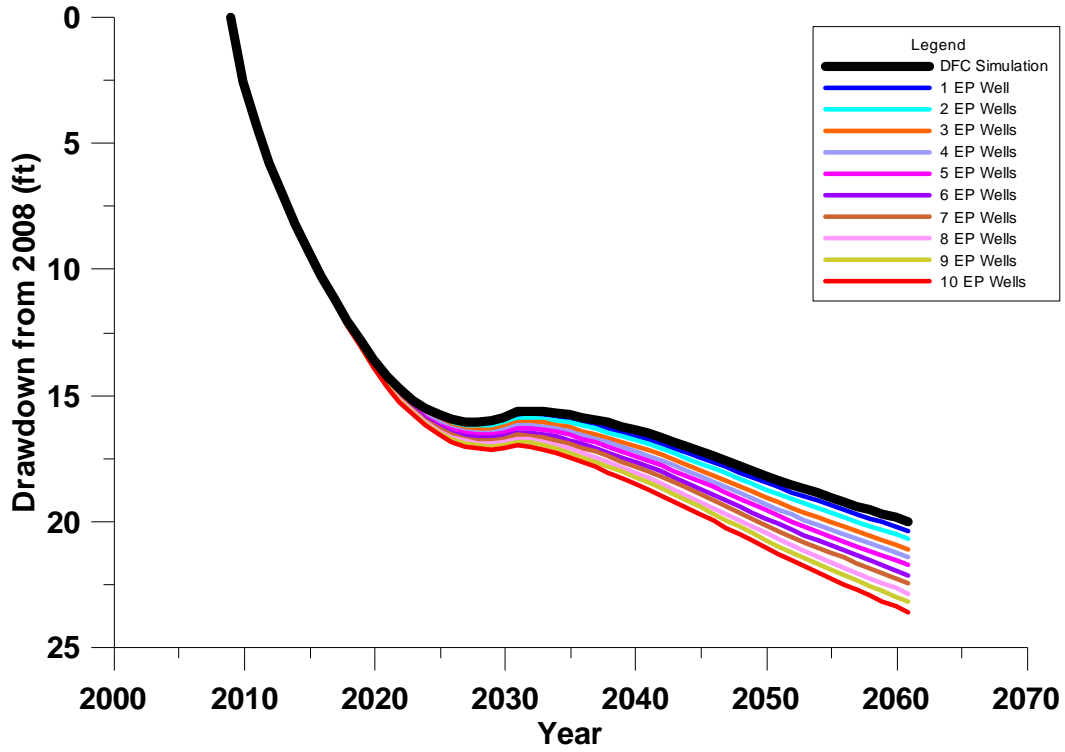


Figure D-8
Fort Bend County - Chicot
Electro Purification Pumping in Addition to MAG (HAGM)

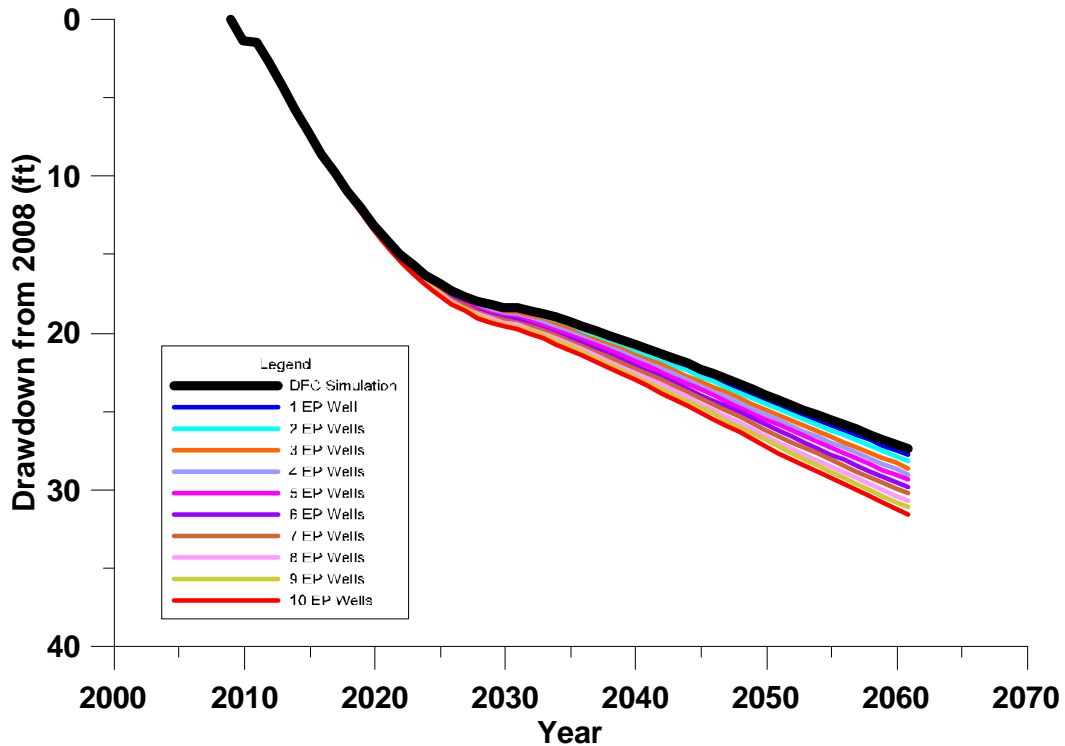


Figure D-9
Fort Bend County - Evangeline
Electro Purification Pumping in Addition to MAG (GAM)

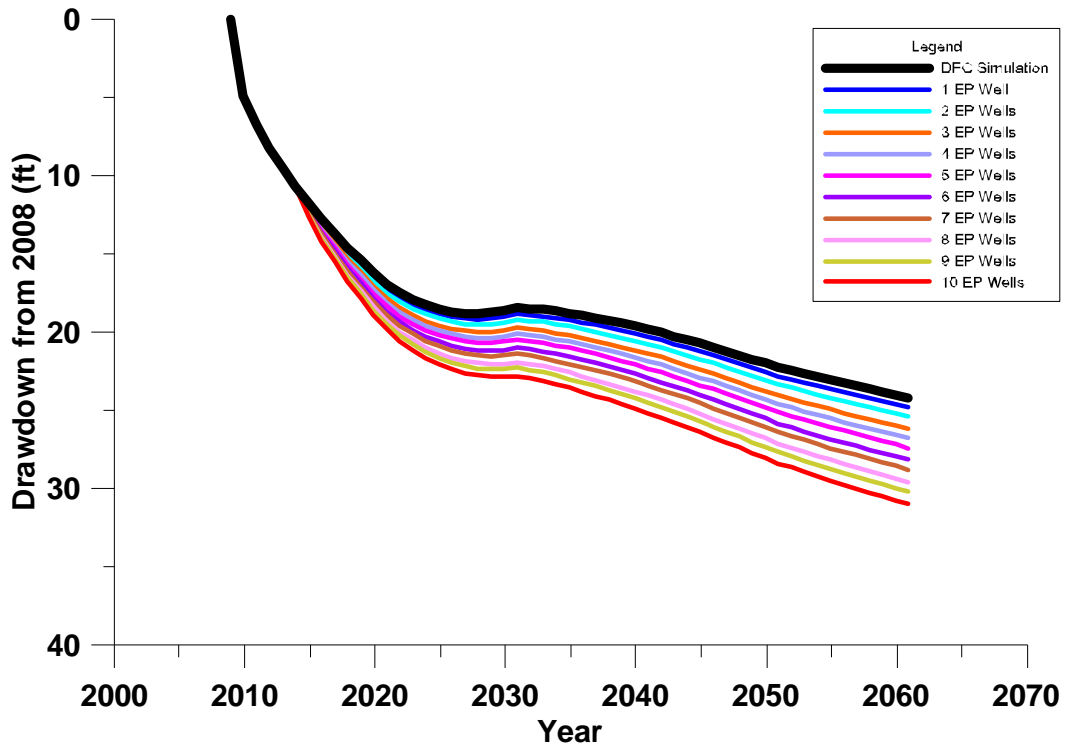


Figure D-10
Fort Bend County - Evangeline
Electro Purification Pumping in Addition to MAG (HAGM)

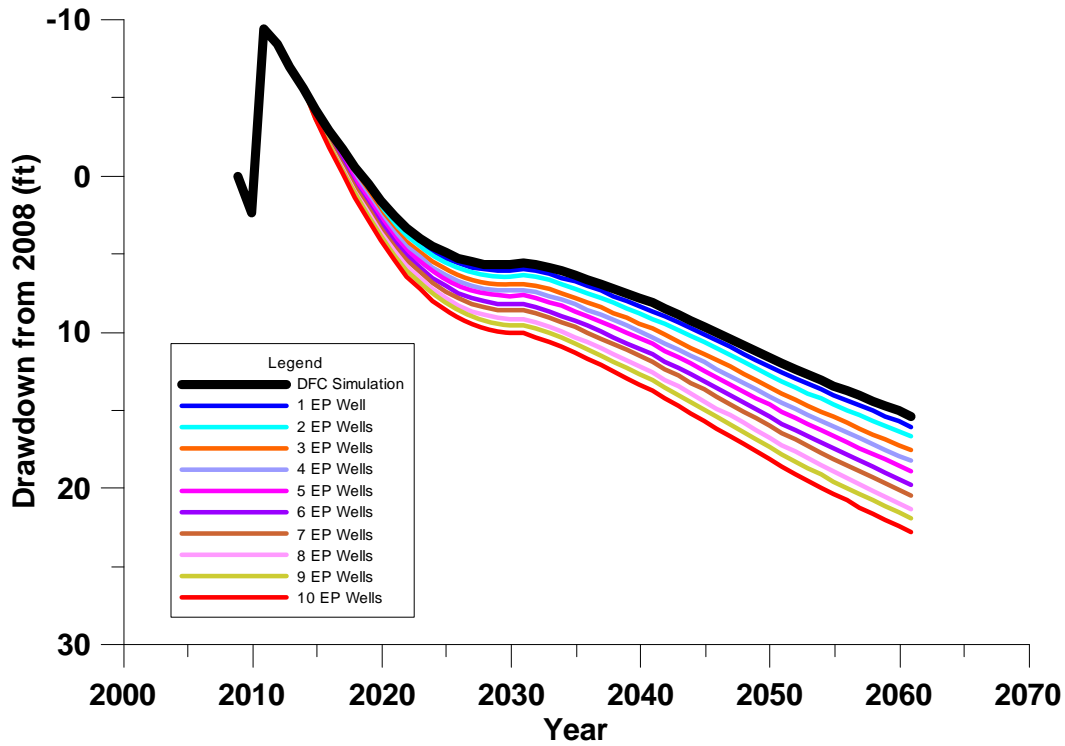


Figure D-11
Fort Bend County - Jasper
Electro Purification Pumping in Addition to MAG (GAM)

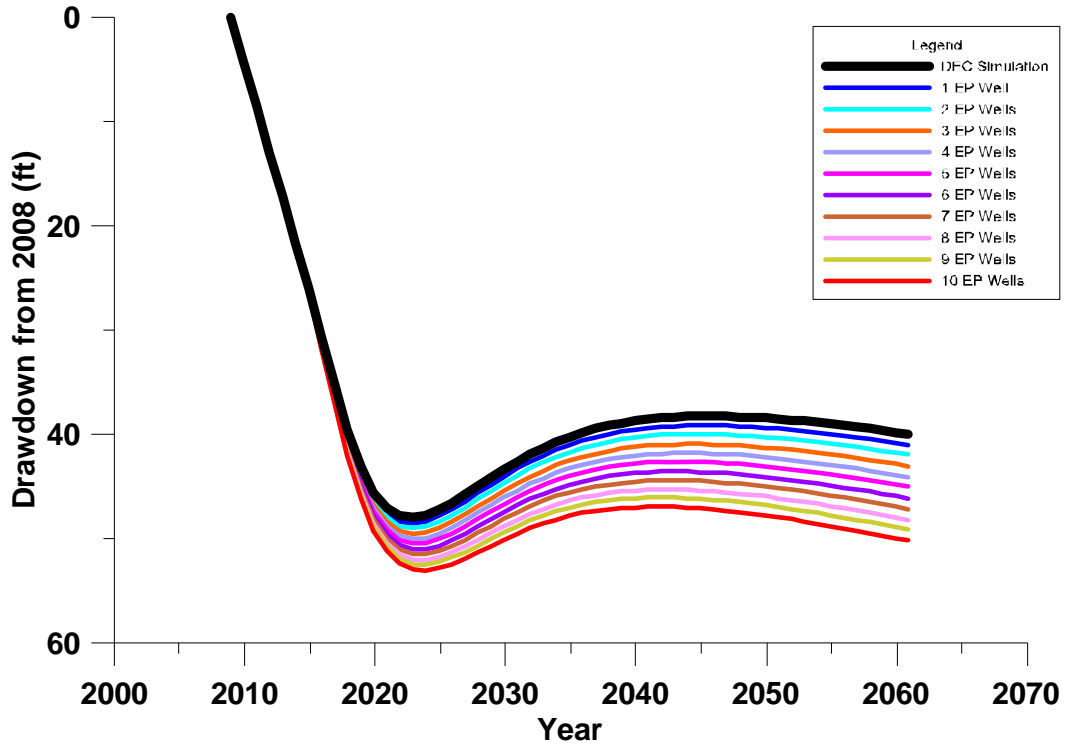
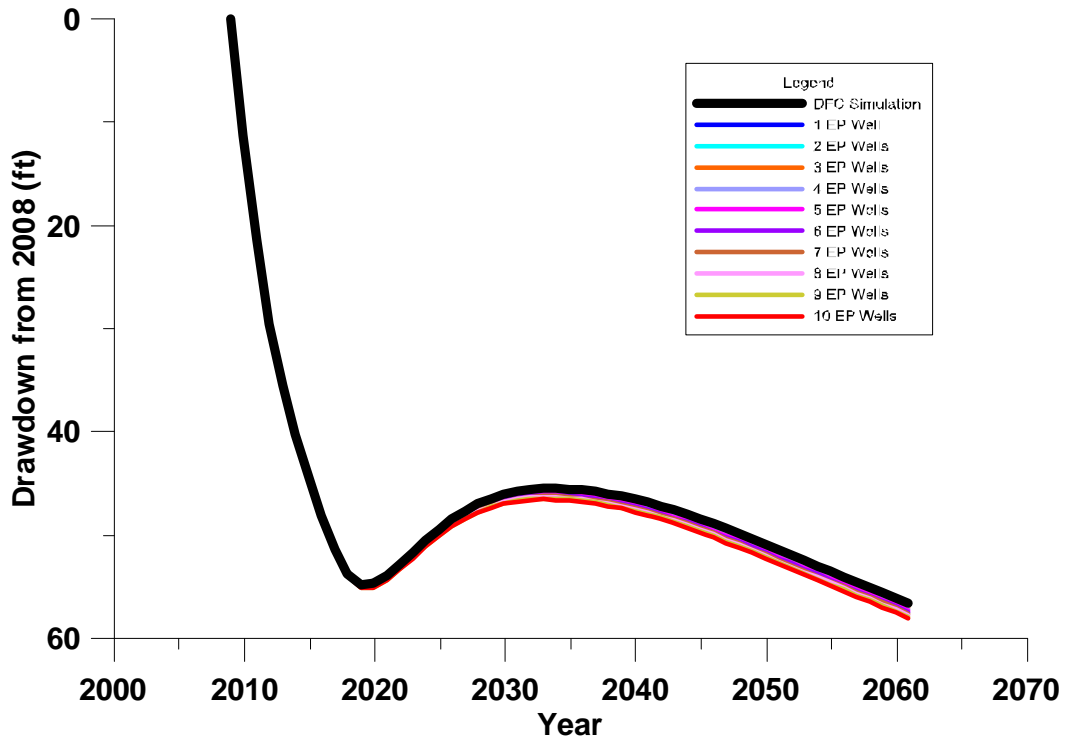
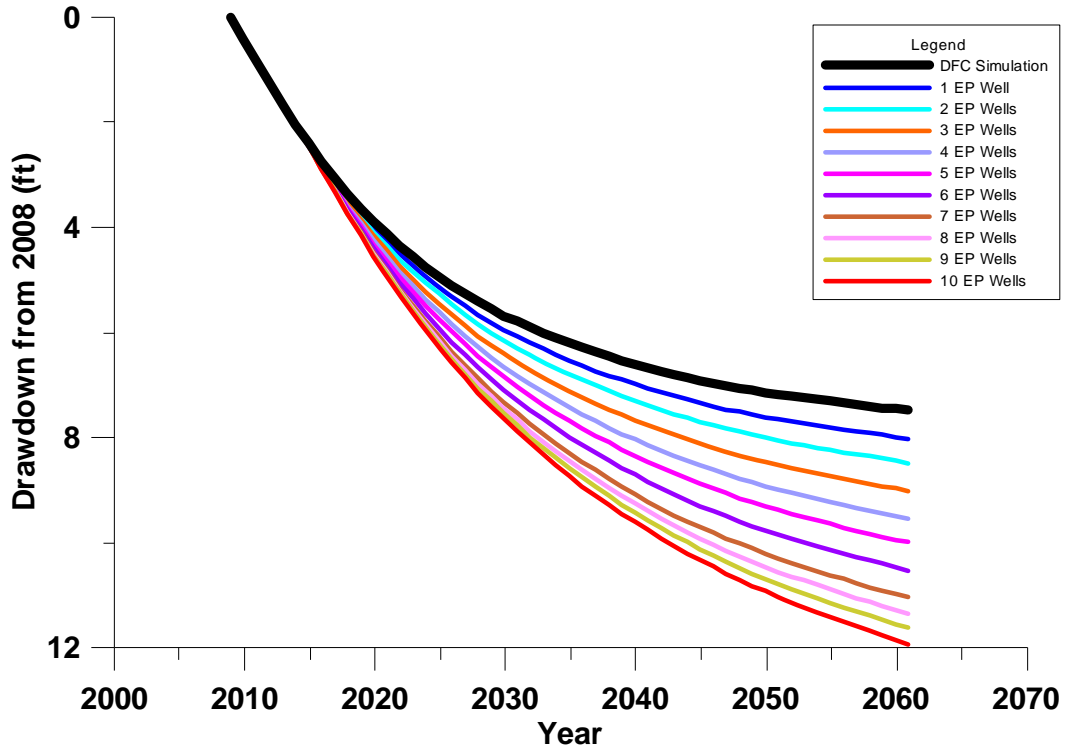


Figure D-12
Fort Bend County - Jasper
Electro Purification Pumping in Addition to MAG (HAGM)



**Figure D-13
Waller County - Chicot
Electro Purification Pumping in Addition to MAG (GAM)**



**Figure D-14
Waller County - Chicot
Electro Purification Pumping in Addition to MAG (HAGM)**

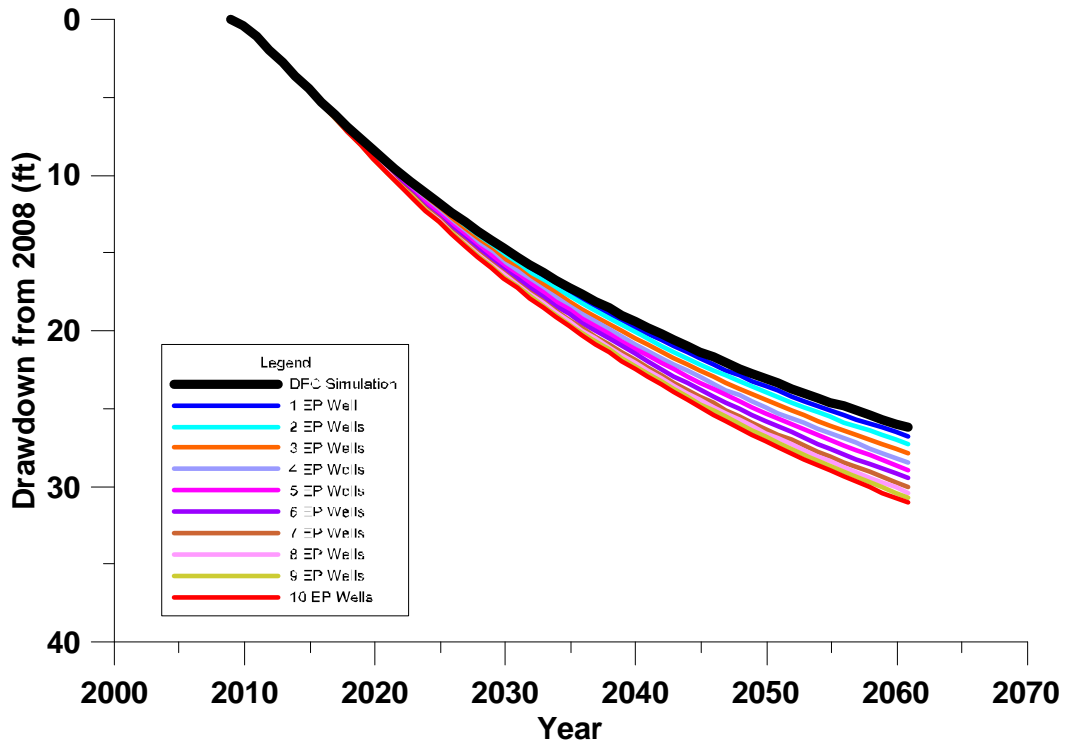


Figure D-15
Waller County - Evangeline
Electro Purification Pumping in Addition to MAG (GAM)

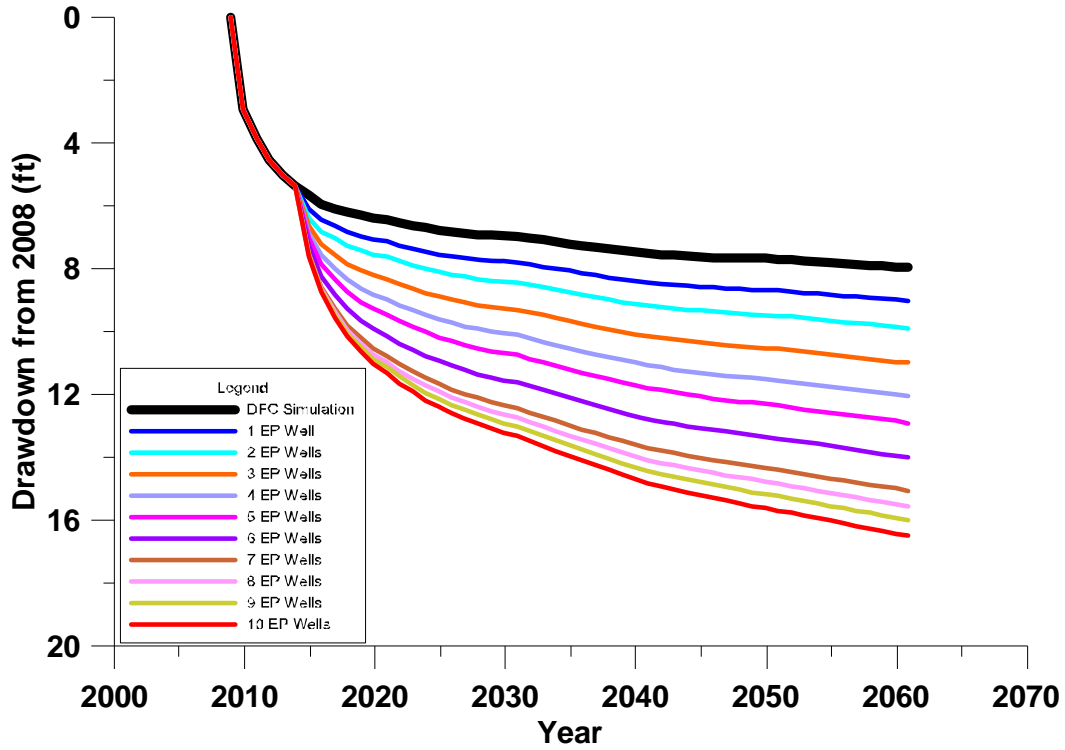


Figure D-16
Waller County - Evangeline
Electro Purification Pumping in Addition to MAG (HAGM)

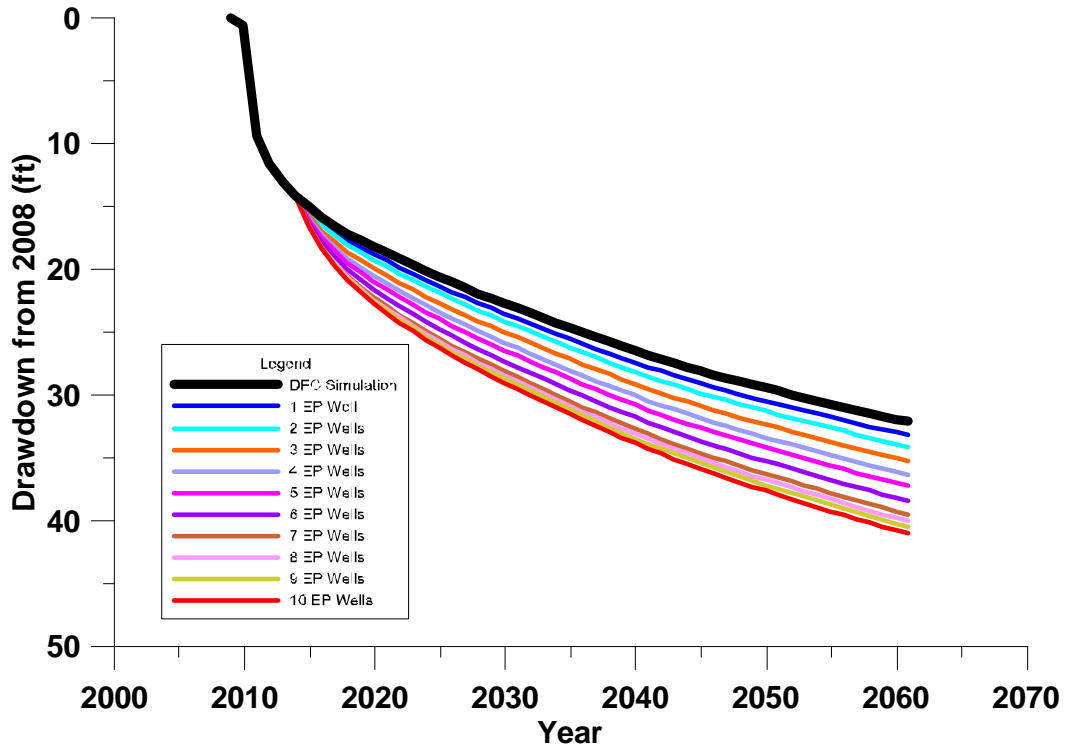


Figure D-17
Waller County - Jasper
Electro Purification Pumping in Addition to MAG (GAM)

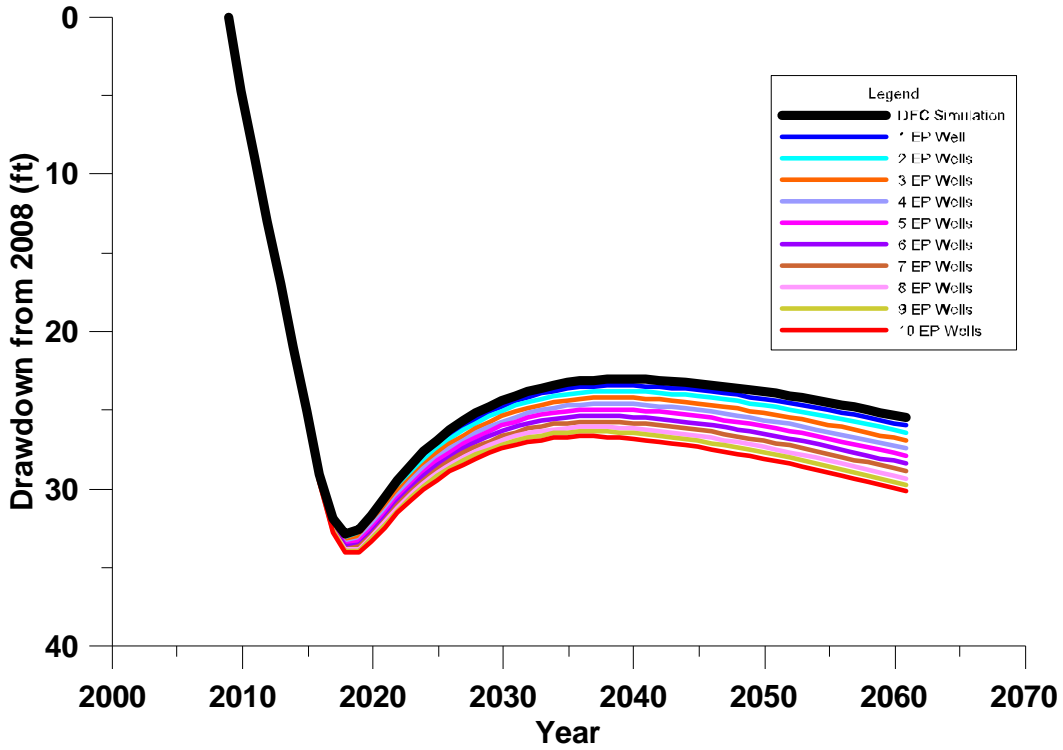


Figure D-18
Waller County - Jasper
Electro Purification Pumping in Addition to MAG (HAGM)

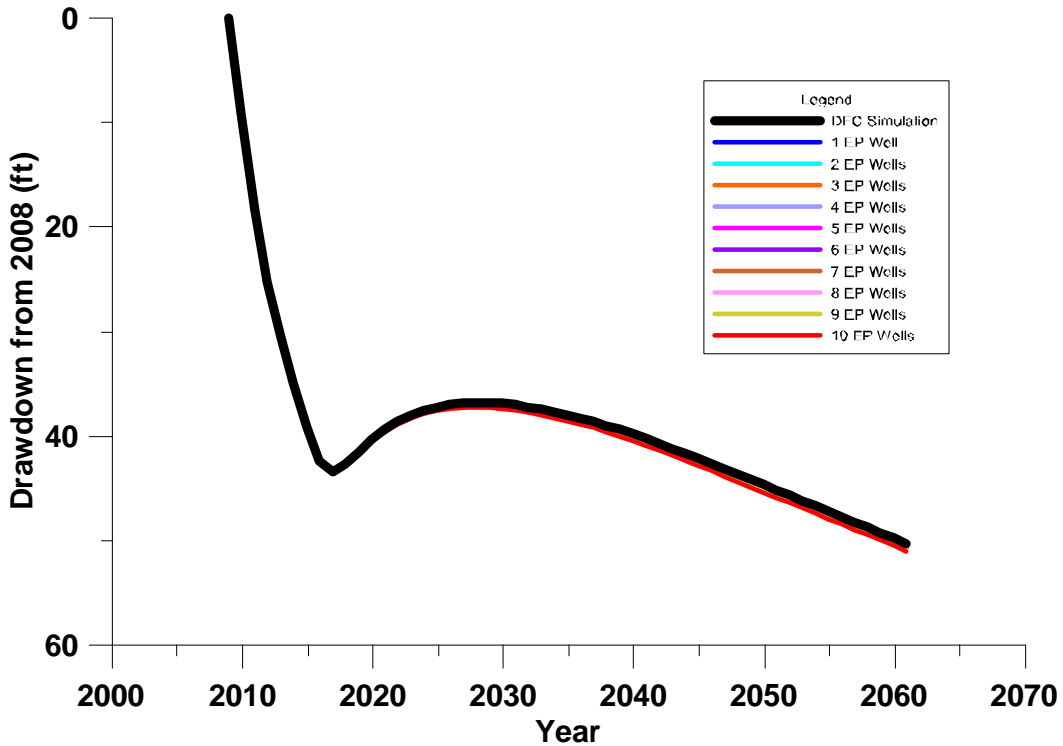


Figure D-19
Austin County - Chicot
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

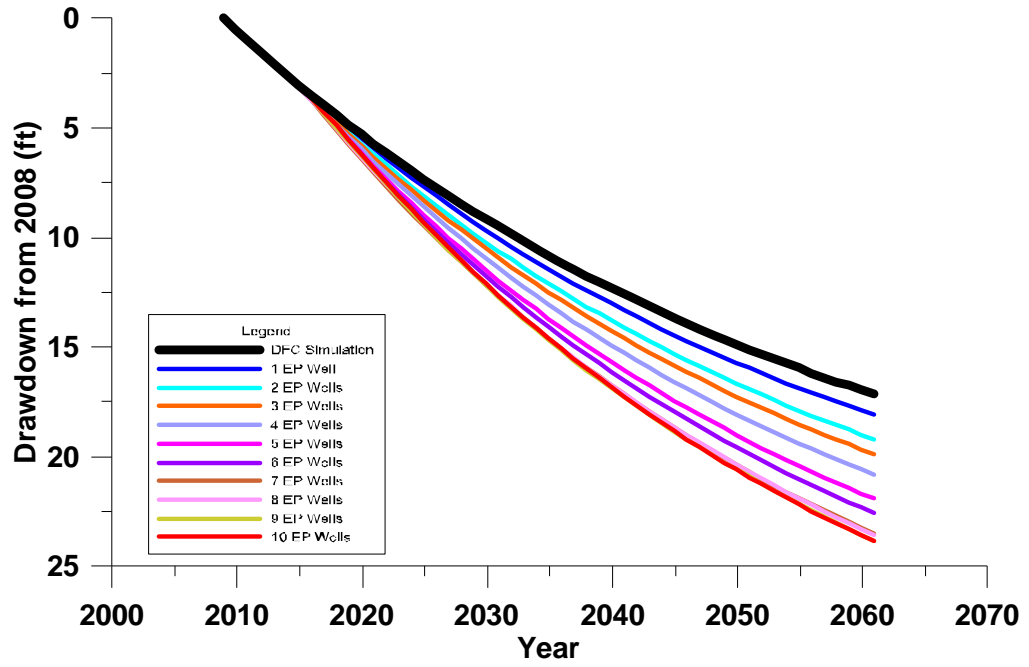


Figure D-20
Austin County - Chicot
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

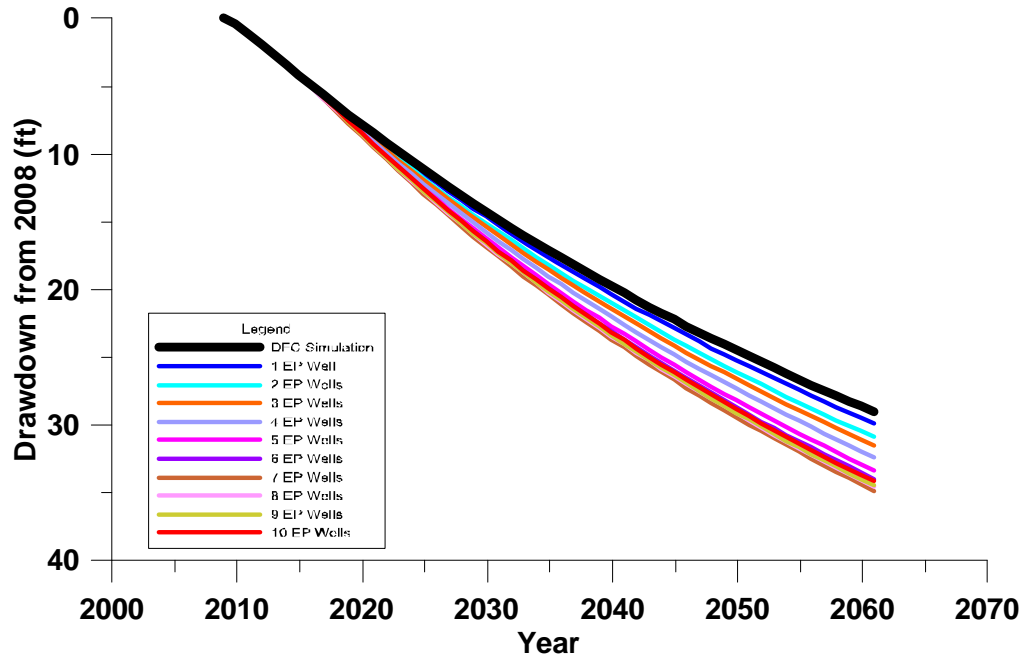


Figure D-21
Austin County - Evangeline
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

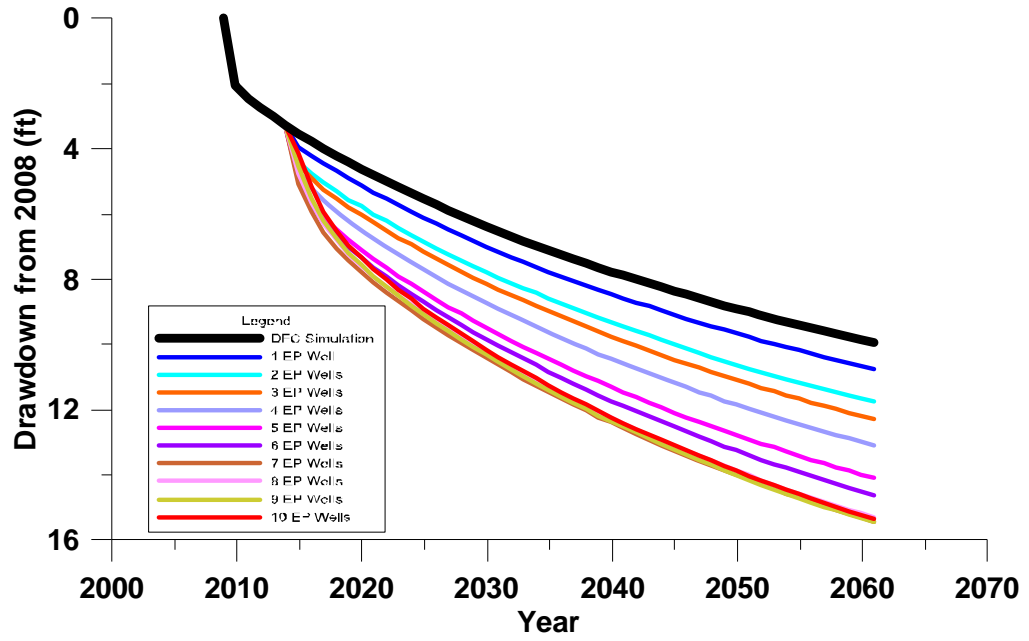


Figure D-22
Austin County - Evangeline
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

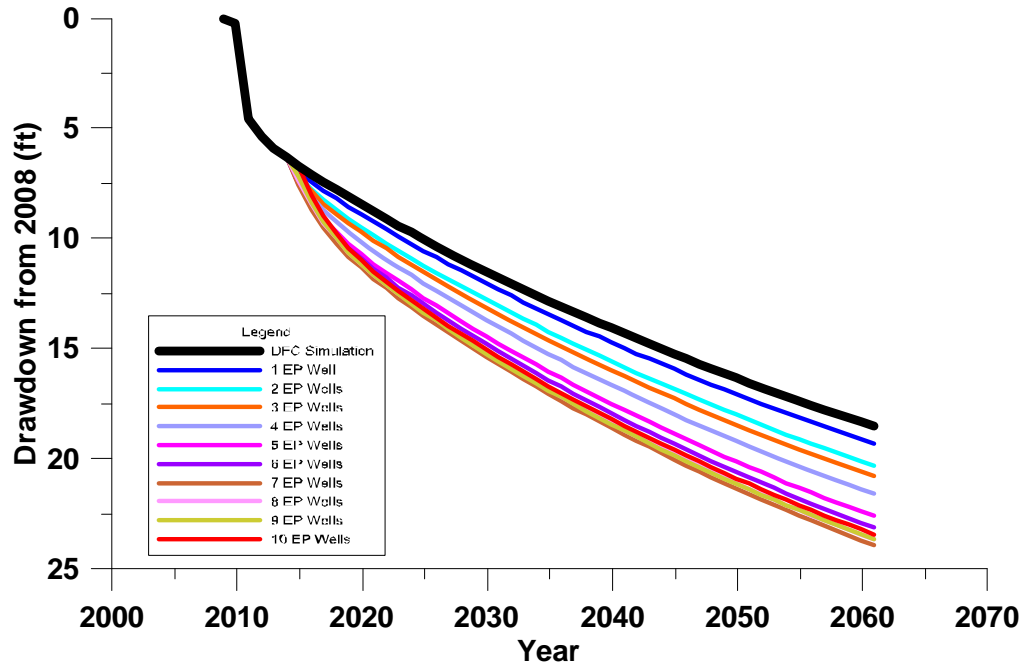


Figure D-23
Austin County - Jasper
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

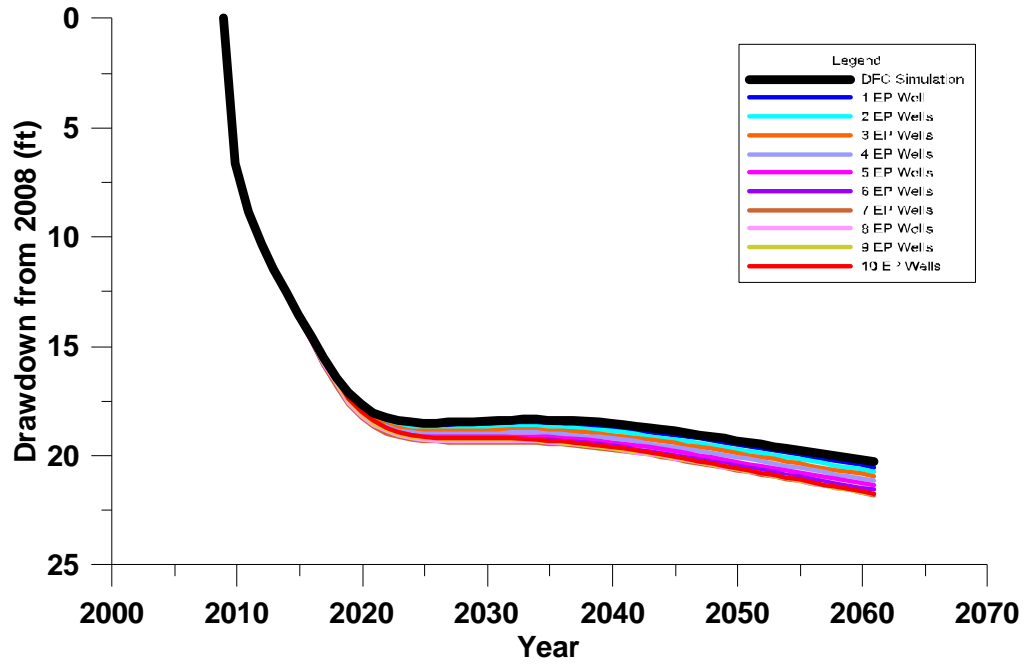


Figure D-24
Austin County - Jasper
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

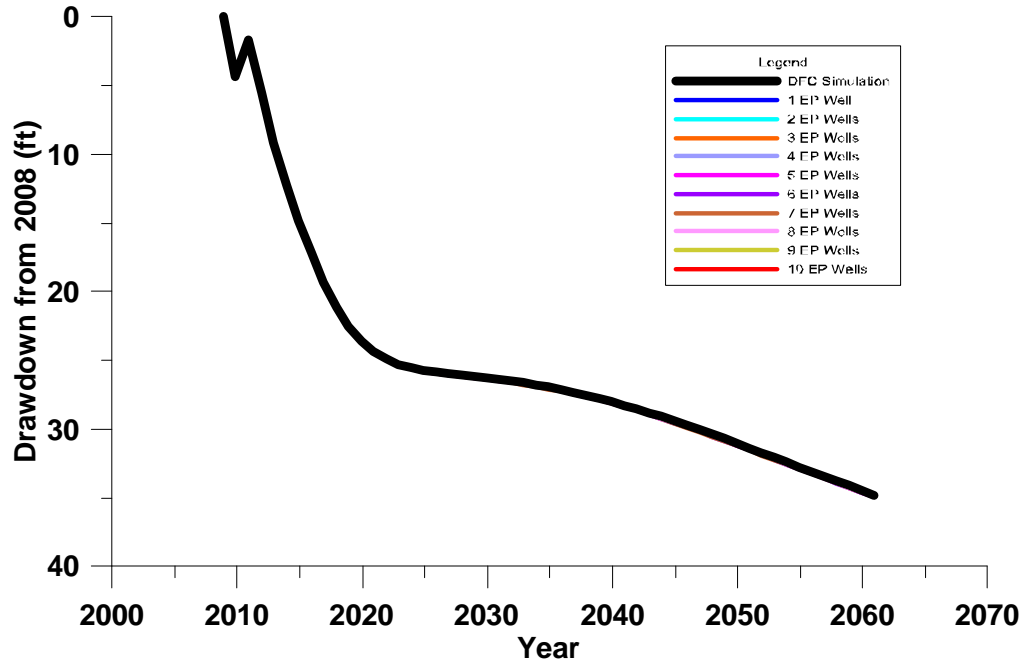


Figure D-25
Fort Bend County - Chicot
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

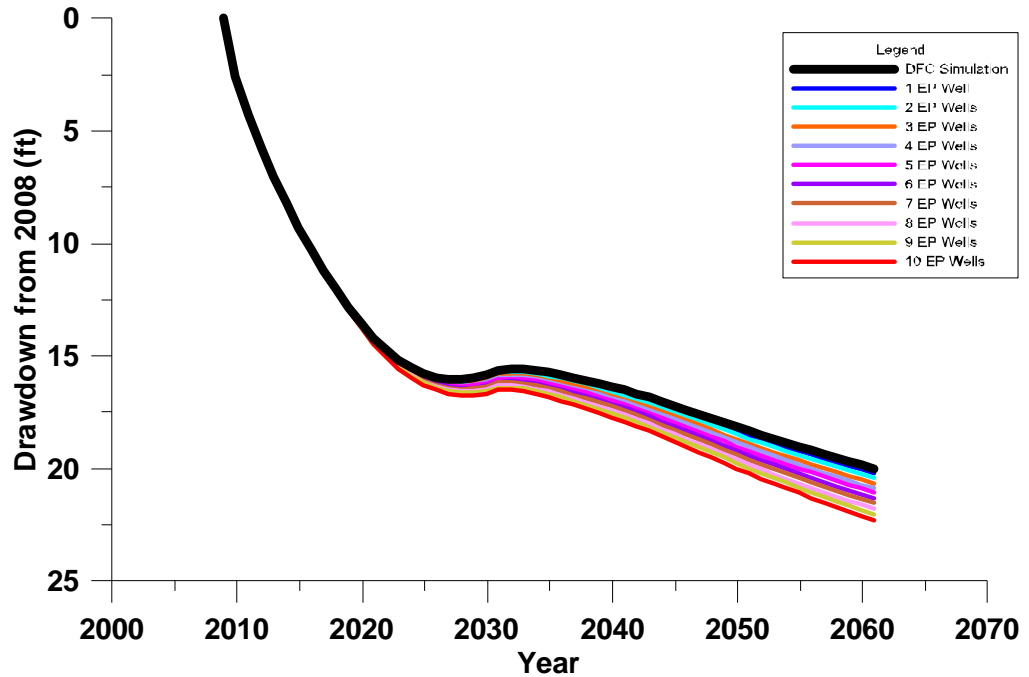


Figure D-26
Fort Bend County - Chicot
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

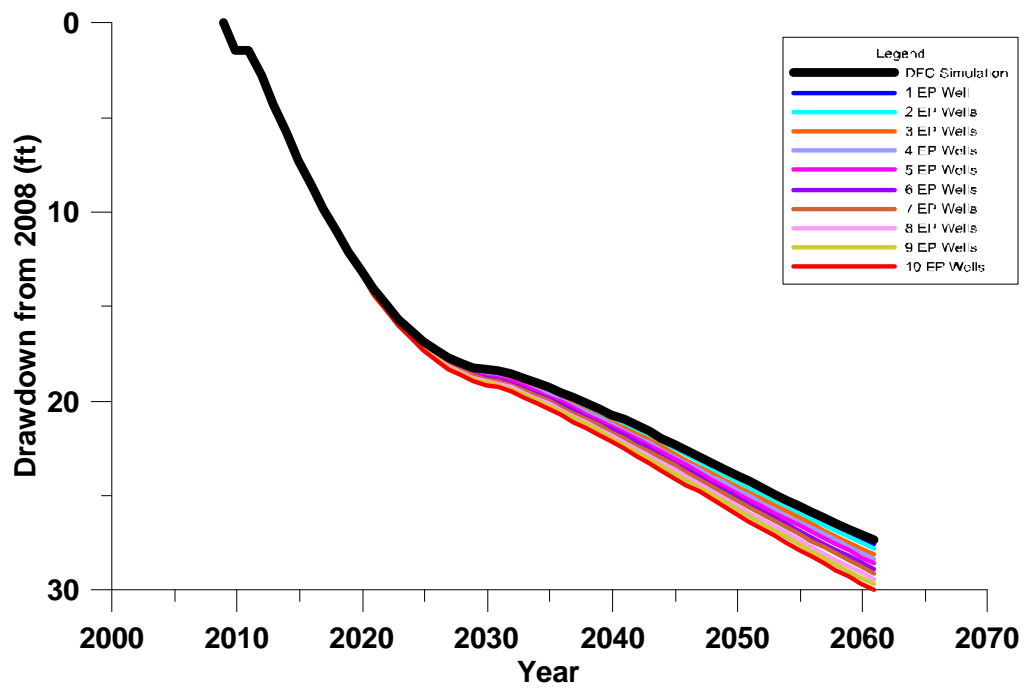


Figure D-27
Fort Bend County - Evangeline
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

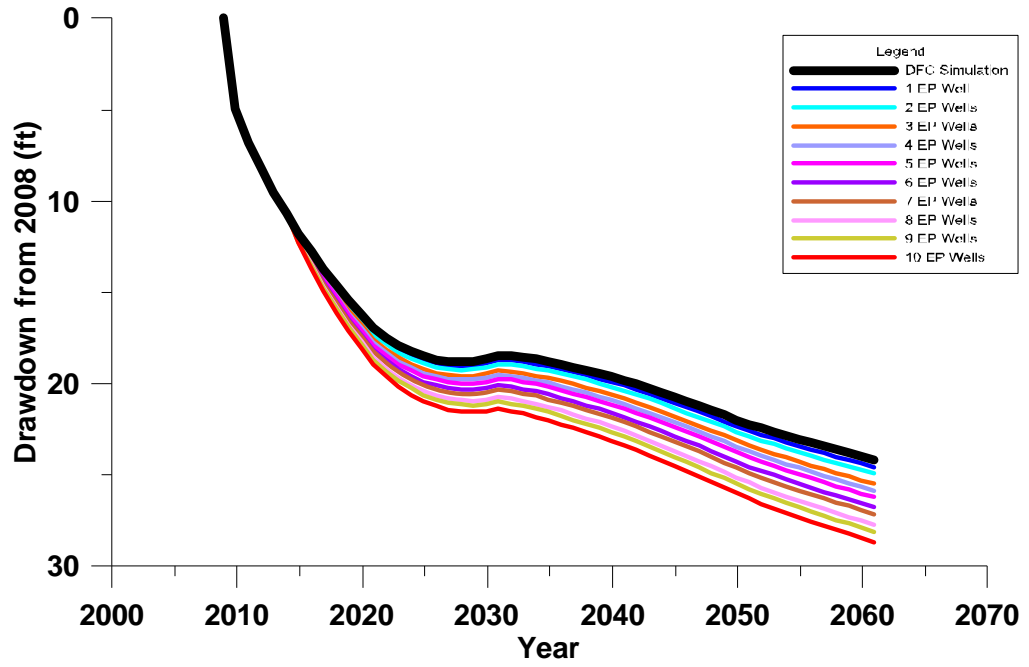


Figure D-28
Fort Bend County - Evangeline
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

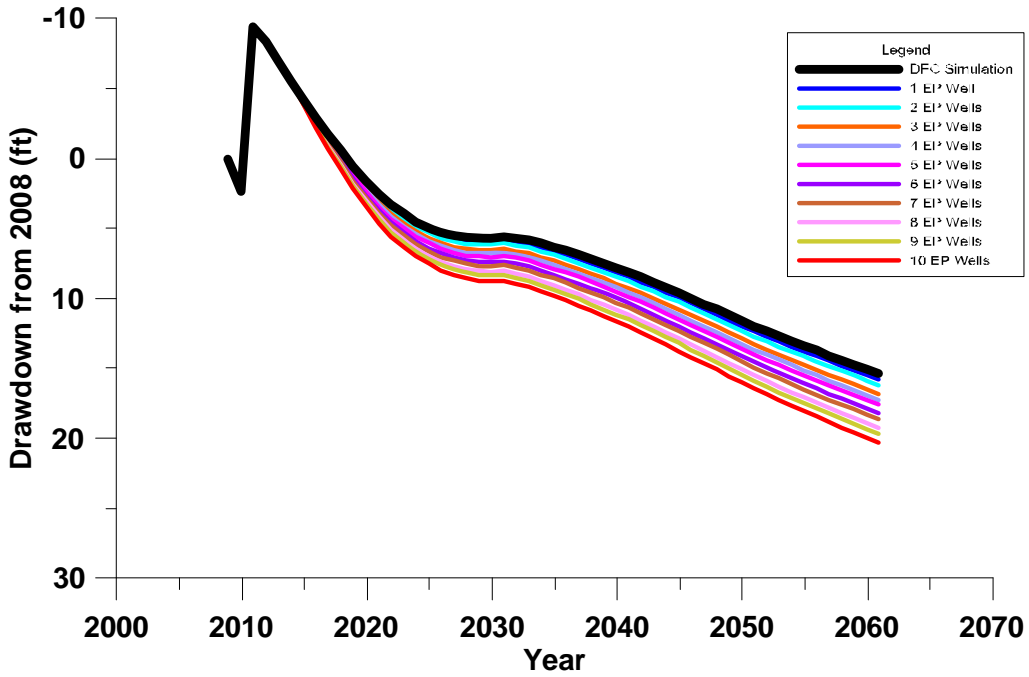


Figure D-29
Fort Bend County - Jasper
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

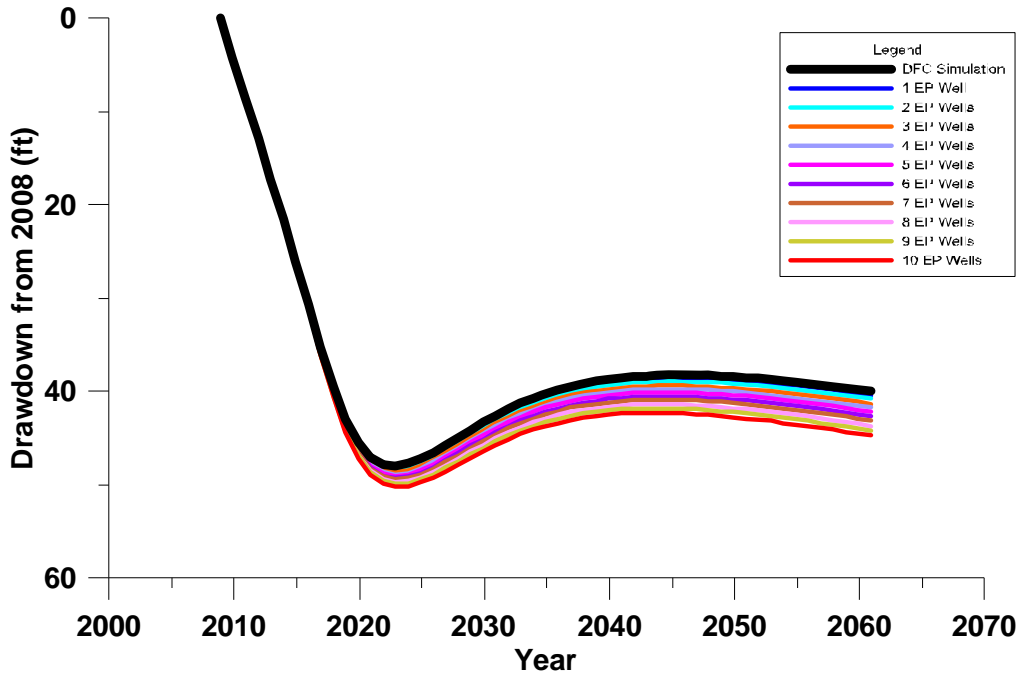


Figure D-30
Fort Bend County - Jasper
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

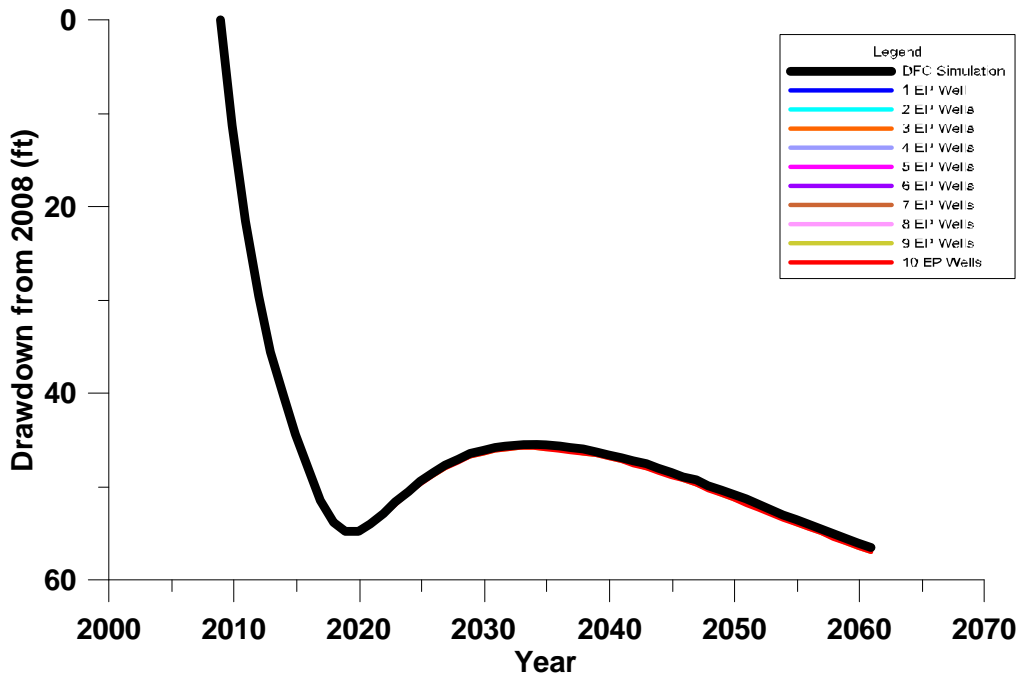


Figure D-31
Waller County - Chicot
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

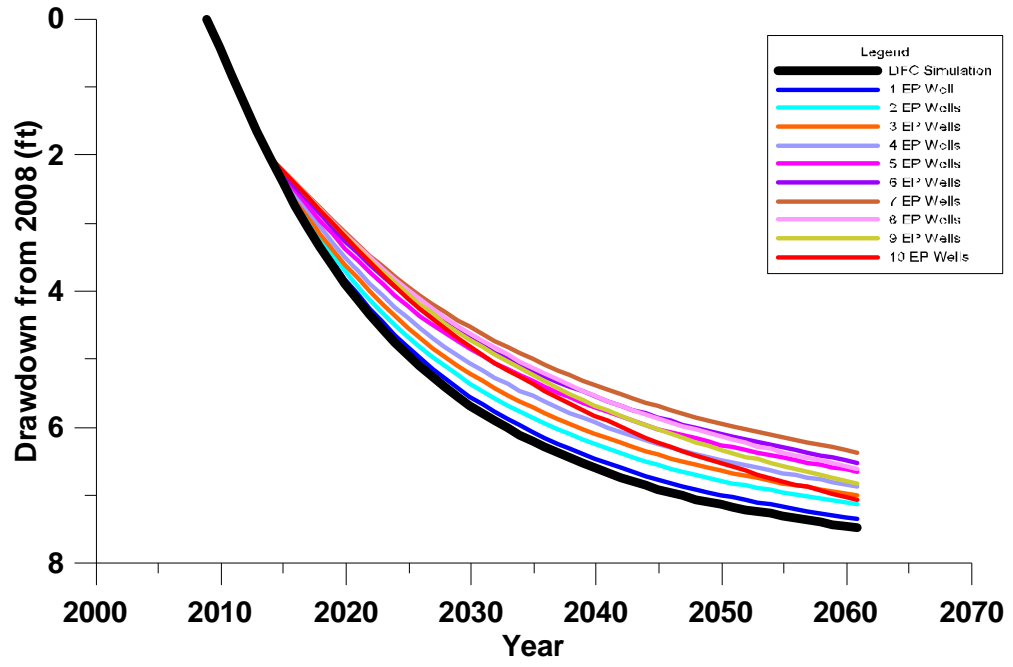


Figure D-32
Waller County - Chicot
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

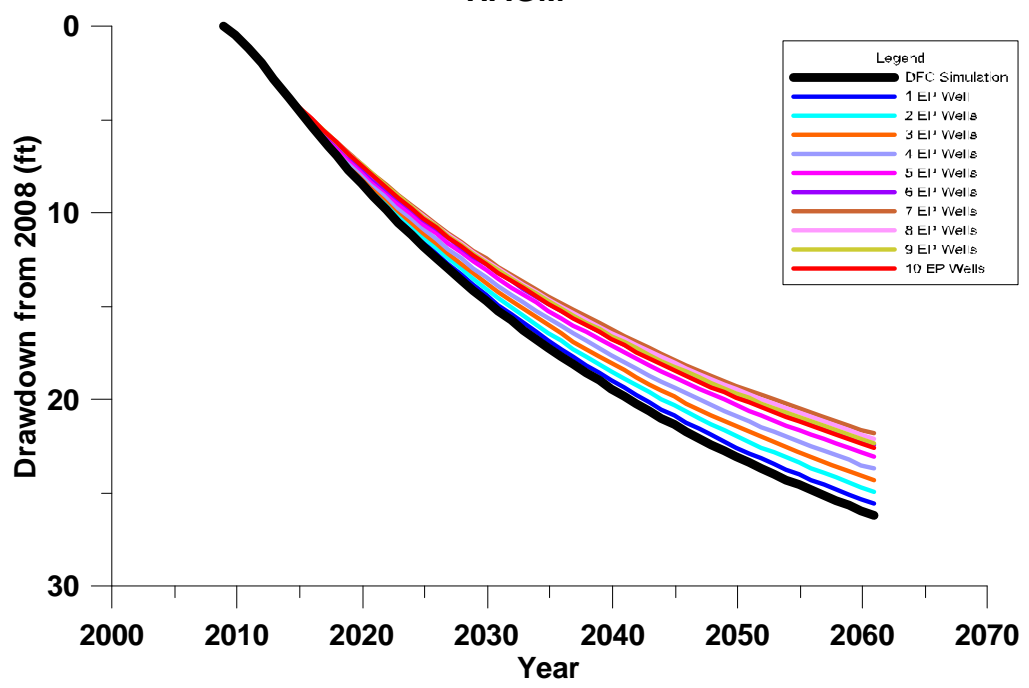


Figure D-33
Waller County - Evangeline
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

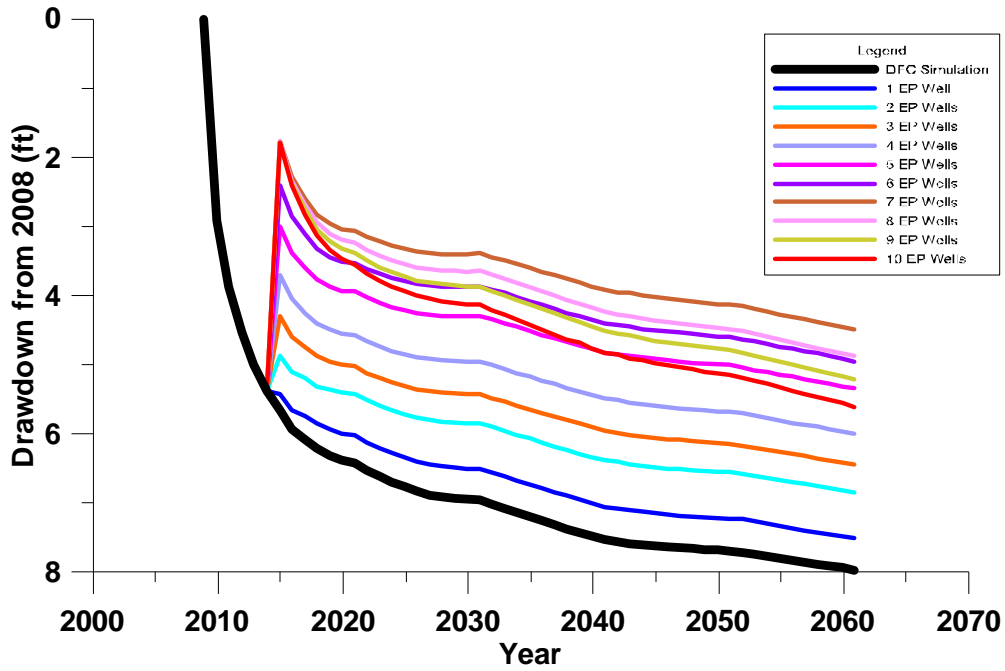


Figure D-34
Waller County - Evangeline
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

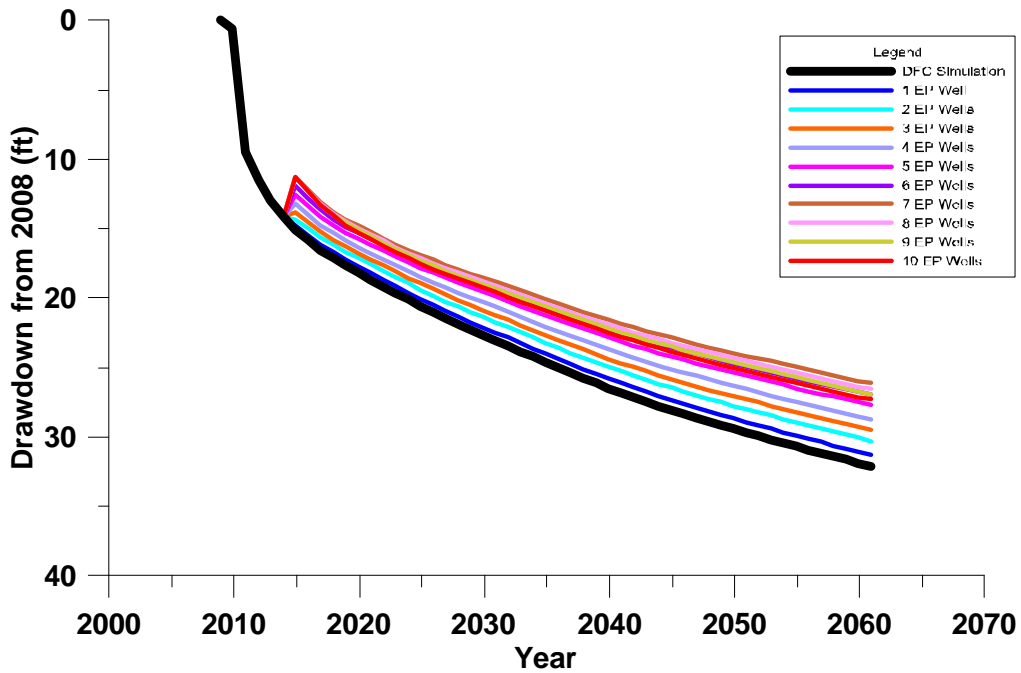


Figure D-35
Waller County - Jasper
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

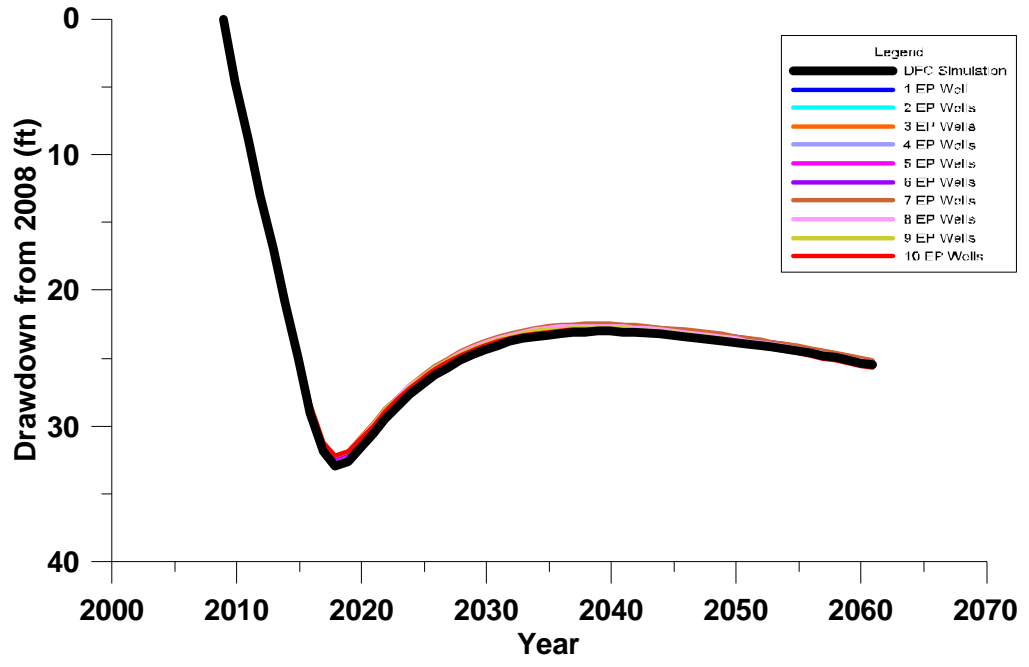


Figure D-36
Waller County - Jasper
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

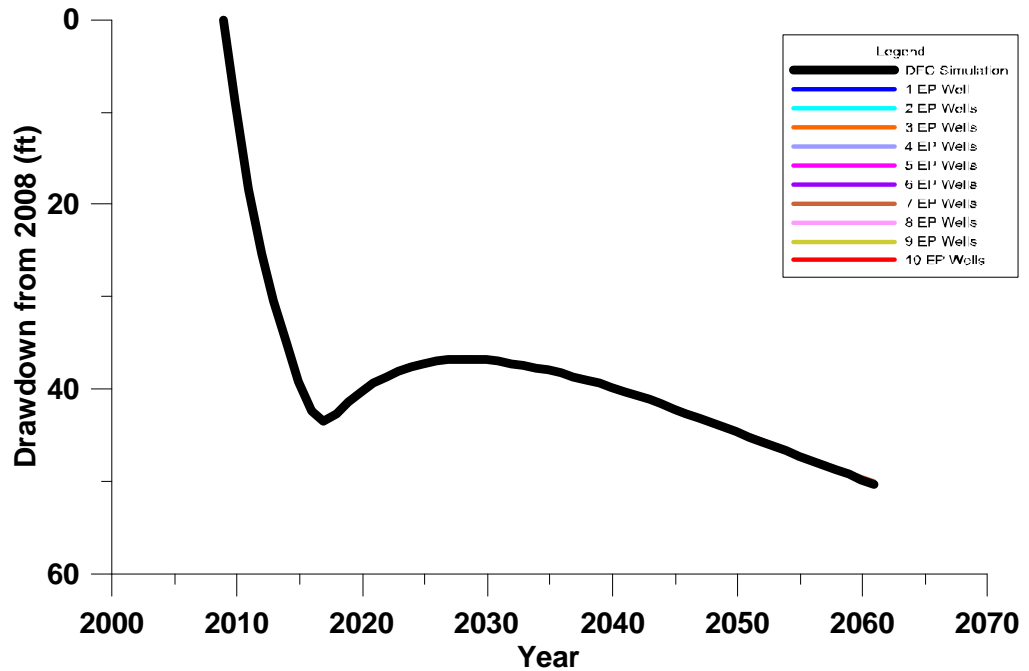


Figure D-37
Austin County - Chicot
Electro Purification Pumping - Evangeline/Jasper
GAM

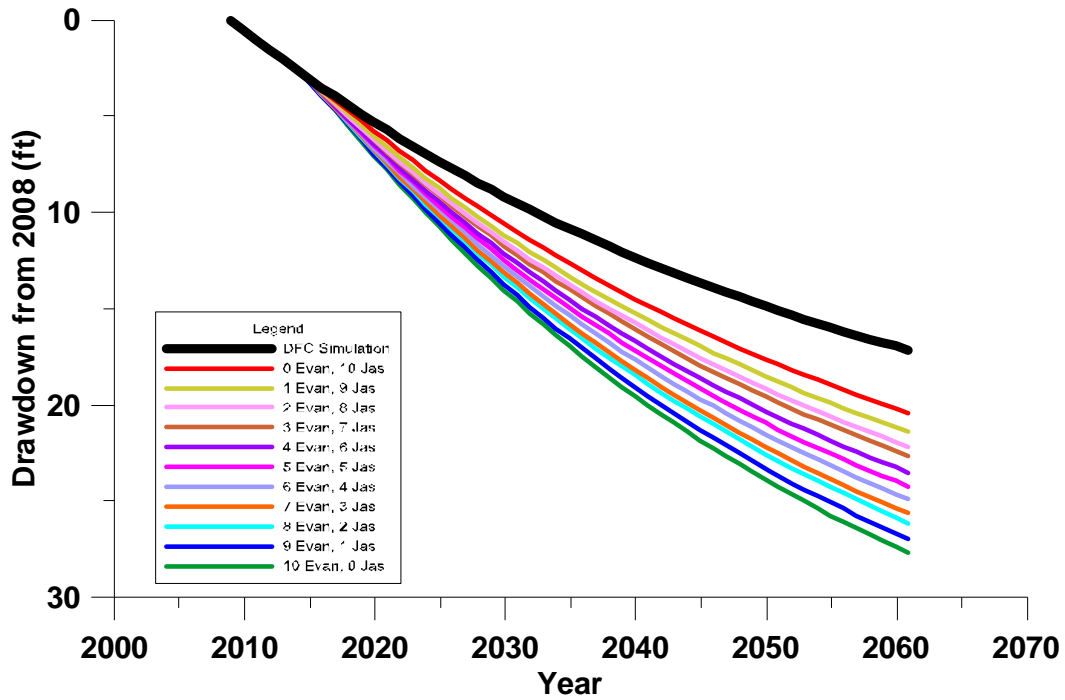


Figure D-38
Austin County - Chicot
Electro Purification Pumping - Evangeline/Jasper
HAGM

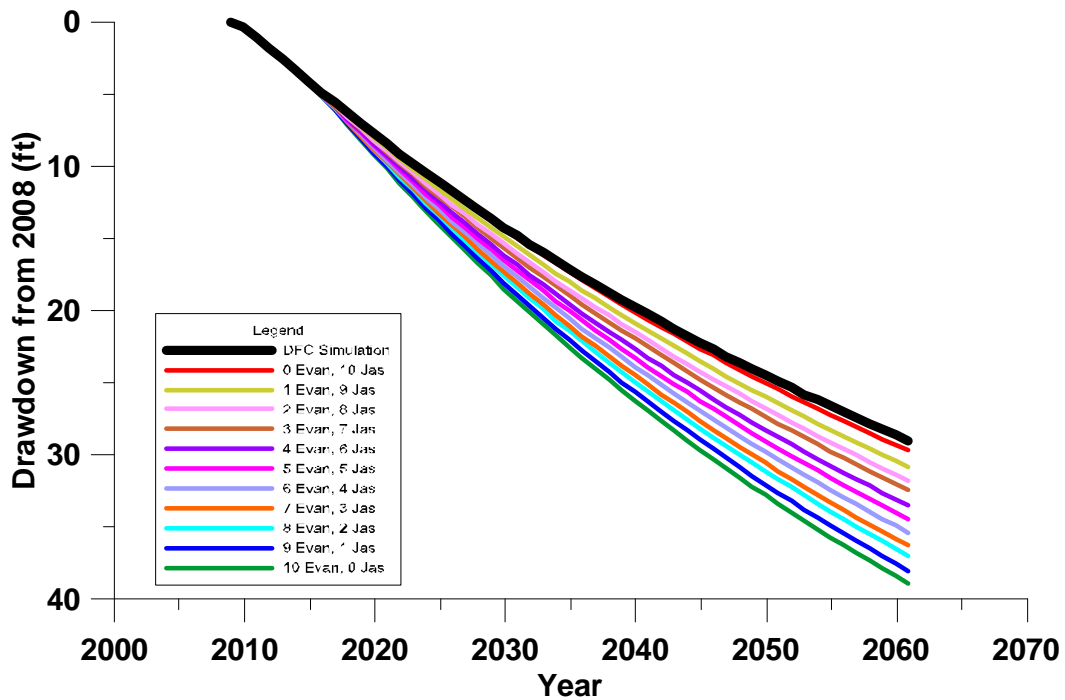


Figure D-39
Austin County - Evangeline
Electro Purification Pumping - Evangeline/Jasper
GAM

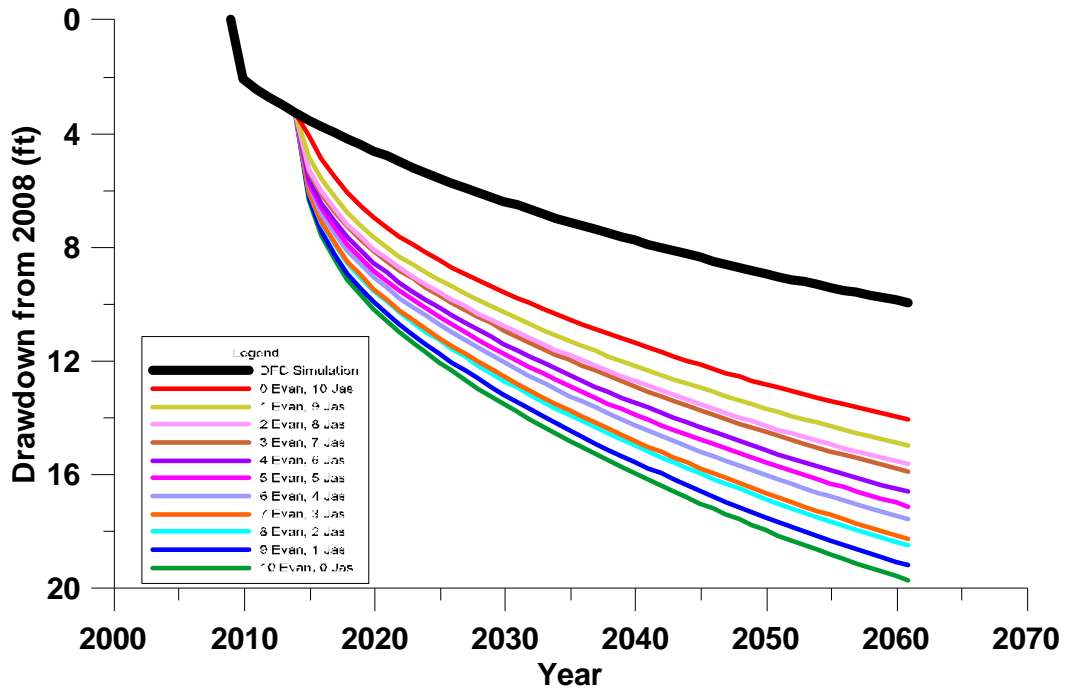


Figure D-40
Austin County - Evangeline
Electro Purification Pumping - Evangeline/Jasper
HAGM

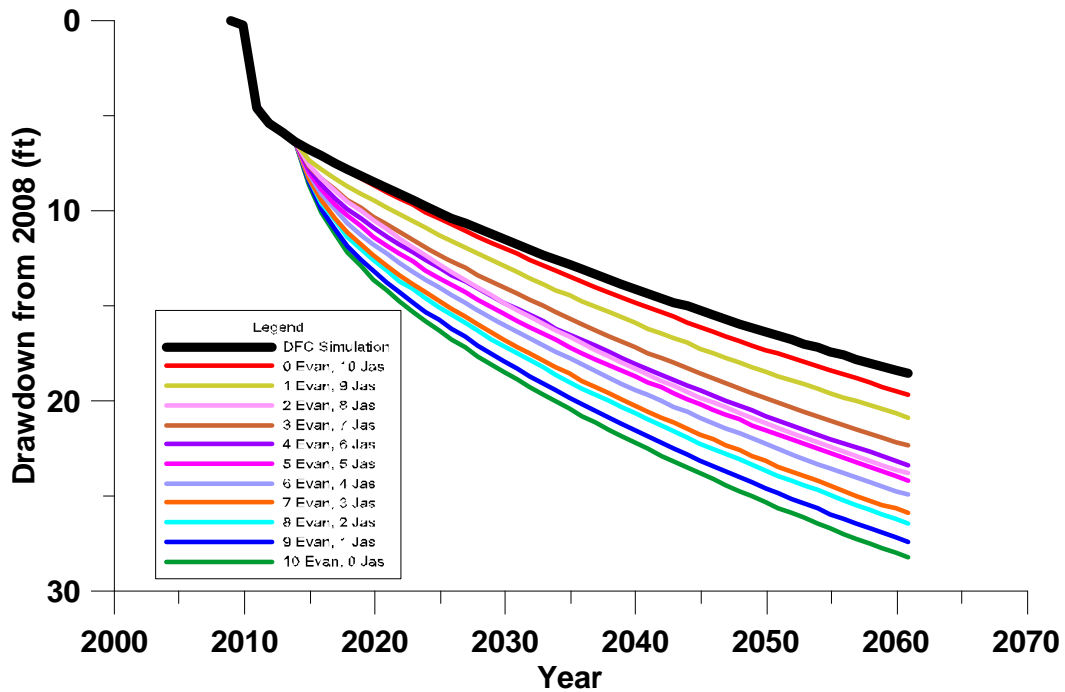


Figure D-41
Austin County - Jasper
Electro Purification Pumping - Evangeline/Jasper
GAM

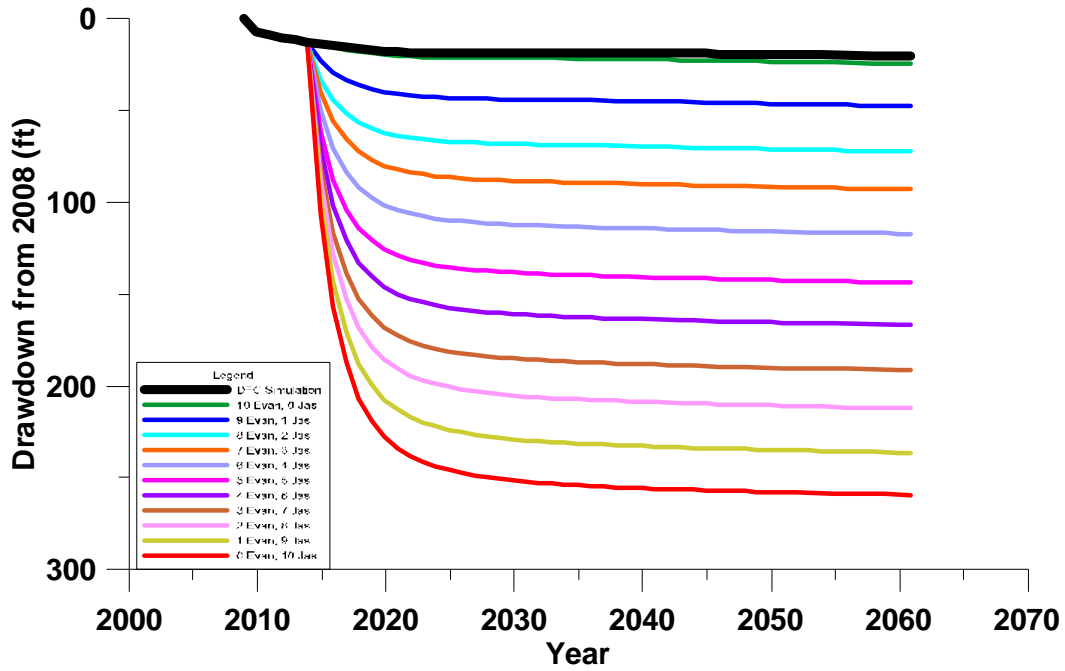


Figure D-42
Austin County - Jasper
Electro Purification Pumping - Evangeline/Jasper
HAGM

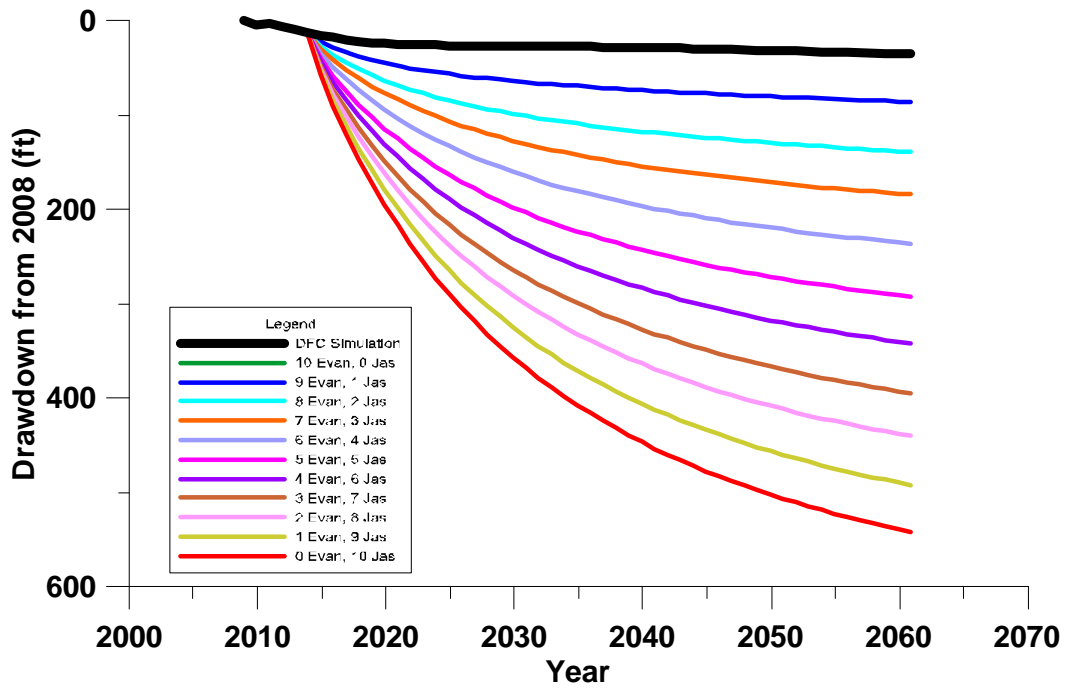


Figure D-43
Fort Bend County - Chicot
Electro Purification Pumping - Evangeline/Jasper
GAM

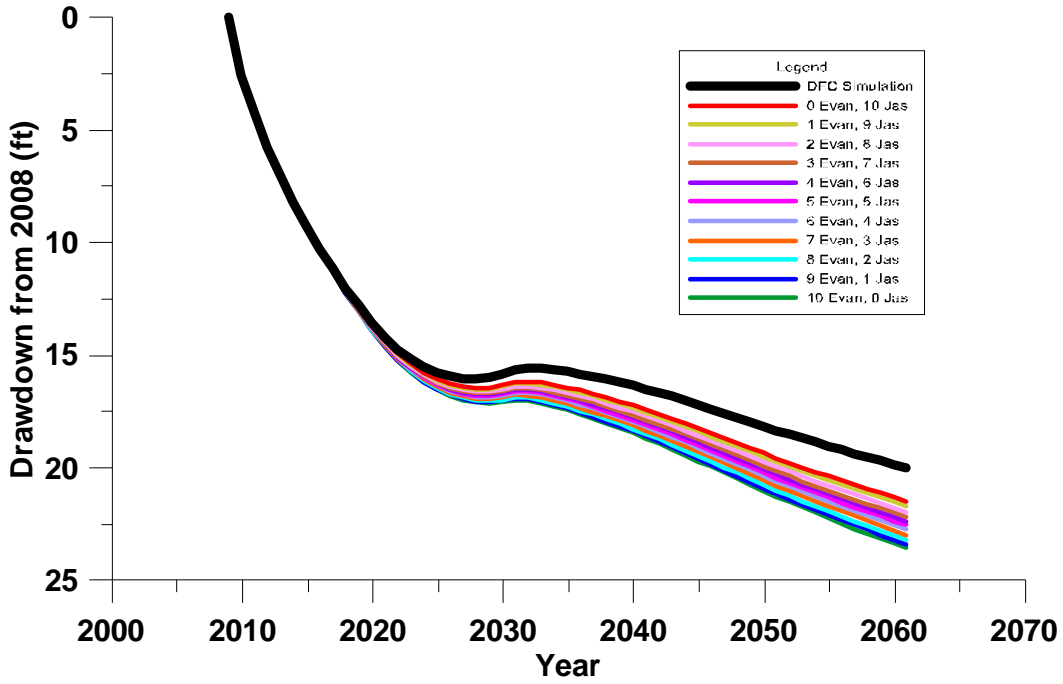


Figure D-44
Fort Bend County - Chicot
Electro Purification Pumping - Evangeline/Jasper
HAGM

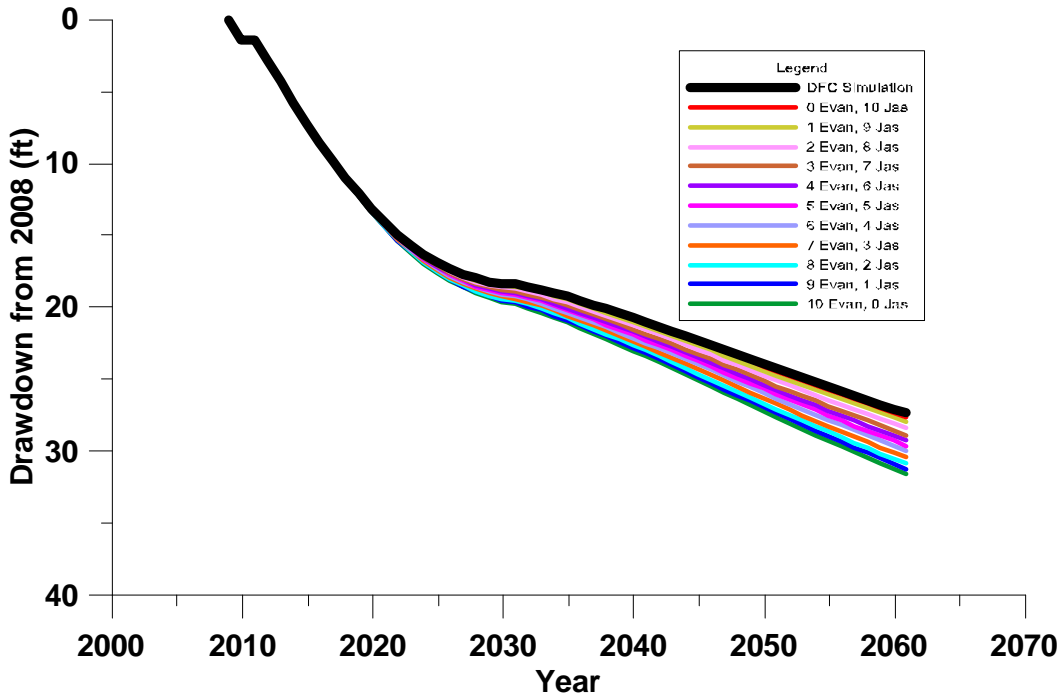


Figure D-45
Fort Bend County - Evangeline
Electro Purification Pumping - Evangeline/Jasper
GAM

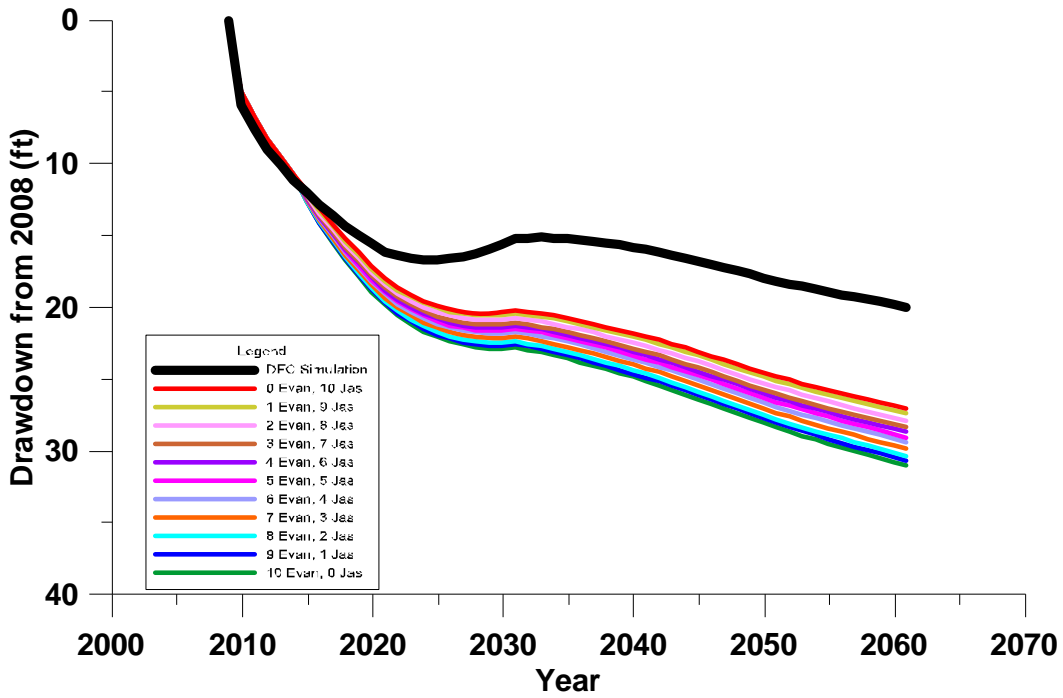


Figure D-46
Fort Bend County - Evangeline
Electro Purification Pumping - Evangeline/Jasper
HAGM

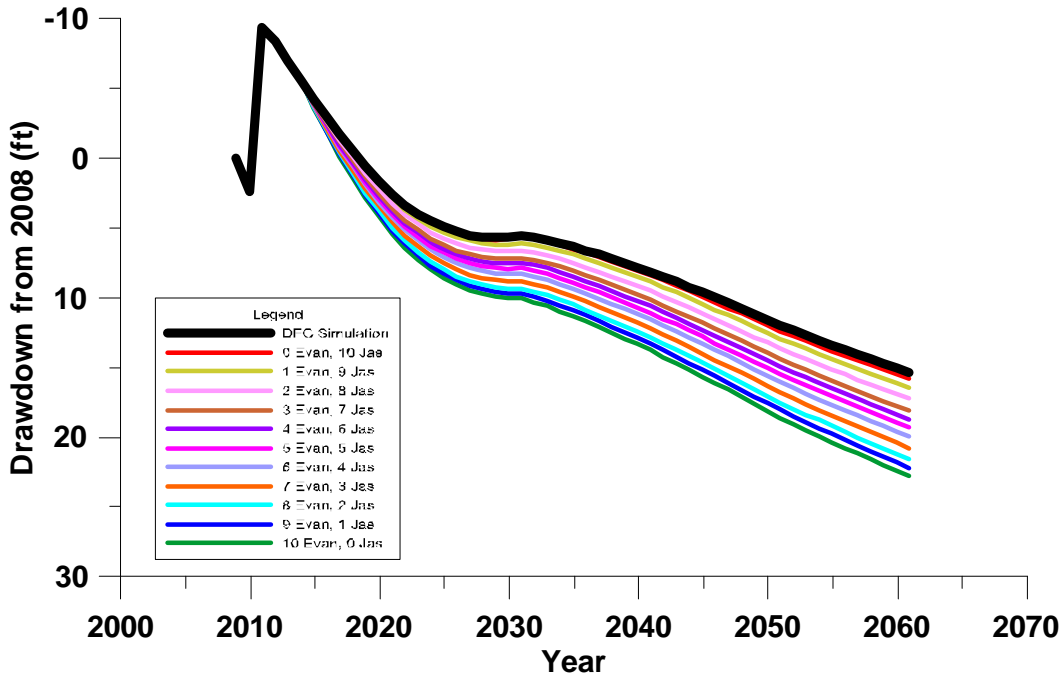


Figure D-47
Fort Bend County - Jasper
Electro Purification Pumping - Evangeline/Jasper
GAM

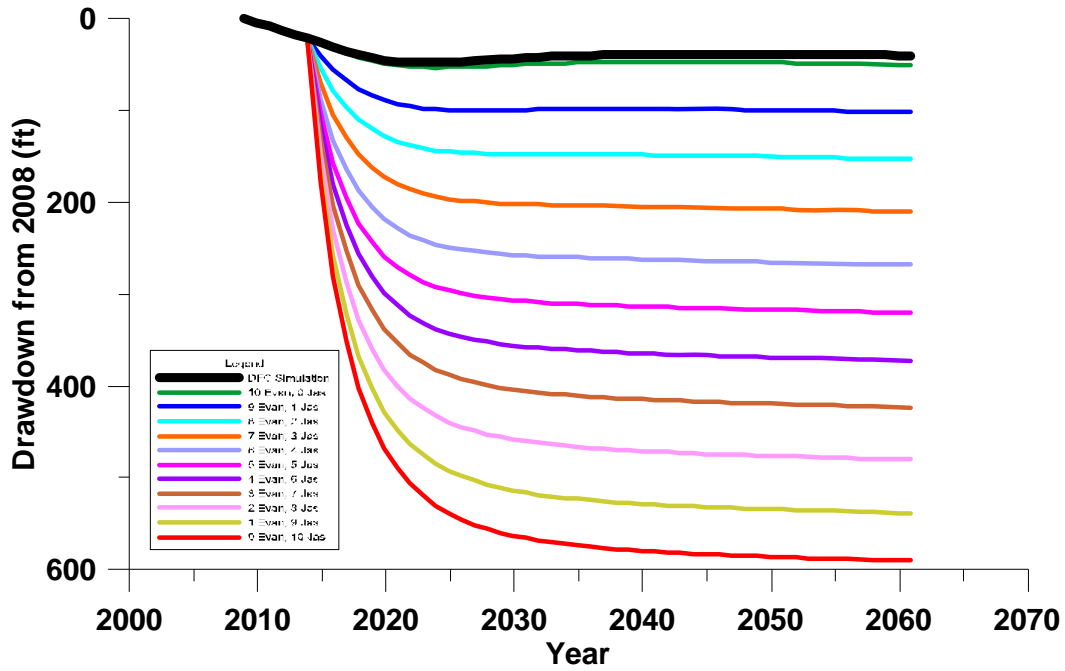


Figure D-48
Fort Bend County - Jasper
Electro Purification Pumping - Evangeline/Jasper
HAGM

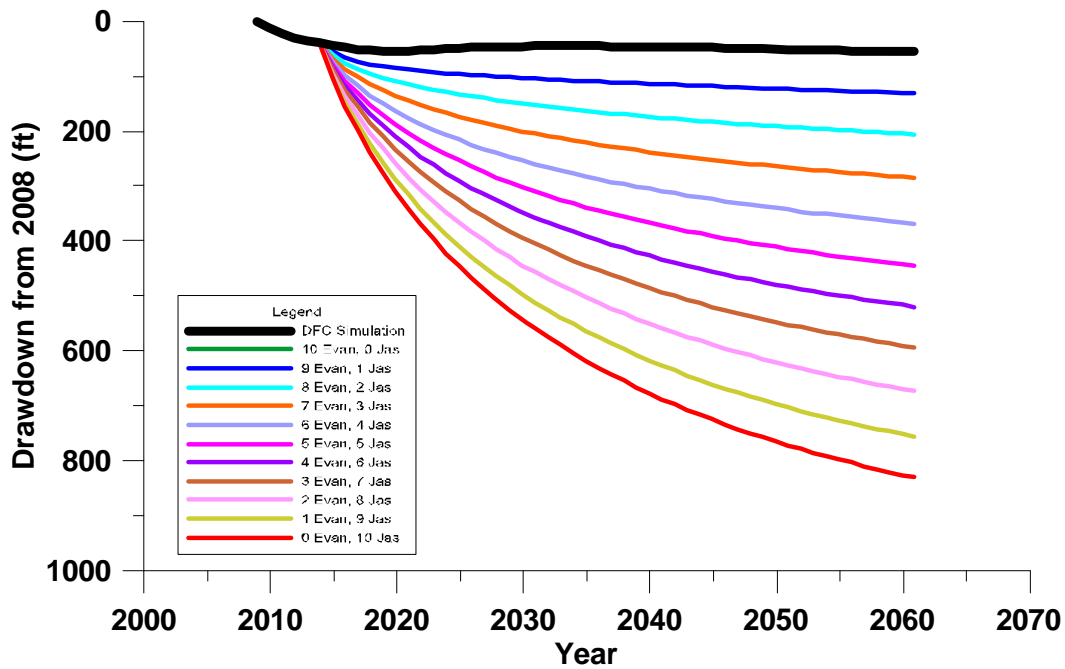


Figure D-49
Waller County - Chicot
Electro Purification Pumping - Evangeline/Jasper
GAM

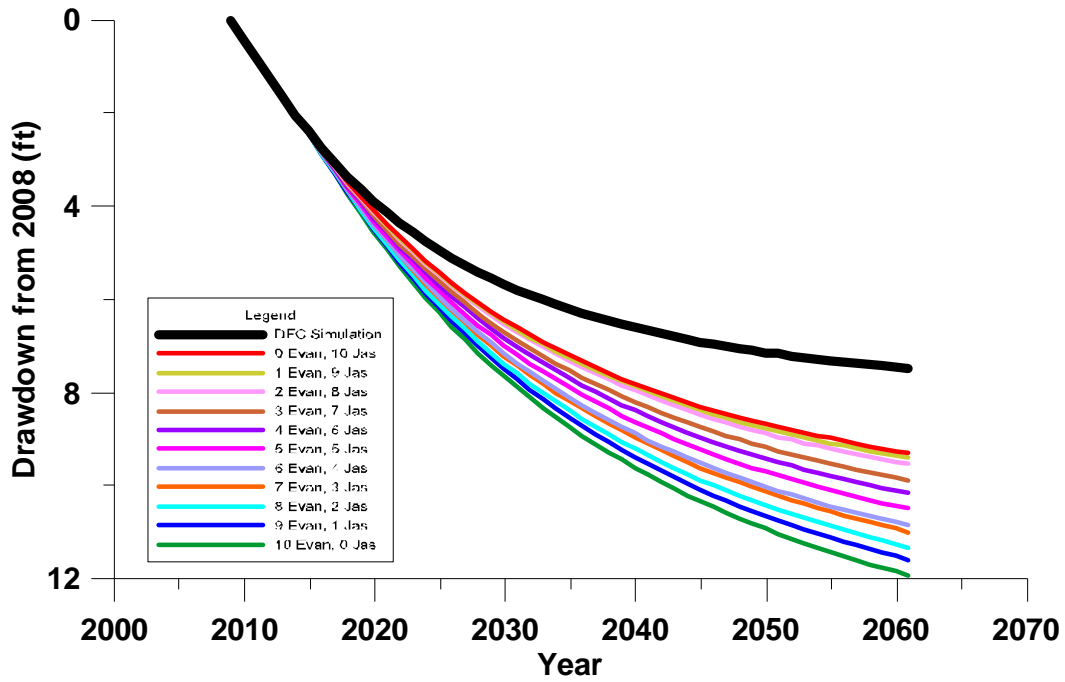


Figure D-50
Waller County - Chicot
Electro Purification Pumping - Evangeline/Jasper
HAGM

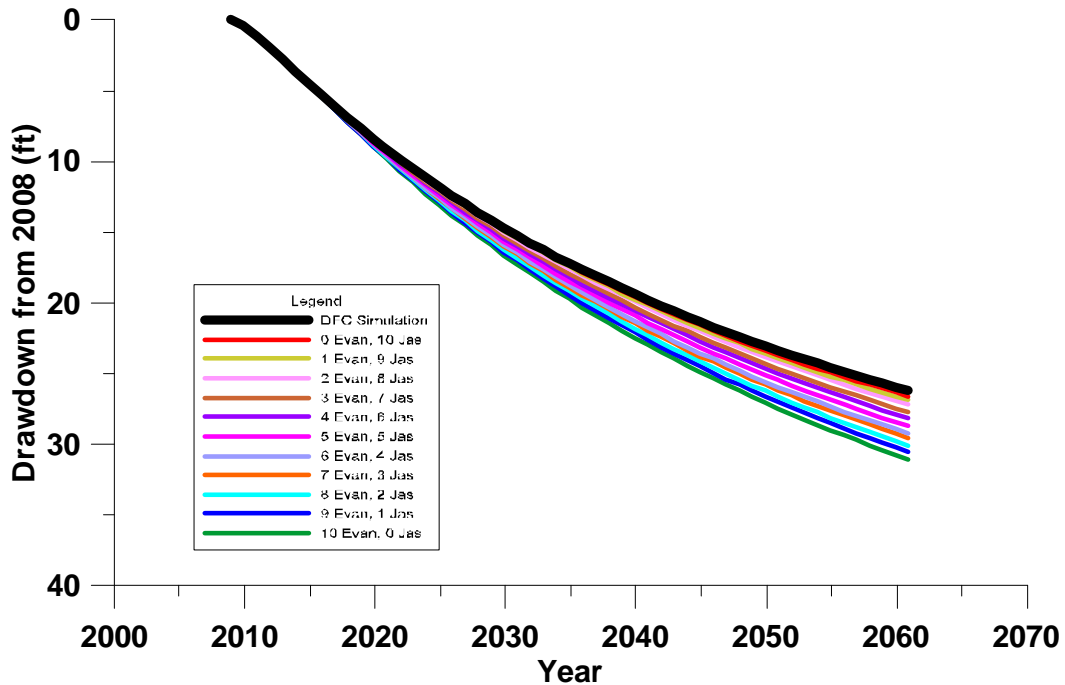


Figure D-51
Waller County - Evangeline
Electro Purification Pumping - Evangeline/Jasper
GAM

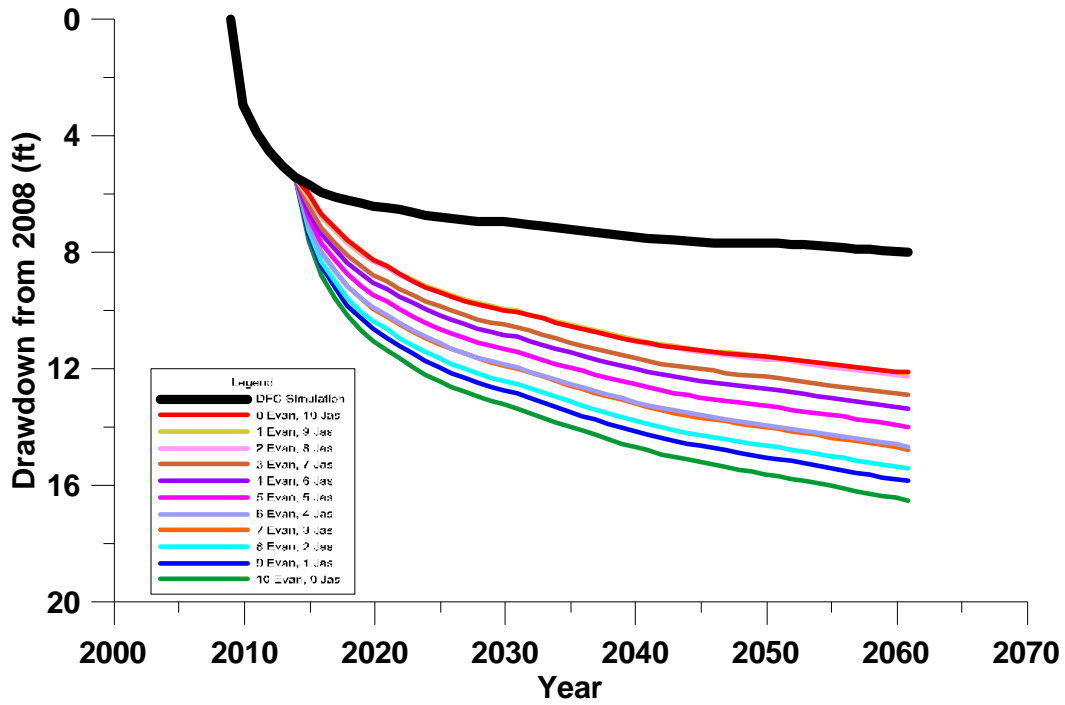


Figure D-52
Waller County - Evangeline
Electro Purification Pumping - Evangeline/Jasper
HAGM

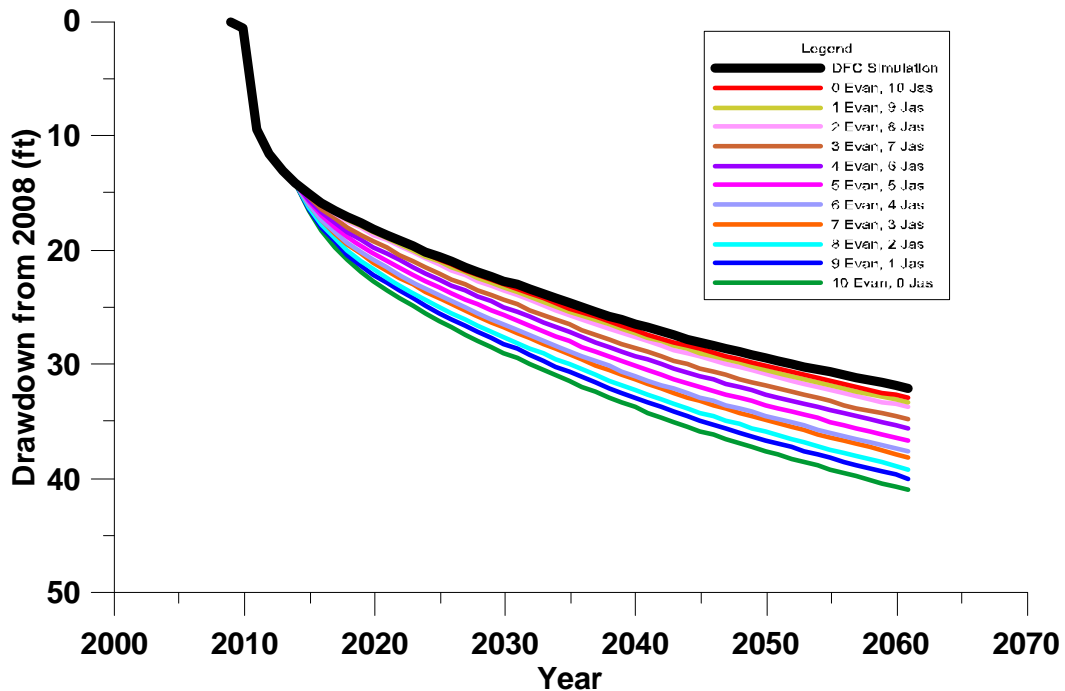


Figure D-53
Waller County - Jasper
Electro Purification Pumping - Evangeline/Jasper
GAM

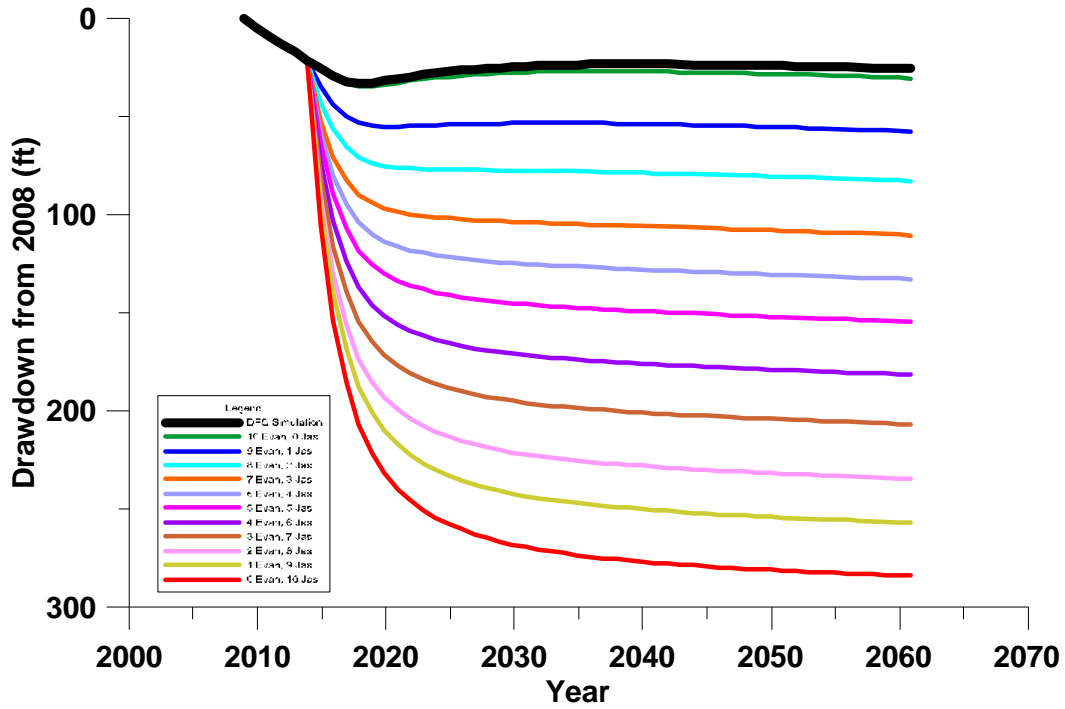


Figure D-54
Waller County - Jasper
Electro Purification Pumping - Evangeline/Jasper
HAGM

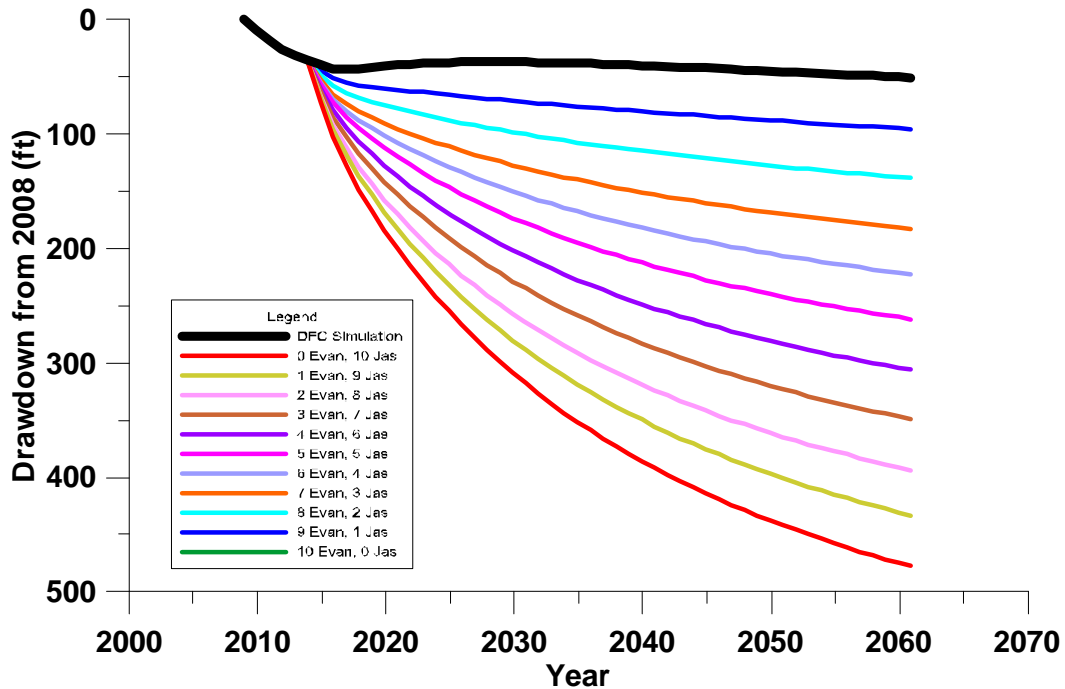


Figure D-55
Austin County - Chicot
Electro Purification Pumping - Conversion Schedule (GAM)

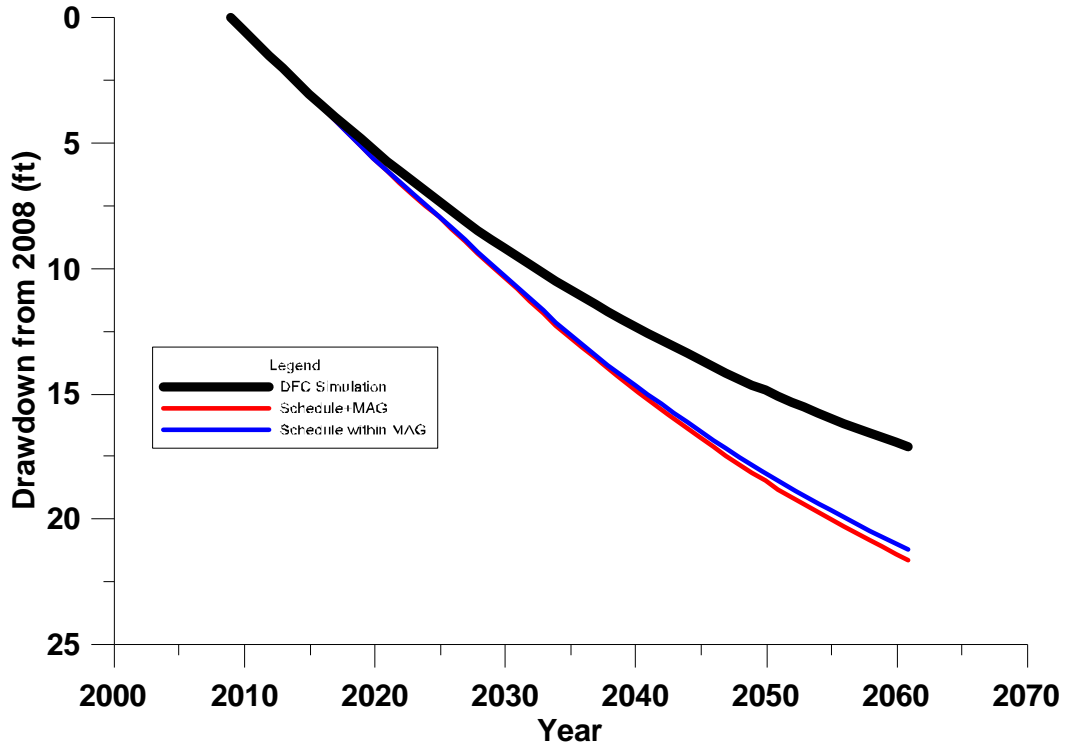


Figure D-56
Austin County - Chicot
Electro Purification Pumping - Conversion Schedule (HAGM)

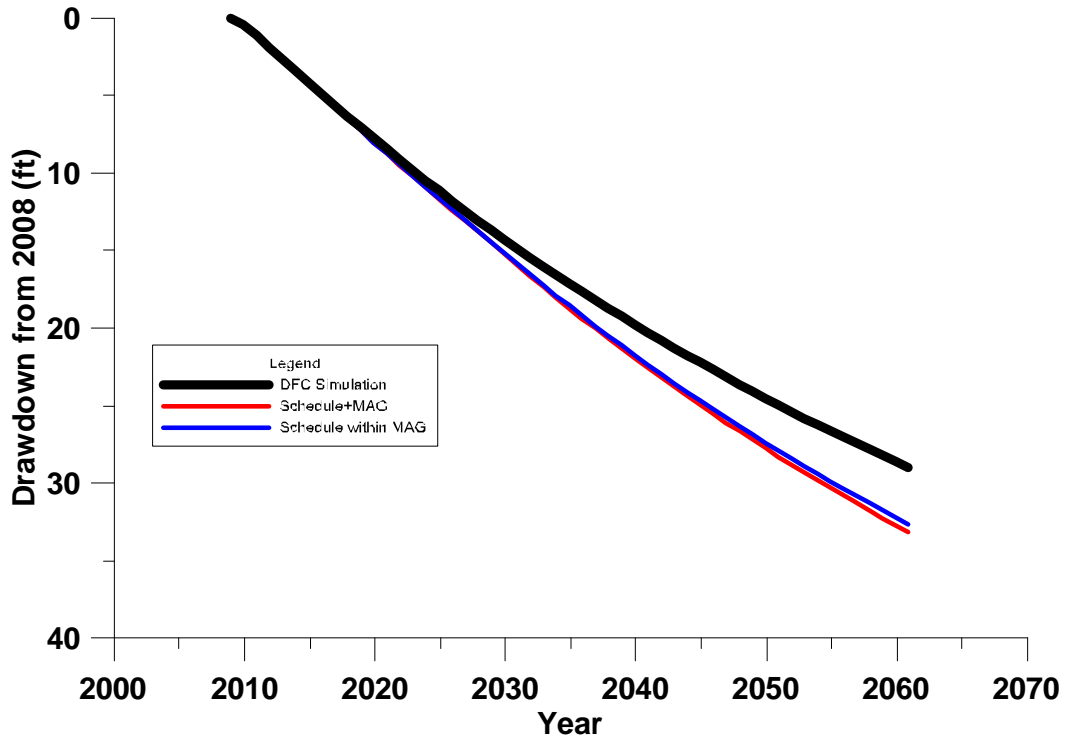


Figure D-57
Austin County - Evangeline
Electro Purification Pumping - Conversion Schedule (GAM)

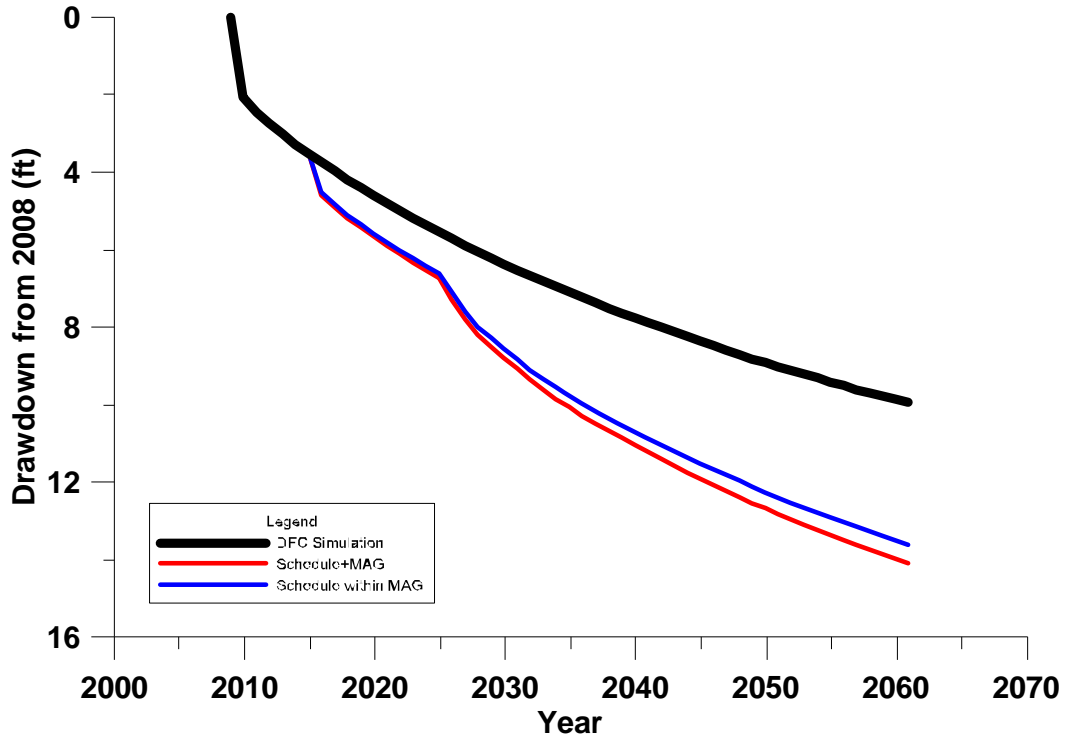


Figure D-58
Austin County - Evangeline
Electro Purification Pumping - Conversion Schedule (HAGM)

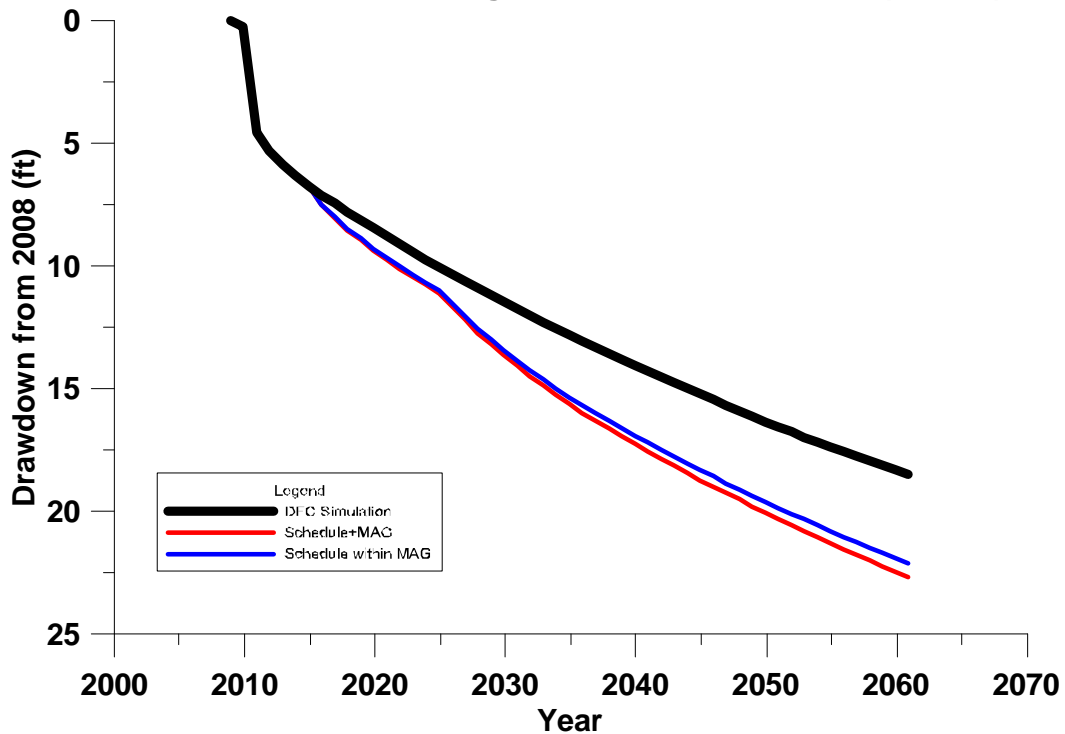


Figure D-59
Austin County - Jasper

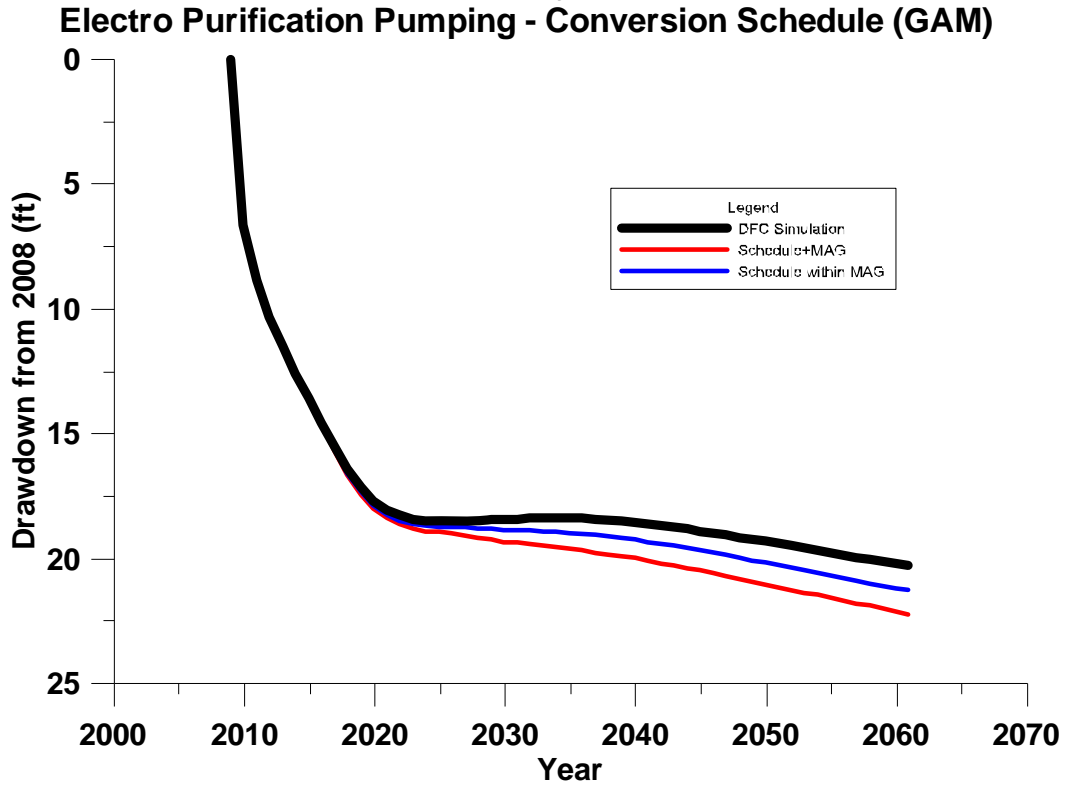


Figure D-60
Austin County - Jasper

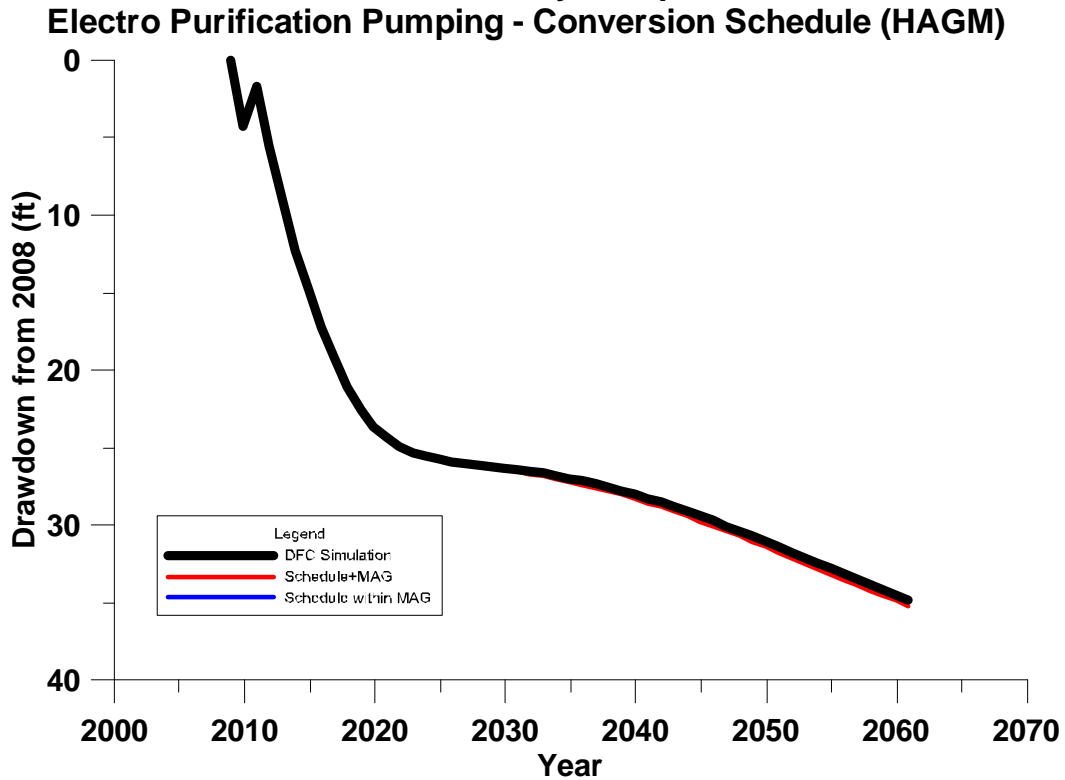


Figure D-61
Fort Bend County - Chicot
Electro Purification Pumping - Conversion Schedule (GAM)

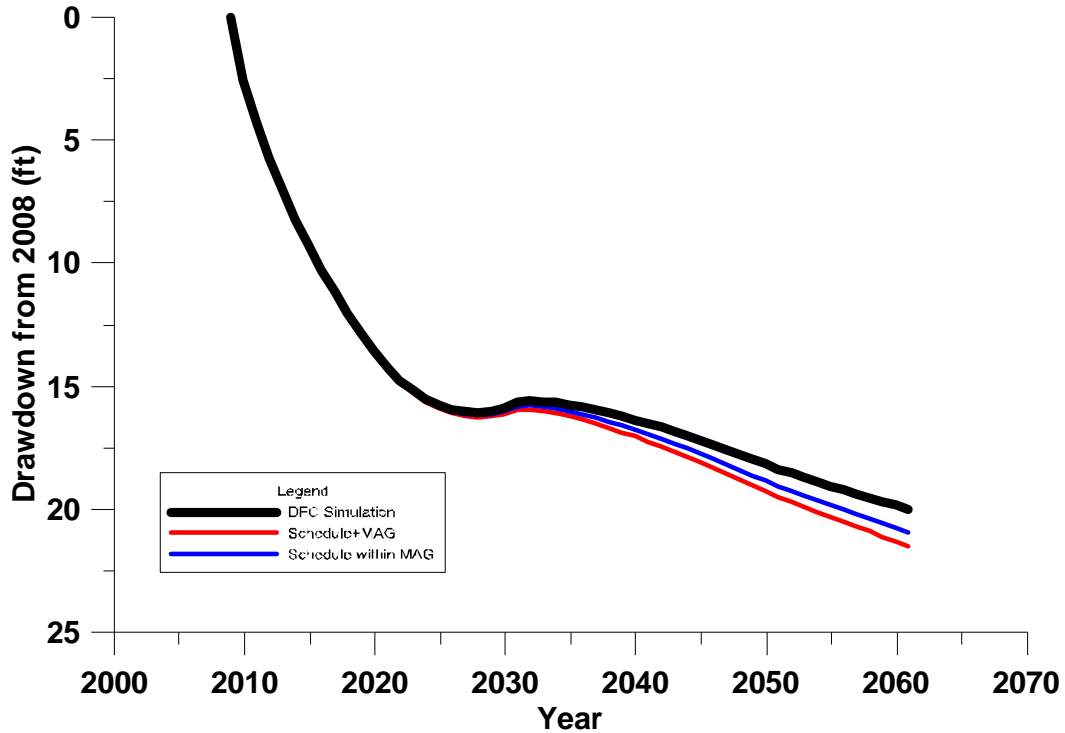


Figure D-62
Fort Bend County - Chicot
Electro Purification Pumping - Conversion Schedule (HAGM)

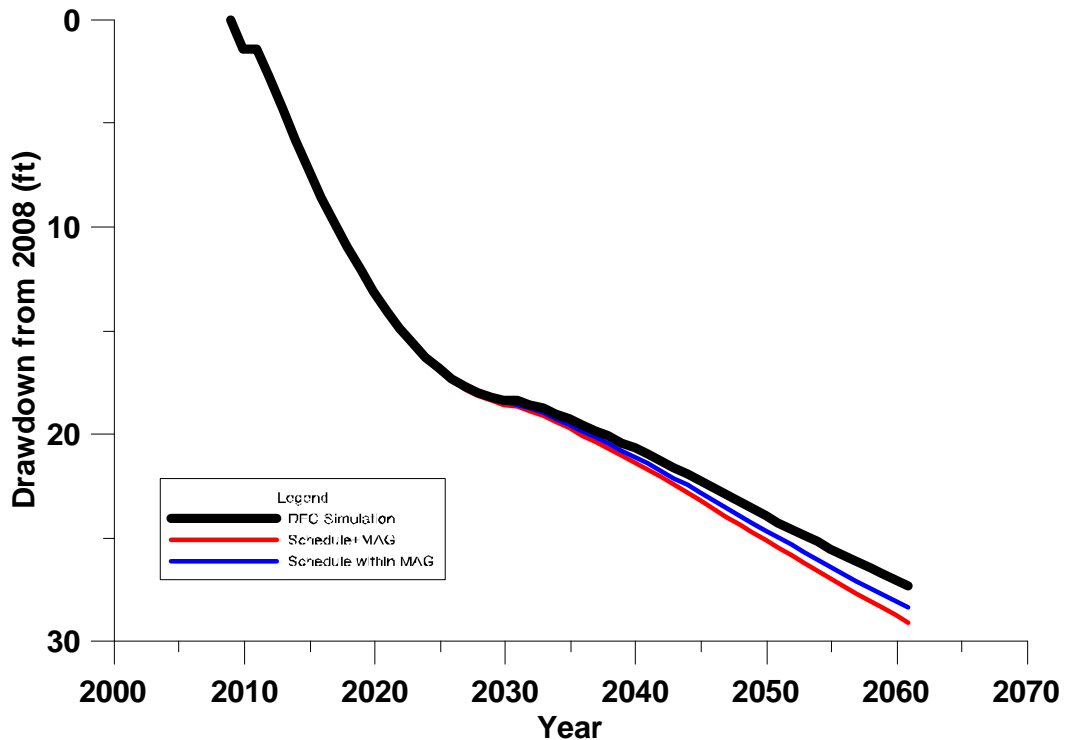


Figure D-63
Fort Bend County - Evangeline
Electro Purification Pumping - Conversion Schedule (GAM)

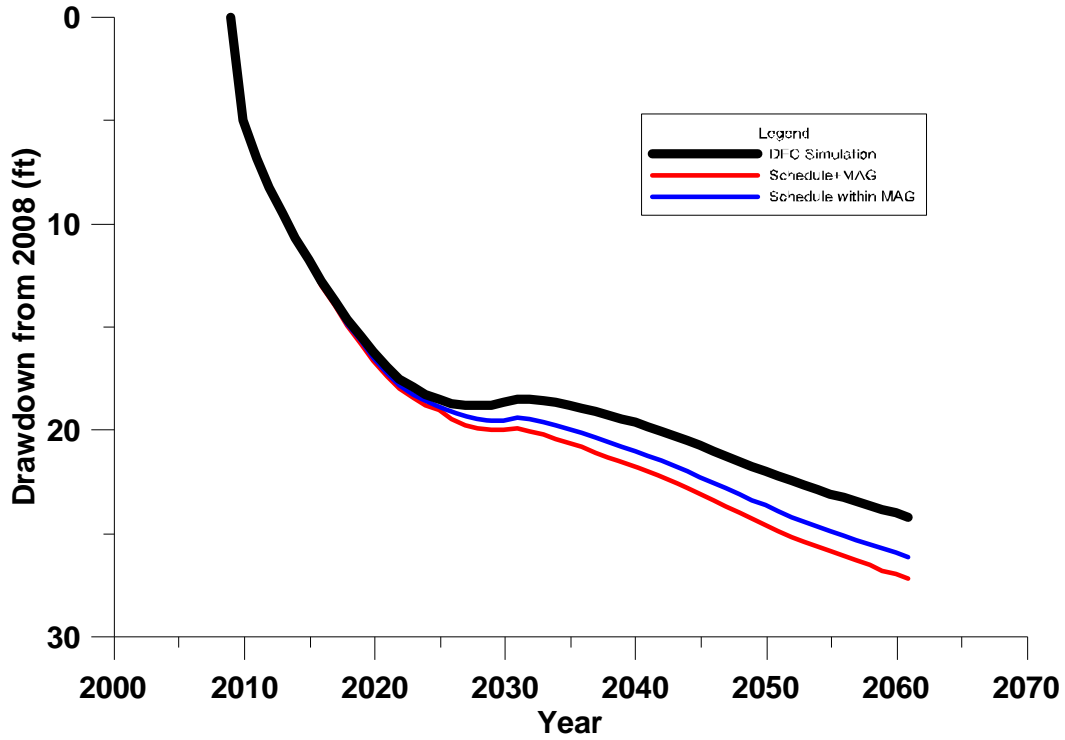


Figure D-64
Fort Bend County - Evangeline
Electro Purification Pumping - Conversion Schedule (HAGM)

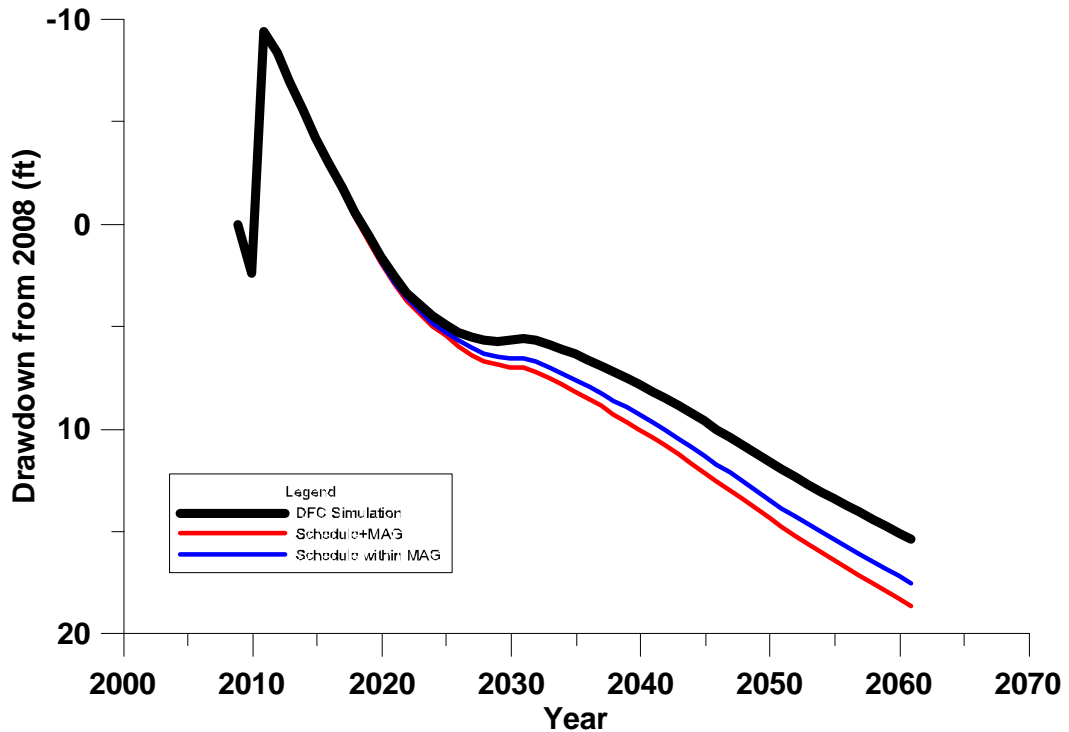


Figure D-65
Fort Bend County - Jasper
Electro Purification Pumping - Conversion Schedule (GAM)

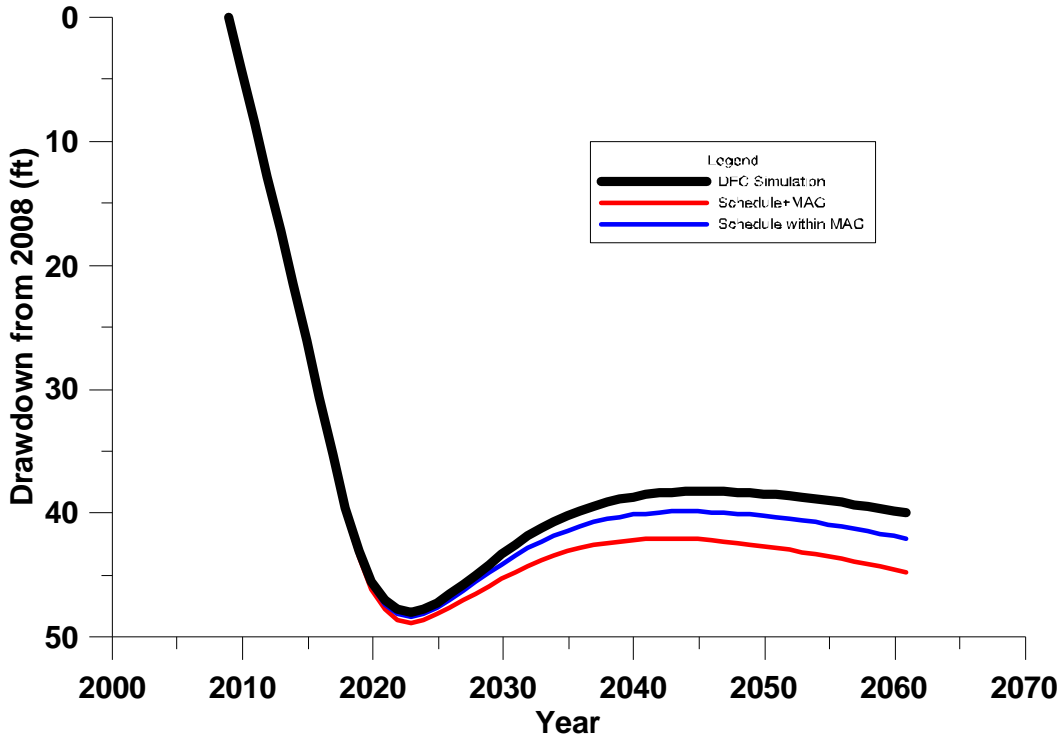


Figure D-66
Fort Bend County - Jasper
Electro Purification Pumping - Conversion Schedule (HAGM)

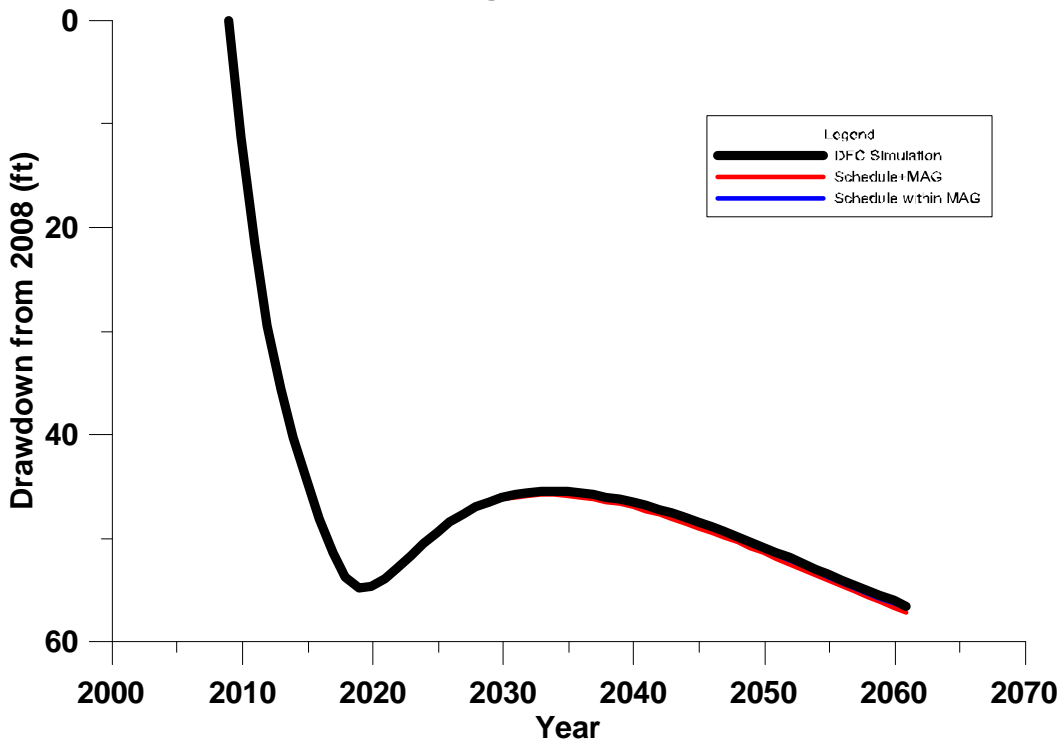


Figure D-67
Waller County - Chicot
Electro Purification Pumping - Conversion Schedule (GAM)

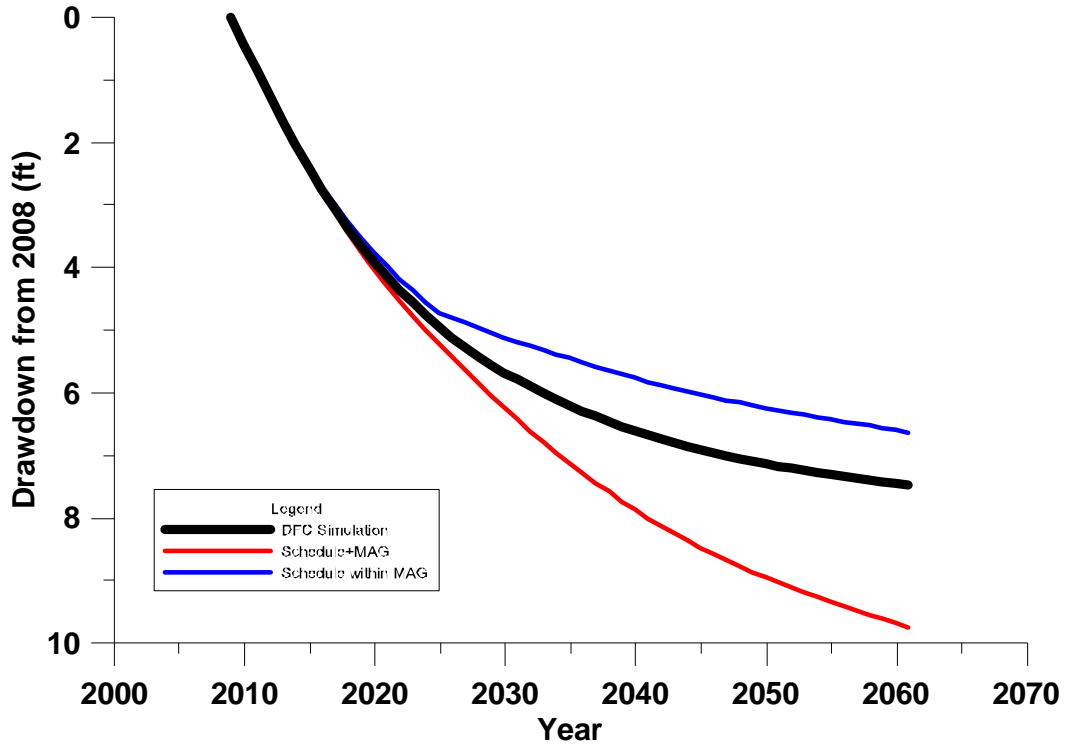


Figure D-68
Waller County - Chicot
Electro Purification Pumping - Conversion Schedule (HAGM)

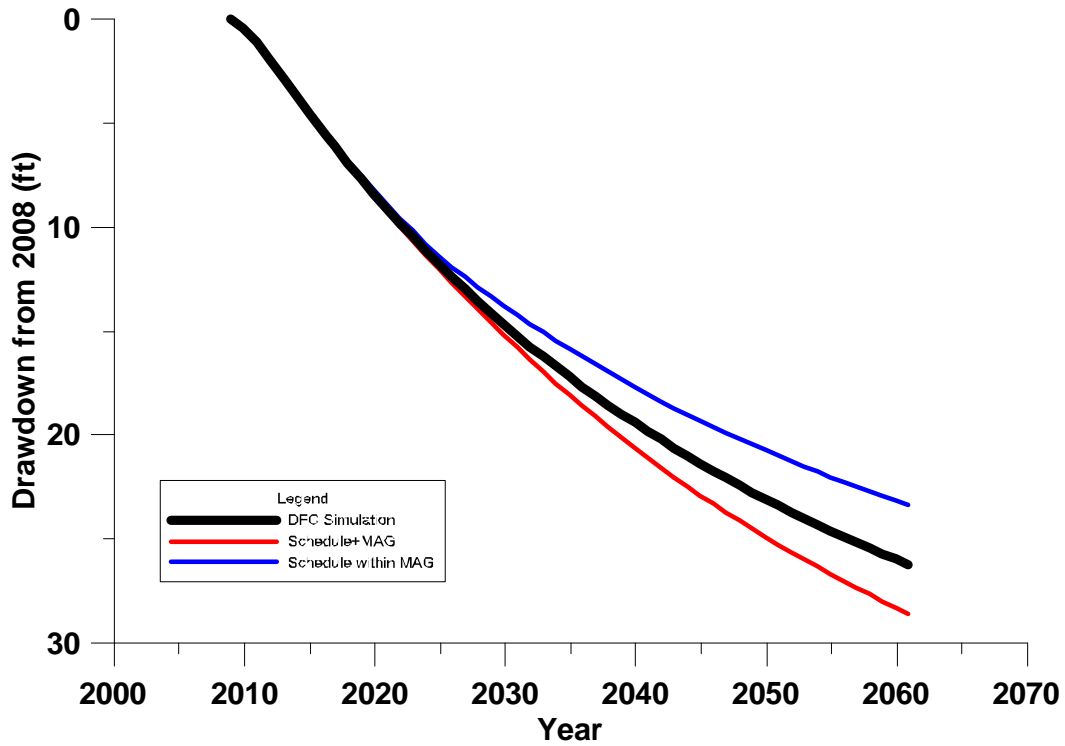


Figure D-69
Waller County - Evangeline
Electro Purification Pumping - Conversion Schedule (GAM)

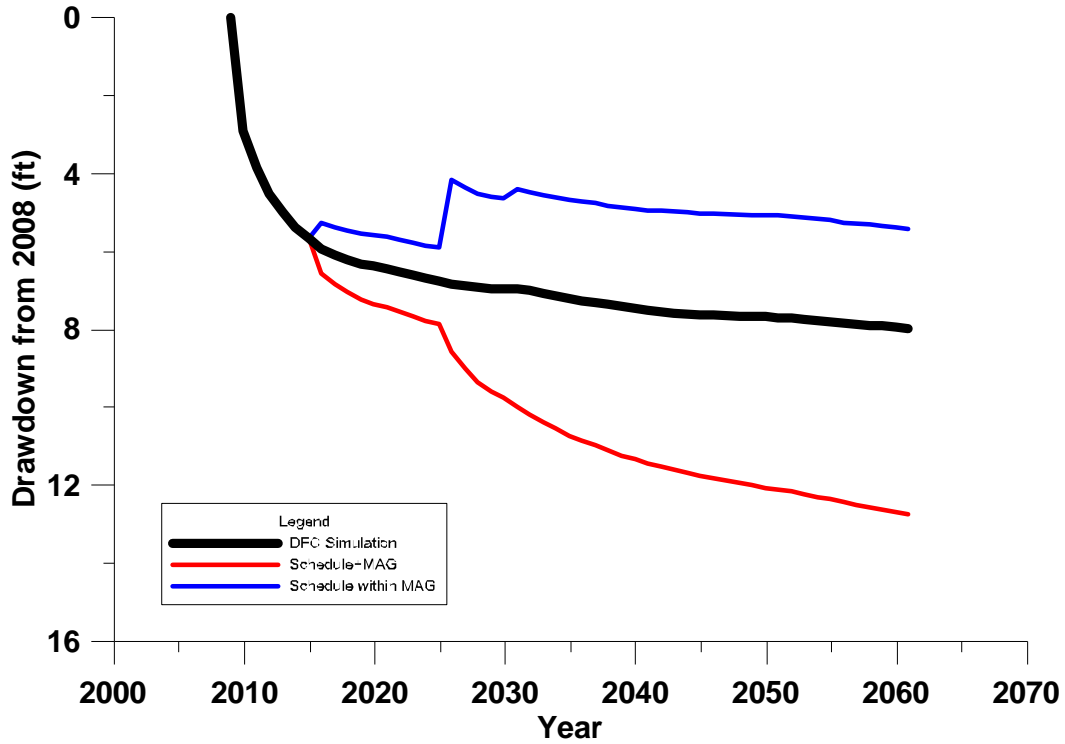


Figure D-70
Waller County - Evangeline
Electro Purification Pumping - Conversion Schedule (HAGM)

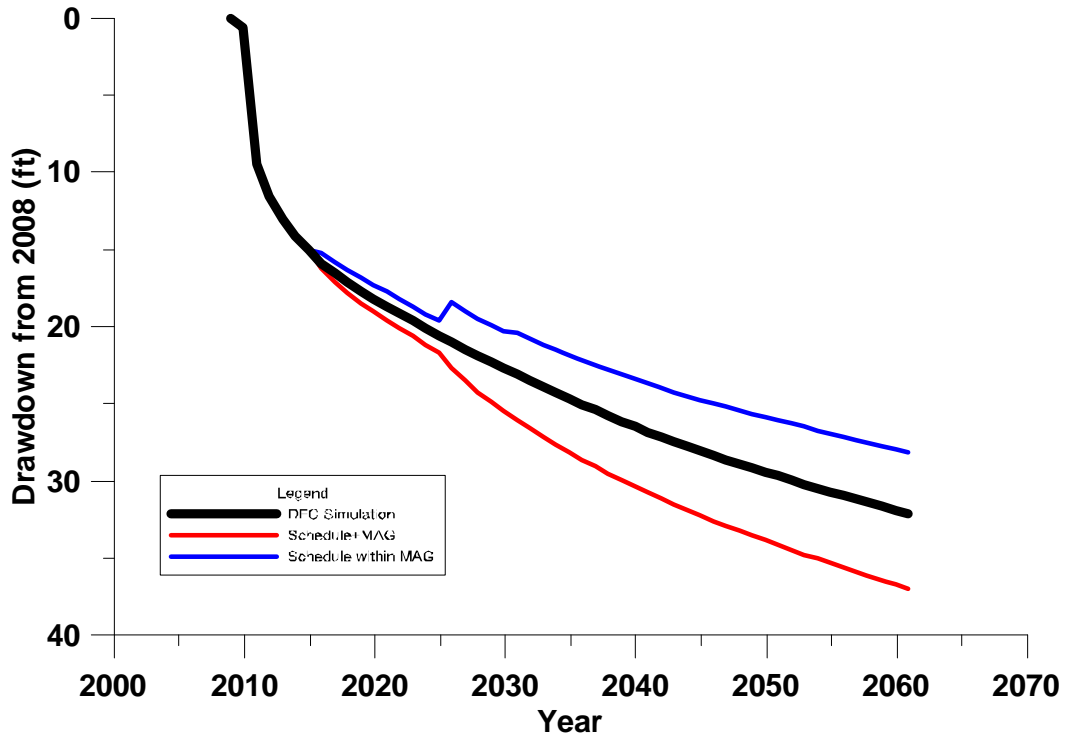


Figure D-71
Waller County - Jasper
Electro Purification Pumping - Conversion Schedule (GAM)

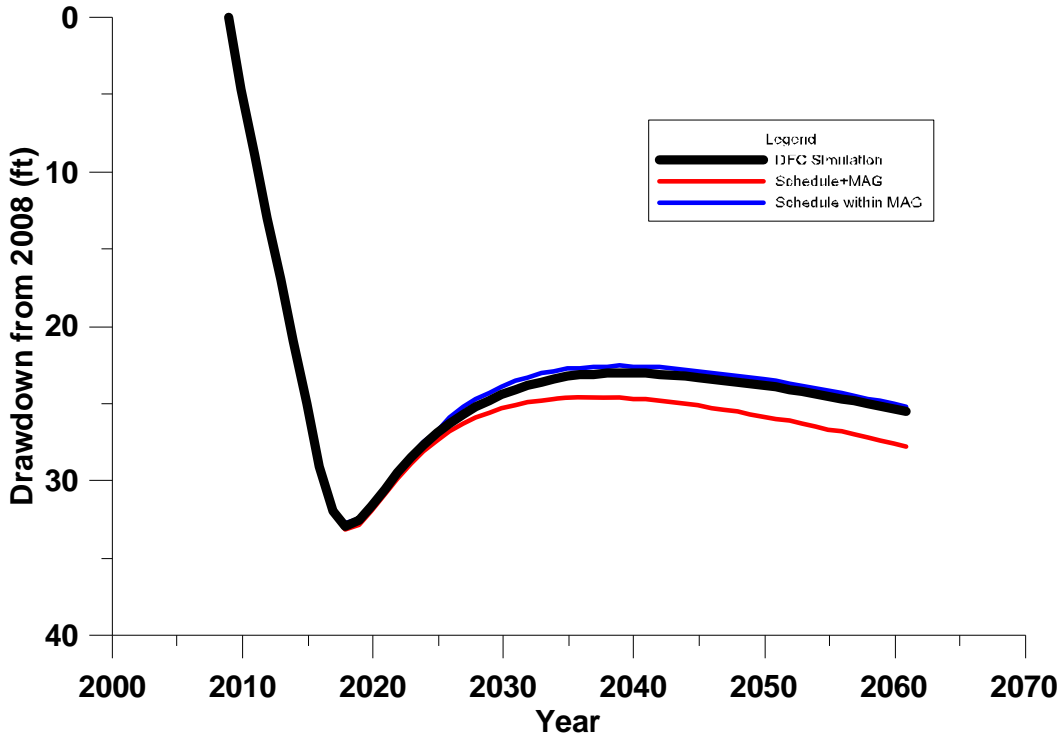
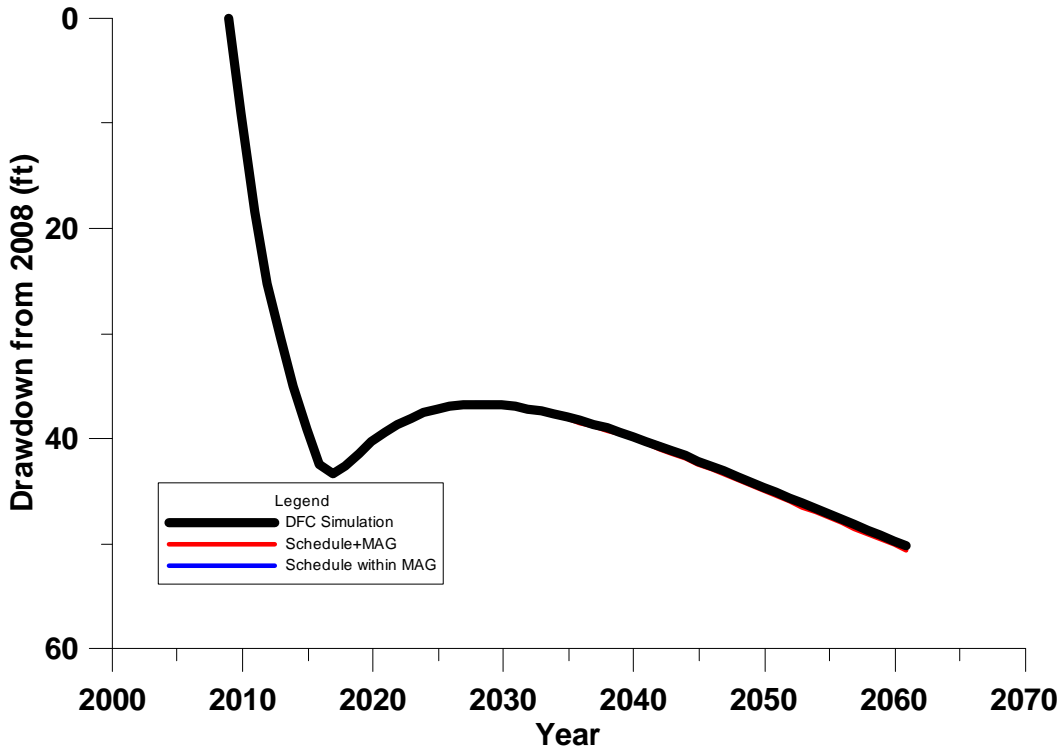


Figure D-72
Waller County - Jasper
Electro Purification Pumping - Conversion Schedule (HAGM)



Appendix E – Tables, Hydrographs, and Maps of Subsidence Estimates

Table E-1**Austin County - Simulated Subsidence from 1890 to 2060**

Scenario	Subsidence (ft) from GAM		Subsidence (ft) from HAGM	
	Average	Maximum	Average	Maximum
Baseline	0.03	0.98	0.35	2.08
1	0.04	1.03	0.38	2.12
2	0.05	1.09	0.42	2.17
3	0.05	1.13	0.44	2.22
4	0.06	1.18	0.47	2.26
5	0.08	1.51	0.51	2.31
6	0.09	1.70	0.54	2.46
7	0.10	2.04	0.57	2.80
8	0.12	2.21	0.61	2.95
9	0.14	2.41	0.65	3.13
10	0.16	2.77	0.69	3.59
11	0.04	1.03	0.37	2.12
12	0.05	1.08	0.41	2.16
13	0.05	1.12	0.43	2.20
14	0.06	1.16	0.46	2.24
15	0.07	1.43	0.50	2.28
16	0.08	1.60	0.52	2.35
17	0.09	1.92	0.55	2.66
18	0.10	2.07	0.55	2.80
19	0.11	2.24	0.57	2.96
20	0.12	2.58	0.58	3.40
21	0.14	2.59	0.69	3.46
22	0.13	2.38	0.69	3.31
23	0.12	2.23	0.69	3.22
24	0.11	1.57	0.69	2.64
25	0.10	1.43	0.69	2.61
26	0.09	1.41	0.69	2.61
27	0.08	1.38	0.69	2.61
28	0.08	1.36	0.69	2.61
29	0.06	1.30	0.69	2.59
30	0.05	1.24	0.67	2.57
31	0.07	1.33	0.49	2.28
32	0.07	1.25	0.48	2.26

Note: Red Numbers represent maximum subsidence values greater than one foot. Simulated subsidence greater than one foot are considered measureable based on model calibration

Table E-2
Fort Bend County - Simulated Subsidence from 1890 to
2060

Scenario	Subsidence (ft) from GAM		Subsidence (ft) from HAGM	
	Average	Maximum	Average	Maximum
Baseline	1.75	6.65	2.49	5.61
1	1.78	6.65	2.51	5.61
2	1.81	6.65	2.53	5.61
3	1.85	6.65	2.54	5.61
4	1.88	6.65	2.56	5.61
5	1.91	6.65	2.57	5.61
6	1.95	6.65	2.59	5.61
7	1.99	6.65	2.61	5.61
8	2.03	6.65	2.63	5.61
9	2.07	6.65	2.65	5.61
10	2.11	6.65	2.67	5.61
11	1.77	6.65	2.51	5.61
12	1.79	6.65	2.52	5.61
13	1.82	6.65	2.53	5.61
14	1.84	6.65	2.54	5.61
15	1.86	6.65	2.55	5.61
16	1.89	6.65	2.57	5.61
17	1.92	6.65	2.58	5.61
18	1.95	6.65	2.59	5.61
19	1.97	6.65	2.60	5.61
20	2.00	6.65	2.61	5.61
21	2.09	6.65	2.66	5.61
22	2.07	6.65	2.67	5.61
23	2.04	6.65	2.66	5.61
24	2.00	6.65	2.66	5.61
25	1.98	6.65	2.67	5.61
26	1.96	6.65	2.67	5.61
27	1.94	6.65	2.67	5.61
28	1.91	6.65	2.67	5.61
29	1.88	6.65	2.67	5.61
30	1.87	6.65	2.67	5.61
31	1.90	6.65	2.57	5.61
32	1.86	6.65	2.55	5.61

Note: Red Numbers represent maximum subsidence values greater than one foot. Simulated subsidence greater than one foot are considered measureable based on model calibration

Table E-3**Waller County - Simulated Subsidence from 1890 to 2060**

Scenario	Subsidence (ft) from GAM		Subsidence (ft) from HAGM	
	Average	Maximum	Average	Maximum
Baseline	0.38	5.49	0.61	3.52
1	0.40	5.56	0.63	3.58
2	0.41	5.61	0.65	3.62
3	0.43	5.71	0.67	3.68
4	0.44	5.79	0.68	3.74
5	0.46	5.84	0.70	3.78
6	0.48	5.94	0.72	3.85
7	0.49	6.01	0.74	4.46
8	0.50	6.06	0.75	4.65
9	0.51	6.09	0.76	4.82
10	0.52	6.13	0.77	5.01
11	0.39	5.47	0.61	3.49
12	0.39	5.46	0.60	3.45
13	0.39	5.46	0.61	3.43
14	0.40	5.45	0.61	3.41
15	0.40	5.44	0.60	3.37
16	0.41	5.44	0.61	3.51
17	0.42	5.43	0.61	4.31
18	0.42	5.43	0.62	4.47
19	0.43	5.43	0.62	4.62
20	0.44	5.43	0.63	4.78
21	0.51	6.11	0.77	4.32
22	0.50	6.10	0.77	3.99
23	0.48	6.06	0.77	3.95
24	0.48	6.06	0.78	3.95
25	0.46	6.03	0.78	3.93
26	0.45	6.00	0.78	3.92
27	0.44	5.99	0.79	3.91
28	0.43	5.95	0.79	3.89
29	0.43	5.95	0.80	3.89
30	0.43	5.96	0.81	3.90
31	0.45	5.80	0.70	3.76
32	0.41	5.47	0.61	3.37

Note: Red Numbers represent maximum subsidence values greater than one foot. Simulated subsidence greater than one foot are considered measureable based on model calibration

Table E-4**Project Area - Simulated Subsidence from 1890 to 2060**

Scenario	Subsidence (ft) from GAM		Subsidence (ft) from HAGM	
	Average	Maximum	Average	Maximum
Baseline	0.11	0.85	0.77	1.97
1	0.24	0.97	1.00	2.09
2	0.42	1.08	1.23	2.18
3	0.61	1.27	1.45	2.36
4	0.81	2.02	1.68	2.90
5	1.03	2.45	1.91	3.33
6	1.25	2.78	2.14	3.64
7	1.49	3.62	2.37	4.46
8	1.71	3.82	2.58	4.65
9	1.93	4.01	2.79	4.82
10	2.16	4.22	3.00	5.01
11	0.23	0.94	0.98	2.05
12	0.39	1.01	1.19	2.11
13	0.56	1.23	1.39	2.26
14	0.75	1.97	1.60	2.81
15	0.94	2.35	1.81	3.22
16	1.14	2.65	2.01	3.51
17	1.36	3.47	2.22	4.31
18	1.55	3.65	2.41	4.47
19	1.74	3.82	2.59	4.62
20	1.94	4.00	2.77	4.78
21	1.94	3.40	2.84	4.32
22	1.73	2.98	2.69	3.99
23	1.52	2.68	2.54	3.77
24	1.33	2.52	2.40	3.66
25	1.12	1.71	2.25	2.91
26	0.93	1.50	2.10	2.79
27	0.75	1.43	1.94	2.75
28	0.58	1.28	1.80	2.65
29	0.42	1.21	1.66	2.61
30	0.27	1.16	1.53	2.61
31	0.99	2.18	1.87	3.07
32	0.91	2.09	1.77	2.97

Note: Red Numbers represent maximum subsidence values greater than one foot. Simulated subsidence greater than one foot are considered measureable based on model calibration

Table E-5
Austin County - Simulated Subsidence from 1890 to 2060
Attributable to Electro Purification Pumping

Scenario	Subsidence (ft) from GAM		Subsidence (ft) from HAGM	
	Average	Maximum	Average	Maximum
Baseline	0	0	0	0
1	0.01	0.05	0.03	0.04
2	0.02	0.11	0.07	0.09
3	0.02	0.15	0.09	0.14
4	0.03	0.20	0.12	0.18
5	0.05	0.53	0.16	0.23
6	0.06	0.72	0.19	0.38
7	0.07	1.06	0.22	0.72
8	0.09	1.23	0.26	0.87
9	0.11	1.43	0.30	1.05
10	0.13	1.79	0.34	1.51
11	0.01	0.05	0.02	0.04
12	0.02	0.10	0.06	0.08
13	0.02	0.14	0.08	0.12
14	0.03	0.18	0.11	0.16
15	0.04	0.45	0.15	0.20
16	0.05	0.62	0.17	0.27
17	0.06	0.94	0.20	0.58
18	0.07	1.09	0.20	0.72
19	0.08	1.26	0.22	0.88
20	0.09	1.60	0.23	1.32
21	0.11	1.61	0.34	1.38
22	0.10	1.40	0.34	1.23
23	0.09	1.25	0.34	1.14
24	0.08	0.59	0.34	0.56
25	0.07	0.45	0.34	0.53
26	0.06	0.43	0.34	0.53
27	0.05	0.40	0.34	0.53
28	0.05	0.38	0.34	0.53
29	0.03	0.32	0.34	0.51
30	0.02	0.26	0.32	0.49
31	0.04	0.35	0.14	0.20
32	0.04	0.27	0.13	0.18

Note: Red Numbers represent maximum subsidence values greater than one foot. Simulated subsidence greater than one foot are considered measureable based on model calibration

Table E-6
Fort Bend County - Simulated Subsidence from 1890 to
2060 Attributable to Electro Purification Pumping

Scenario	Subsidence (ft) from GAM		Subsidence (ft) from HAGM	
	Average	Maximum	Average	Maximum
Baseline	0	0	0	0
1	0.03	0.00	0.02	0.00
2	0.06	0.00	0.04	0.00
3	0.10	0.00	0.05	0.00
4	0.13	0.00	0.07	0.00
5	0.16	0.00	0.08	0.00
6	0.20	0.00	0.10	0.00
7	0.24	0.00	0.12	0.00
8	0.28	0.00	0.14	0.00
9	0.32	0.00	0.16	0.00
10	0.36	0.00	0.18	0.00
11	0.02	0.00	0.02	0.00
12	0.04	0.00	0.03	0.00
13	0.07	0.00	0.04	0.00
14	0.09	0.00	0.05	0.00
15	0.11	0.00	0.06	0.00
16	0.14	0.00	0.08	0.00
17	0.17	0.00	0.09	0.00
18	0.20	0.00	0.10	0.00
19	0.22	0.00	0.11	0.00
20	0.25	0.00	0.12	0.00
21	0.34	0.00	0.17	0.00
22	0.32	0.00	0.18	0.00
23	0.29	0.00	0.17	0.00
24	0.25	0.00	0.17	0.00
25	0.23	0.00	0.18	0.00
26	0.21	0.00	0.18	0.00
27	0.19	0.00	0.18	0.00
28	0.16	0.00	0.18	0.00
29	0.13	0.00	0.18	0.00
30	0.12	0.00	0.18	0.00
31	0.15	0.00	0.08	0.00
32	0.11	0.00	0.06	0.00

Note: Red Numbers represent maximum subsidence values greater than one foot. Simulated subsidence greater than one foot are considered measureable based on model calibration

Table E-7
Waller County - Simulated Subsidence from 1890 to 2060
Attributable to Electro Purification Pumping

Scenario	Subsidence (ft) from GAM		Subsidence (ft) from HAGM	
	Average	Maximum	Average	Maximum
Baseline	0	0	0	0
1	0.02	0.07	0.02	0.06
2	0.03	0.12	0.04	0.10
3	0.05	0.22	0.06	0.16
4	0.06	0.30	0.07	0.22
5	0.08	0.35	0.09	0.26
6	0.10	0.45	0.11	0.33
7	0.11	0.52	0.13	0.94
8	0.12	0.57	0.14	1.13
9	0.13	0.60	0.15	1.30
10	0.14	0.64	0.16	1.49
11	0.01	-0.02	0.00	-0.03
12	0.01	-0.03	-0.01	-0.07
13	0.01	-0.03	0.00	-0.09
14	0.02	-0.04	0.00	-0.11
15	0.02	-0.05	-0.01	-0.15
16	0.03	-0.05	0.00	-0.01
17	0.04	-0.06	0.00	0.79
18	0.04	-0.06	0.01	0.95
19	0.05	-0.06	0.01	1.10
20	0.06	-0.06	0.02	1.26
21	0.13	0.62	0.16	0.80
22	0.12	0.61	0.16	0.47
23	0.10	0.57	0.16	0.43
24	0.10	0.57	0.17	0.43
25	0.08	0.54	0.17	0.41
26	0.07	0.51	0.17	0.40
27	0.06	0.50	0.18	0.39
28	0.05	0.46	0.18	0.37
29	0.05	0.46	0.19	0.37
30	0.05	0.47	0.20	0.38
31	0.07	0.31	0.09	0.24
32	0.03	-0.02	0.00	-0.15

Note: Red Numbers represent maximum subsidence values greater than one foot. Simulated subsidence greater than one foot are considered measureable based on model calibration

Table E-8
Project Area - Simulated Subsidence from 1890 to 2060
Attributable to Electro Purification Pumping

Scenario	Subsidence (ft) from GAM		Subsidence (ft) from HAGM	
	Average	Maximum	Average	Maximum
Baseline	0	0	0	0
1	0.13	0.12	0.23	0.12
2	0.31	0.23	0.46	0.21
3	0.50	0.42	0.68	0.39
4	0.70	1.17	0.91	0.93
5	0.92	1.60	1.14	1.36
6	1.14	1.93	1.37	1.67
7	1.38	2.77	1.60	2.49
8	1.60	2.97	1.81	2.68
9	1.82	3.16	2.02	2.85
10	2.05	3.37	2.23	3.04
11	0.12	0.09	0.21	0.08
12	0.28	0.16	0.42	0.14
13	0.45	0.38	0.62	0.29
14	0.64	1.12	0.83	0.84
15	0.83	1.50	1.04	1.25
16	1.03	1.80	1.24	1.54
17	1.25	2.62	1.45	2.34
18	1.44	2.80	1.64	2.50
19	1.63	2.97	1.82	2.65
20	1.83	3.15	2.00	2.81
21	1.83	2.55	2.07	2.35
22	1.62	2.13	1.92	2.02
23	1.41	1.83	1.77	1.80
24	1.22	1.67	1.63	1.69
25	1.01	0.86	1.48	0.94
26	0.82	0.65	1.33	0.82
27	0.64	0.58	1.17	0.78
28	0.47	0.43	1.03	0.68
29	0.31	0.36	0.89	0.64
30	0.16	0.31	0.76	0.64
31	0.88	1.33	1.10	1.10
32	0.80	1.24	1.00	1.00

Note: Red Numbers represent maximum subsidence values greater than one foot. Simulated subsidence greater than one foot are considered measureable based on model calibration

Table E-9
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 1 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-5429	54	66	6180054.5	19142336	0.15	1	0.02	0.31	2.77	0.59	0.28	2.74	0.57
BAUS-5430	54	66	6180054.5	19142336	0.15	1	0.02	0.31	2.77	0.59	0.28	2.74	0.57
BWLL-5117	53	69	6191012.5	19154344	0.34	1	0.02	1.16	3.31	1.91	1.14	3.28	1.88
BWLL-5481	53	70	6191500	19157906	0.36	1	0.24	0.91	2.37	1.42	0.67	2.14	1.19
BWLL-5006	54	69	6190699	19153424	0.46	1	0.07	0.73	2.28	1.16	0.66	2.21	1.09
BAUS-4159	53	66	6177818.5	19144046	0.47	1	0.02	0.41	2.51	0.78	0.39	2.49	0.76
BAUS-4158	53	66	6177811.5	19144248	0.49	1	0.02	0.41	2.51	0.78	0.39	2.49	0.76
BWLL-5541	52	69	6186065.5	19157628	0.50	1	0.02	0.91	2.86	1.52	0.89	2.84	1.49
BWLL-5541	53	69	6188533	19157786	0.54	1	0.02	1.16	3.31	1.91	1.14	3.28	1.88
BWLL-5543	52	69	6186496.5	19157650	0.56	1	0.02	0.91	2.86	1.52	0.89	2.84	1.49
BAUS-4458	51	67	6175604	19159156	0.63	1	0.02	0.74	2.59	1.33	0.72	2.57	1.31
BWLL-4133	51	67	6175182.5	19158636	0.63	1	0.02	0.74	2.59	1.33	0.72	2.57	1.31
BAUS-5436	51	67	6174074	19157298	0.72	1	0.02	0.74	2.59	1.33	0.72	2.57	1.31
BAUS-5447	51	67	6173795	19157412	0.78	1	0.02	0.74	2.59	1.33	0.72	2.57	1.31
BAUS-4340	53	65	6171277.5	19142192	0.84	1	0.02	0.22	2.18	0.47	0.19	2.16	0.45
BWLL-4363	52	69	6186773	19159558	0.88	1	0.02	0.91	2.86	1.52	0.89	2.84	1.49
BAUS-5426	51	67	6173430.5	19159360	0.98	1	0.02	0.74	2.59	1.33	0.72	2.57	1.31
BAUS-5401	51	67	6172709	19157480	0.99	1	0.02	0.74	2.59	1.33	0.72	2.57	1.31
BAUS-5398	51	66	6171645	19154492	1.25	1	0.08	0.71	2.27	1.14	0.63	2.19	1.06
BAUS-4236	50	67	6173220	19161806	1.31	1	0.04	0.59	1.89	0.97	0.54	1.85	0.93
6517415	55	67	6187339.5	19141354	1.34	1	0.03	0.38	1.87	0.64	0.36	1.84	0.61
BAUS-4485	50	67	6172028.5	19160648	1.34	1	0.04	0.59	1.89	0.97	0.54	1.85	0.93
BAUS-4325	50	67	6172780	19161790	1.36	1	0.04	0.59	1.89	0.97	0.54	1.85	0.93
BAUS-4518	50	68	6174657	19163476	1.42	1	0.02	0.42	1.65	0.76	0.41	1.64	0.74
BAUS-5298	50	67	6172278	19161868	1.44	1	0.04	0.59	1.89	0.97	0.54	1.85	0.93
BAUS-4515	51	66	6170610	19153510	1.50	1	0.08	0.71	2.27	1.14	0.63	2.19	1.06
BAUS-4519	50	68	6175159	19164204	1.52	1	0.02	0.42	1.65	0.76	0.41	1.64	0.74
BAUS-5397	51	66	6169866.5	19155934	1.52	1	0.08	0.71	2.27	1.14	0.63	2.19	1.06
BAUS-0002A	50	68	6175328	19164412	1.54	1	0.02	0.42	1.65	0.76	0.41	1.64	0.74
BAUS-0002B	50	68	6175328	19164412	1.54	1	0.02	0.42	1.65	0.76	0.41	1.64	0.74
BAUS-5400	50	67	6171322	19161498	1.54	1	0.04	0.59	1.89	0.97	0.54	1.85	0.93
BAUS-5402	50	67	6170748.5	19160828	1.56	1	0.04	0.59	1.89	0.97	0.54	1.85	0.93
BWLL-5690	51	69	6184161	19164328	1.65	1	0.02	0.57	1.99	0.98	0.55	1.97	0.96
BAUS-4430	50	66	6168784	19157800	1.73	1	0.02	0.45	1.64	0.77	0.43	1.62	0.75
BAUS-4185	52	66	6170700	19150982	1.73	1	0.02	0.58	2.56	1.02	0.55	2.54	1.00
BAUS-5399	50	66	6168767	19157550	1.73	1	0.02	0.45	1.64	0.77	0.43	1.62	0.75
BWLL-4303	50	68	6177915	19165922	1.75	1	0.02	0.42	1.65	0.76	0.41	1.64	0.74
6509702	52	71	6193335.5	19165170	1.76	1	0.38	0.83	1.80	1.14	0.45	1.42	0.76
BAUS-4429	50	66	6168601	19157996	1.77	1	0.02	0.45	1.64	0.77	0.43	1.62	0.75
BAUS-5297	50	68	6173472	19165068	1.79	1	0.02	0.42	1.65	0.76	0.41	1.64	0.74
BAUS-4129	55	65	6178444	19131512	1.81	1	0.03	0.18	1.47	0.36	0.16	1.44	0.33
BWLL-4992	50	68	6177988.5	19166330	1.83	1	0.02	0.42	1.65	0.76	0.41	1.64	0.74
BWLL-4272	50	68	6177805.5	19166526	1.87	1	0.02	0.42	1.65	0.76	0.41	1.64	0.74
BAUS-0024	56	65	6179473	19131326	1.87	1	0.03	0.27	1.30	0.40	0.24	1.27	0.37
BWLL-5674	51	69	6184132.5	19165744	1.92	1	0.02	0.57	1.99	0.98	0.55	1.97	0.96
BWLL-4161	50	69	6177699	19167028	1.96	1	0.02	0.31	1.23	0.57	0.29	1.22	0.56
BAUS-4299	50	69	6178487	19167158	1.99	1	0.02	0.31	1.23	0.57	0.29	1.22	0.56
BWLL-5082	51	69	6183630	19166128	1.99	1	0.02	0.57	1.99	0.98	0.55	1.97	0.96
BAUS-4138	51	65	6166124	19148388	2.10	1	0.06	0.48	1.73	0.77	0.42	1.67	0.71
6624203	51	65	6166932	19150042	2.15	1	0.06	0.48	1.73	0.77	0.42	1.67	0.71
BWLL-4134	52	71	6197009.5	19166208	2.19	1	0.38	0.83	1.80	1.14	0.45	1.42	0.76
BAUS-4137	51	65	6165560.5	19149382	2.29	1	0.06	0.48	1.73	0.77	0.42	1.67	0.71
BAUS-5120	50	66	6166456	19161362	2.33	1	0.02	0.45	1.64	0.77	0.43	1.62	0.75
BAUS-4552	49	66	6166768	19162486	2.37	1	0.01	0.26	1.07	0.47	0.25	1.05	0.45
BAUS-4235	49	66	6166764.5	19162588	2.38	1	0.01	0.26	1.07	0.47	0.25	1.05	0.45
BAUS-4324	49	66	6166588.5	19162582	2.41	1	0.01	0.26	1.07	0.47	0.25	1.05	0.45
BAUS-4067	50	65	6165176.5	19155240	2.42	1	0.03	0.36	1.36	0.61	0.33	1.33	0.58
BAUS-5146	56	64	6177989	19128236	2.43	1	0.04	0.24	1.10	0.35	0.20	1.06	0.31
BAUS-4288	49	66	6166412.5	19162576	2.44	1	0.01	0.26	1.07	0.47	0.25	1.05	0.45
BAUS-5437	49	68	6171384	19168042	2.48	1	0.01	0.12	0.84	0.32	0.10	0.83	0.31
BAUS-4309	49	66	6166229.5	19162772	2.49	1	0.01	0.26	1.07	0.47	0.25	1.05	0.45
BAUS-4558	49	66	6166226	19162872	2.50	1	0.01	0.26	1.07	0.47	0.25	1.05	0.45

Table E-9
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 2 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4140	50	65	6164582	19154612	2.54	1	0.03	0.36	1.36	0.61	0.33	1.33	0.58
BAUS-5394	50	65	6164439	19155042	2.56	1	0.03	0.36	1.36	0.61	0.33	1.33	0.58
BAUS-5395C	50	65	6164439	19155042	2.56	1	0.03	0.36	1.36	0.61	0.33	1.33	0.58
BAUS-4321	49	66	6165863.5	19163164	2.58	1	0.01	0.26	1.07	0.47	0.25	1.05	0.45
BAUS-4314	49	66	6165765	19163464	2.63	1	0.01	0.26	1.07	0.47	0.25	1.05	0.45
BAUS-4495	49	66	6165427.5	19163046	2.64	1	0.01	0.26	1.07	0.47	0.25	1.05	0.45
BAUS-4541	49	66	6165427.5	19163046	2.64	1	0.01	0.26	1.07	0.47	0.25	1.05	0.45
6624102	51	64	6161925	19145490	2.65	1	0.04	0.33	1.33	0.54	0.28	1.29	0.50
BAUS-5425	51	65	6164243.5	19152214	2.71	1	0.06	0.48	1.73	0.77	0.42	1.67	0.71
BAUS-5344	49	67	6168874	19168294	2.78	1	0.02	0.28	1.17	0.50	0.26	1.15	0.49
BWLL-4987	53	72	6203934.5	19164638	2.85	1	0.81	1.20	1.90	1.42	0.38	1.09	0.60
BAUS-5251	49	66	6163571	19161666	2.86	1	0.01	0.26	1.07	0.47	0.25	1.05	0.45
BWLL-5574	53	72	6204376	19164880	2.95	1	0.81	1.20	1.90	1.42	0.38	1.09	0.60
BWLL-5666	53	72	6204376	19164880	2.95	1	0.81	1.20	1.90	1.42	0.38	1.09	0.60
BWLL-5671	53	72	6203411.5	19166926	3.05	1	0.81	1.20	1.90	1.42	0.38	1.09	0.60
BAUS-4315	50	65	6162008	19152698	3.09	1	0.03	0.36	1.36	0.61	0.33	1.33	0.58
6517418	57	67	6193783.5	19132988	3.16	1	0.16	0.40	1.35	0.57	0.24	1.18	0.41
6616810	48	67	6165870	19168340	3.17	1	0.01	0.09	0.61	0.22	0.08	0.60	0.21
BAUS-4001	50	64	6161187.5	19153480	3.21	1	0.02	0.23	0.99	0.40	0.22	0.97	0.38
BWLL-5144	54	72	6208083.5	19161954	3.32	1	1.15	1.61	2.47	1.86	0.45	1.32	0.71
6616808	48	67	6164696	19168372	3.33	1	0.01	0.09	0.61	0.22	0.08	0.60	0.21
BAUS-5369	50	64	6159339.5	19150220	3.40	1	0.02	0.23	0.99	0.40	0.22	0.97	0.38
6616807	48	67	6164759	19169286	3.44	1	0.01	0.09	0.61	0.22	0.08	0.60	0.21
BAUS-4165	50	64	6159584.5	19151498	3.47	1	0.02	0.23	0.99	0.40	0.22	0.97	0.38
BAUS-4332	56	63	6173628.5	19123240	3.49	1	0.20	0.36	1.16	0.48	0.16	0.96	0.29
BWLL-5283	54	73	6206956.5	19166268	3.50	1	2.76	3.36	4.51	3.67	0.60	1.75	0.91
BAUS-4272	49	65	6159772.5	19161124	3.53	1	0.01	0.19	0.87	0.33	0.17	0.85	0.31
BAUS-0025	48	67	6164912.5	19170116	3.53	1	0.01	0.09	0.61	0.22	0.08	0.60	0.21
6616905	49	70	6181892	19174892	3.54	1	0.01	0.17	0.67	0.32	0.15	0.66	0.31
6517416	57	68	6197967	19136210	3.56	1	0.21	0.46	1.37	0.65	0.25	1.16	0.44
BAUS-4251	48	66	6162705.5	19167810	3.56	1	0.01	0.13	0.66	0.25	0.12	0.65	0.23
BAUS-5354	50	64	6158858.5	19151168	3.56	1	0.02	0.23	0.99	0.40	0.22	0.97	0.38
BAUS-5388	57	63	6178570	19121956	3.62	1	0.45	0.67	1.35	0.78	0.22	0.90	0.33
BAUS-4446	56	63	6172414	19122690	3.65	1	0.20	0.36	1.16	0.48	0.16	0.96	0.29
BWLL-5099	50	71	6188851	19175126	3.66	1	0.15	0.43	1.03	0.59	0.27	0.87	0.44
BWLL-4914	48	69	6175618.5	19175966	3.68	1	0.01	0.02	0.42	0.11	0.00	0.40	0.10
BAUS-4103	48	66	6162497.5	19168714	3.70	1	0.01	0.13	0.66	0.25	0.12	0.65	0.23
BAUS-4482	48	65	6159595	19163650	3.70	1	0.01	0.08	0.54	0.18	0.07	0.53	0.17
BWLL-5083	51	72	6196246	19175092	3.72	1	0.62	0.93	1.50	1.11	0.31	0.88	0.49
BAUS-4046	49	65	6158552	19160778	3.74	1	0.01	0.19	0.87	0.33	0.17	0.85	0.31
6517506	57	70	6206333.5	19142652	3.77	1	0.51	0.84	1.55	1.02	0.33	1.04	0.51
BAUS-4330	56	63	6172527	19121986	3.77	1	0.20	0.36	1.16	0.48	0.16	0.96	0.29
BAUS-4499	50	64	6157484	19151120	3.79	1	0.02	0.23	0.99	0.40	0.22	0.97	0.38
BAUS-5172	49	65	6158516.5	19161790	3.79	1	0.01	0.19	0.87	0.33	0.17	0.85	0.31
BAUS-4197	48	69	6172692.5	19176572	3.89	1	0.01	0.02	0.42	0.11	0.00	0.40	0.10
BAUS-5427	48	65	6158124.5	19162332	3.89	1	0.01	0.08	0.54	0.18	0.07	0.53	0.17
BAUS-4554	50	64	6157482.5	19153652	3.90	1	0.02	0.23	0.99	0.40	0.22	0.97	0.38
BAUS-4244	48	69	6172513	19176666	3.92	1	0.01	0.02	0.42	0.11	0.00	0.40	0.10
BAUS-4245	48	69	6172513	19176666	3.92	1	0.01	0.02	0.42	0.11	0.00	0.40	0.10
BAUS-4381	48	65	6157883	19162274	3.93	1	0.01	0.08	0.54	0.18	0.07	0.53	0.17
BAUS-4161	56	63	6173447	19120904	3.93	1	0.20	0.36	1.16	0.48	0.16	0.96	0.29
BAUS-4377	50	64	6156590	19151494	3.97	1	0.02	0.23	0.99	0.40	0.22	0.97	0.38
BWLL-4902	51	72	6196194.5	19176508	3.98	1	0.62	0.93	1.50	1.11	0.31	0.88	0.49
BAUS-4002	49	64	6156882.5	19158188	3.98	1	0.01	0.08	0.58	0.18	0.07	0.56	0.16
BWLL-5712	52	73	6201356	19174950	4.03	1	1.00	1.27	1.75	1.41	0.27	0.75	0.42
BWLL-4901	51	72	6196531.5	19176924	4.07	1	0.62	0.93	1.50	1.11	0.31	0.88	0.49
BAUS-4106	48	69	6173004	19177696	4.09	1	0.01	0.02	0.42	0.11	0.00	0.40	0.10
BAUS-4326	49	64	6156076.5	19158564	4.14	1	0.01	0.08	0.58	0.18	0.07	0.56	0.16
6624105	49	64	6156073.5	19158552	4.14	1	0.01	0.08	0.58	0.18	0.07	0.56	0.16
BAUS-4130	50	63	6154803.5	19149710	4.17	1	0.02	0.09	0.62	0.18	0.08	0.60	0.17
BWLL-4479	54	73	6211756.5	19165026	4.18	1	2.76	3.36	4.51	3.67	0.60	1.75	0.91
BWLL-5046	48	70	6175780.5	19178808	4.21	1	0.01	0.07	0.44	0.18	0.06	0.43	0.17

Table E-9
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 3 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4440	56	62	6169492.5	19120560	4.22	1	0.29	0.46	1.11	0.56	0.17	0.82	0.27
BWLL-5107	50	72	6193152	19178698	4.31	1	0.25	0.46	0.92	0.58	0.21	0.67	0.33
BAUS-4178	50	63	6153445.5	19148244	4.34	1	0.02	0.09	0.62	0.18	0.08	0.60	0.17
6509803	55	73	6213403	19163354	4.36	1	1.35	1.59	2.04	1.72	0.23	0.69	0.36
BWLL-5036	50	72	6193462	19179040	4.37	1	0.25	0.46	0.92	0.58	0.21	0.67	0.33
BAUS-5365	49	64	6154709.5	19158668	4.40	1	0.01	0.08	0.58	0.18	0.07	0.56	0.16
BWLL-4586	50	72	6193187.5	19179334	4.43	1	0.25	0.46	0.92	0.58	0.21	0.67	0.33
BWLL-4957	50	72	6193187.5	19179334	4.43	1	0.25	0.46	0.92	0.58	0.21	0.67	0.33
BAUS-4231	49	64	6154315	19156072	4.46	1	0.01	0.08	0.58	0.18	0.07	0.56	0.16
BAUS-5178	54	61	6159714	19125378	4.47	1	0.02	0.06	0.43	0.12	0.04	0.41	0.10
BAUS-4433	47	68	6164433	19176176	4.48	1	0.01	0.01	0.24	0.01	0.00	0.23	0.00
BAUS-4555	49	64	6154125	19156470	4.49	1	0.01	0.08	0.58	0.18	0.07	0.56	0.16
BAUS-4323	49	64	6153822	19157574	4.55	1	0.01	0.08	0.58	0.18	0.07	0.56	0.16
BAUS-4215	49	64	6153833	19157270	4.55	1	0.01	0.08	0.58	0.18	0.07	0.56	0.16
BWLL-4273	49	72	6190162.5	19180238	4.60	1	0.20	0.37	0.75	0.47	0.17	0.55	0.27
BAUS-4100	47	67	6159614.5	19173068	4.64	1	0.01	0.01	0.20	0.01	0.00	0.19	0.00
BWLL-4020	50	72	6192689	19180938	4.72	1	0.25	0.46	0.92	0.58	0.21	0.67	0.33
BWLL-4510	54	74	6212934	19168918	4.72	1	1.90	2.13	2.58	2.26	0.24	0.69	0.36
BAUS-5408	57	62	6169281	19117216	4.82	1	0.52	0.71	1.28	0.80	0.19	0.76	0.28
BAUS-4331	54	60	6155456.5	19126140	4.96	1	0.17	0.25	0.53	0.30	0.09	0.36	0.13
BAUS-5307	55	61	6161433.5	19120750	4.97	1	0.16	0.27	0.72	0.33	0.11	0.56	0.17
BAUS-4322	49	63	6151606.5	19155470	4.98	1	0.01	0.02	0.40	0.10	0.01	0.38	0.09
BWLL-5404	49	72	6186798.5	19182242	5.05	1	0.20	0.37	0.75	0.47	0.17	0.55	0.27
BWLL-5720	48	70	6177109.5	19183434	5.07	1	0.01	0.07	0.44	0.18	0.06	0.43	0.17
BWLL-4968	52	74	6207057	19177918	5.08	1	1.66	1.92	2.41	2.06	0.27	0.75	0.40
BAUS-4151	47	64	6152060.5	19165106	5.14	1	0.01	0.02	0.25	0.07	0.01	0.24	0.06
BAUS-4240	47	66	6156685	19173776	5.15	1	0.01	0.01	0.27	0.04	0.00	0.26	0.03
BWLL-0046	50	73	6198713	19182270	5.15	1	0.55	0.76	1.14	0.87	0.21	0.59	0.32
BAUS-5332	46	67	6159231	19176600	5.17	1	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BAUS-4095	46	67	6159387	19177010	5.20	1	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BAUS-4361	48	64	6150553	19160396	5.22	1	0.01	0.02	0.34	0.08	0.00	0.33	0.07
BAUS-4252	46	66	6155967.5	19174154	5.30	1	0.01	0.01	0.05	0.01	0.00	0.04	0.00
BAUS-0023	58	62	6177353.5	19112740	5.37	1	0.74	0.91	1.40	0.98	0.16	0.66	0.24
6616701	46	66	6154947.5	19173422	5.37	1	0.01	0.01	0.05	0.01	0.00	0.04	0.00
BWLL-4175	47	70	6175471.5	19184974	5.38	1	0.01	0.01	0.24	0.05	0.00	0.23	0.04
BAUS-4157	55	60	6157945	19120556	5.39	1	0.37	0.45	0.87	0.51	0.08	0.50	0.15
BAUS-4229	52	60	6150139	19129496	5.45	1	0.02	0.03	0.29	0.08	0.02	0.27	0.06
BAUS-5374	47	64	6149640.5	19162492	5.46	1	0.01	0.02	0.25	0.07	0.01	0.24	0.06
BWLL-4391	50	73	6195988	19184602	5.48	1	0.55	0.76	1.14	0.87	0.21	0.59	0.32
BAUS-5320	46	66	6155757.5	19175638	5.51	1	0.01	0.01	0.05	0.01	0.00	0.04	0.00
BWLL-5619	49	73	6190846.5	19185114	5.51	1	0.44	0.61	0.94	0.71	0.18	0.50	0.27
6616408	46	67	6156879.5	19177938	5.66	1	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BAUS-4533	49	61	6145912	19147068	5.70	1	0.01	0.01	0.22	0.05	0.00	0.21	0.04
BAUS-4441	46	66	6154841	19176140	5.71	1	0.01	0.01	0.05	0.01	0.00	0.04	0.00
6517505	59	70	6212777.5	19134288	5.75	1	0.36	0.58	1.12	0.70	0.21	0.75	0.34
BAUS-4312	47	65	6149991	19168882	5.76	1	0.01	0.02	0.30	0.08	0.00	0.29	0.07
BWLL-4388	47	71	6176538	19187140	5.78	1	0.01	0.01	0.23	0.06	0.00	0.22	0.05
BWLL-4841	55	75	6219268	19169050	5.79	1	4.22	4.67	5.52	4.87	0.45	1.30	0.65
BWLL-4199	48	72	6184208.5	19186706	5.81	1	0.05	0.19	0.44	0.27	0.14	0.39	0.21
BWLL-4019	48	72	6188877	19186572	5.81	1	0.05	0.19	0.44	0.27	0.14	0.39	0.21
BWLL-4198	48	72	6184296.5	19186710	5.82	1	0.05	0.19	0.44	0.27	0.14	0.39	0.21
BWLL-4271	54	75	6216897.5	19173622	5.84	1	3.98	4.40	5.20	4.60	0.42	1.21	0.62
BWLL-4668	46	69	6164915.5	19184902	5.88	1	0.01	0.01	0.05	0.01	0.00	0.04	0.00
BAUS-5321	46	66	6155203.5	19177898	5.88	1	0.01	0.01	0.05	0.01	0.00	0.04	0.00
BAUS-4209	47	64	6148873	19168134	5.90	1	0.01	0.02	0.25	0.07	0.01	0.24	0.06
BWLL-4844	54	75	6219097.5	19171272	5.96	1	3.98	4.40	5.20	4.60	0.42	1.21	0.62
BAUS-5366	59	62	6179431	19109360	6.01	1	0.98	1.13	1.58	1.20	0.15	0.59	0.22
BAUS-4284	46	67	6156156.5	19179906	6.02	1	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-4146	47	71	6177018	19188474	6.03	1	0.01	0.01	0.23	0.06	0.00	0.22	0.05
6525104	60	65	6195083.5	19113996	6.05	1	0.55	0.75	1.28	0.84	0.19	0.73	0.29
BAUS-4111	49	62	6145119.5	19152104	6.05	1	0.01	0.02	0.24	0.02	0.00	0.23	0.01
6517806	60	67	6203449.5	19120438	6.10	1	0.30	0.52	1.09	0.63	0.22	0.78	0.33

Table E-9
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 4 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4320	46	67	6155152.5	19179796	6.14	1	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BAUS-5210	46	66	6152520	19177072	6.16	1	0.01	0.01	0.05	0.01	0.00	0.04	0.00
BWLL-5048	50	74	6201355	19187026	6.16	1	0.91	1.07	1.35	1.15	0.16	0.44	0.24
BWLL-5244	47	71	6176659	19189290	6.18	1	0.01	0.01	0.23	0.06	0.00	0.22	0.05
BAUS-4219	47	63	6146183.5	19164496	6.18	1	0.01	0.01	0.20	0.05	0.00	0.19	0.03
BWLL-4997	48	73	6191791	19188702	6.19	1	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BAUS-4179	51	60	6142840	19136634	6.33	1	0.02	0.05	0.28	0.09	0.03	0.26	0.07
BWLL-4481	51	75	6207214	19185620	6.34	1	1.67	1.85	2.19	1.94	0.18	0.52	0.27
BAUS-4501	47	63	6144274	19161188	6.42	1	0.01	0.01	0.20	0.05	0.00	0.19	0.03
BAUS-4546	45	66	6152776	19179814	6.46	1	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BAUS-4096	45	66	6152178.5	19179288	6.48	1	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-4362	53	59	6146703.5	19124416	6.50	1	0.16	0.23	0.44	0.27	0.07	0.28	0.10
BAUS-4194	45	66	6152336.5	19179800	6.52	1	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-5633	46	72	6178922	19191884	6.67	1	0.01	0.01	0.12	0.02	0.00	0.11	0.01
BWLL-5316	48	73	6188437.5	19191416	6.73	1	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-0050	54	76	6221764	19175320	6.78	1	3.00	3.21	3.61	3.31	0.21	0.61	0.31
6517615	59	73	6225327	19143954	6.79	1	1.52	1.67	1.99	1.74	0.15	0.47	0.23
6517612	59	73	6225327	19143954	6.79	1	1.52	1.67	1.99	1.74	0.15	0.47	0.23
BAUS-4058	55	59	6152213	19115596	6.80	1	0.54	0.61	0.94	0.66	0.08	0.40	0.12
BAUS-4317	53	59	6144949.5	19124152	6.81	1	0.16	0.23	0.44	0.27	0.07	0.28	0.10
BWLL-5218	47	73	6186841.5	19191764	6.83	1	0.04	0.13	0.29	0.17	0.09	0.25	0.13
BWLL-0014B	54	76	6222610.5	19174580	6.85	1	3.00	3.21	3.61	3.31	0.21	0.61	0.31
BAUS-4456	53	59	6145351.5	19122748	6.89	1	0.16	0.23	0.44	0.27	0.07	0.28	0.10
BAUS-4329	53	59	6145263	19122744	6.90	1	0.16	0.23	0.44	0.27	0.07	0.28	0.10
BWLL-4529	50	75	6206447	19189744	6.98	1	1.13	1.25	1.47	1.31	0.12	0.34	0.18
BWLL-4524	50	75	6206447	19189744	6.98	1	1.13	1.25	1.47	1.31	0.12	0.34	0.18
6623602	49	60	6138788.5	19144204	6.99	1	0.01	0.06	0.22	0.09	0.05	0.21	0.08
BWLL-5229	48	73	6190403.5	19193006	7.01	1	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-5228	48	73	6190403.5	19193006	7.01	1	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-5230	48	73	6190403.5	19193006	7.01	1	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-5231	48	73	6190403.5	19193006	7.01	1	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-5234	48	73	6190403.5	19193006	7.01	1	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-5235	48	73	6190403.5	19193006	7.01	1	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-5236	48	73	6190403.5	19193006	7.01	1	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-5278	48	73	6190403.5	19193006	7.01	1	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-0056	48	73	6190403.5	19193006	7.01	1	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-4098	46	72	6180351	19193656	7.02	1	0.01	0.01	0.12	0.02	0.00	0.11	0.01
BAUS-4254	48	61	6139071	19148754	7.02	1	0.01	0.07	0.24	0.10	0.06	0.23	0.09
BAUS-4202	45	65	6145386.5	19174694	7.03	1	0.01	0.01	0.01	0.01	0.00	0.00	0.00
6525106	61	65	6198306	19109812	7.05	1	0.93	1.10	1.57	1.18	0.17	0.64	0.25
6616305	46	71	6175255.5	19193866	7.06	1	0.01	0.01	0.07	0.01	0.00	0.06	0.00
BWLL-0001D	54	76	6224553	19173702	7.08	1	3.00	3.21	3.61	3.31	0.21	0.61	0.31
BWLL-5560	50	76	6207148	19189986	7.08	1	1.51	1.62	1.82	1.67	0.11	0.31	0.16
BWLL-5583	50	76	6207148	19189986	7.08	1	1.51	1.62	1.82	1.67	0.11	0.31	0.16
BWLL-5705	50	76	6207148	19189986	7.08	1	1.51	1.62	1.82	1.67	0.11	0.31	0.16
BAUS-4287	48	61	6139321	19151700	7.09	1	0.01	0.07	0.24	0.10	0.06	0.23	0.09
BWLL-5093	50	76	6206153.5	19190542	7.10	1	1.51	1.62	1.82	1.67	0.11	0.31	0.16
BWLL-4001	50	76	6206776	19190364	7.11	1	1.51	1.62	1.82	1.67	0.11	0.31	0.16
BWLL-5523	49	75	6202579.5	19192032	7.13	1	0.86	0.96	1.15	1.01	0.10	0.29	0.16
BWLL-4387	46	71	6173820.5	19194232	7.15	1	0.01	0.01	0.07	0.01	0.00	0.06	0.00
BWLL-5260	49	75	6202931	19192046	7.15	1	0.86	0.96	1.15	1.01	0.10	0.29	0.16
BWLL-4427	47	73	6189667.5	19193892	7.18	1	0.04	0.13	0.29	0.17	0.09	0.25	0.13
BWLL-5047	49	75	6203183.5	19192358	7.22	1	0.86	0.96	1.15	1.01	0.10	0.29	0.16
BAUS-4164	54	58	6147398	19117150	7.23	1	0.38	0.43	0.65	0.45	0.05	0.28	0.08
BAUS-4369	49	60	6137283	19144440	7.28	1	0.01	0.06	0.22	0.09	0.05	0.21	0.08
BWLL-4753	54	77	6223802.5	19177320	7.31	1	3.14	3.30	3.65	3.38	0.16	0.51	0.24
BWLL-4655	49	75	6202275.5	19193136	7.32	1	0.86	0.96	1.15	1.01	0.10	0.29	0.16
BAUS-4313	48	60	6137047.5	19146152	7.34	1	0.01	0.06	0.20	0.09	0.05	0.19	0.07
BWLL-4599	49	75	6202890.5	19193158	7.35	1	0.86	0.96	1.15	1.01	0.10	0.29	0.16
BWLL-4656	49	75	6201913	19193426	7.35	1	0.86	0.96	1.15	1.01	0.10	0.29	0.16
BAUS-5288	54	58	6148317	19114972	7.39	1	0.38	0.43	0.65	0.45	0.05	0.28	0.08
BAUS-4078	48	61	6137790.5	19152660	7.42	1	0.01	0.07	0.24	0.10	0.06	0.23	0.09

Table E-9
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 5 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BWLL-4660	49	75	6202868	19193764	7.46	1	0.86	0.96	1.15	1.01	0.10	0.29	0.16
BWLL-4227	53	77	6222451.5	19180512	7.46	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4113	53	77	6222902.5	19180224	7.50	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4304	53	77	6222433	19181016	7.52	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4181	53	77	6222891	19180528	7.53	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-5210	49	75	6202498.5	19194258	7.53	1	0.86	0.96	1.15	1.01	0.10	0.29	0.16
BWLL-4297	45	71	6169373.5	19195592	7.54	1	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-4405	54	77	6224743	19178064	7.54	1	3.14	3.30	3.65	3.38	0.16	0.51	0.24
BAUS-4066	47	62	6138023	19158642	7.55	1	0.01	0.01	0.12	0.01	0.00	0.11	0.00
BWLL-4265	53	77	6222608.5	19181024	7.55	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4570	53	77	6223437	19180042	7.55	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BAUS-4075	47	62	6138002	19159248	7.56	1	0.01	0.01	0.12	0.01	0.00	0.11	0.00
BAUS-4297	46	72	6178346	19196654	7.57	1	0.01	0.01	0.12	0.02	0.00	0.11	0.01
BWLL-4590	49	75	6202934	19194374	7.58	1	0.86	0.96	1.15	1.01	0.10	0.29	0.16
BAUS-4230	47	61	6136978	19153238	7.59	1	0.01	0.02	0.15	0.05	0.01	0.14	0.04
BWLL-4127	53	77	6223052	19180938	7.60	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4299	54	77	6225373.5	19177684	7.60	1	3.14	3.30	3.65	3.38	0.16	0.51	0.24
BWLL-4114	53	77	6222864.5	19181236	7.61	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-5339	53	77	6222956.5	19181138	7.61	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4128	53	77	6223876.5	19180058	7.62	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4017	53	77	6224063.5	19179760	7.62	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4014	53	77	6223972	19179858	7.62	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
6510715	57	76	6231432	19161984	7.63	1	2.98	3.16	3.56	3.24	0.17	0.57	0.26
BWLL-4264	53	77	6223319	19180848	7.63	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4262	54	77	6225736	19177392	7.63	1	3.14	3.30	3.65	3.38	0.16	0.51	0.24
6517614	60	73	6228549	19139770	7.65	1	1.39	1.53	1.81	1.59	0.13	0.42	0.20
BWLL-4308	53	77	6224144	19179966	7.65	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BAUS-4472	48	60	6135298.5	19145788	7.67	1	0.01	0.06	0.20	0.09	0.05	0.19	0.07
BWLL-4614	49	75	6202556.5	19195070	7.68	1	0.86	0.96	1.15	1.01	0.10	0.29	0.16
BWLL-4180	53	77	6224041	19180368	7.68	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4294	53	77	6223671	19180860	7.68	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BAUS-5154	47	62	6137316	19158718	7.69	1	0.01	0.01	0.12	0.01	0.00	0.11	0.00
BWLL-4058	53	77	6224133	19180270	7.69	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4266	54	77	6224686.5	19179582	7.69	1	3.14	3.30	3.65	3.38	0.16	0.51	0.24
BWLL-4179	53	77	6224030	19180672	7.72	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4034	54	77	6224862.5	19179588	7.72	1	3.14	3.30	3.65	3.38	0.16	0.51	0.24
BWLL-5165	49	76	6202725	19195278	7.73	1	1.16	1.24	1.38	1.27	0.08	0.22	0.11
BWLL-4225	54	77	6224847	19179992	7.76	1	3.14	3.30	3.65	3.38	0.16	0.51	0.24
BWLL-4279	53	77	6224477	19180486	7.76	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4380	53	77	6223831.5	19181272	7.76	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4566	53	77	6223831.5	19181272	7.76	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4797	55	77	6227917.5	19175550	7.81	1	3.40	3.54	3.87	3.61	0.14	0.47	0.21
BWLL-4916	53	77	6224271	19181288	7.82	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-5324	47	73	6186384	19197114	7.83	1	0.04	0.13	0.29	0.17	0.09	0.25	0.13
BWLL-4990	52	77	6218864.5	19187062	7.83	1	4.36	4.61	5.08	4.72	0.26	0.72	0.36
BWLL-4018	54	77	6225195	19180106	7.83	1	3.14	3.30	3.65	3.38	0.16	0.51	0.24
BWLL-4359	53	77	6224450.5	19181194	7.84	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4226	54	77	6225096	19180408	7.85	1	3.14	3.30	3.65	3.38	0.16	0.51	0.24
BWLL-4016	53	77	6224813.5	19180902	7.86	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4059	54	77	6225271.5	19180414	7.88	1	3.14	3.30	3.65	3.38	0.16	0.51	0.24
BWLL-4060	54	77	6225271.5	19180414	7.88	1	3.14	3.30	3.65	3.38	0.16	0.51	0.24
BWLL-0014A	55	77	6229109.5	19174278	7.90	1	3.40	3.54	3.87	3.61	0.14	0.47	0.21
BAUS-5159	47	61	6136060	19156852	7.91	1	0.01	0.02	0.15	0.05	0.01	0.14	0.04
BAUS-4356	49	59	6133777	19141382	7.94	1	0.06	0.11	0.23	0.13	0.05	0.17	0.07
BWLL-4088	54	77	6225898	19180134	7.94	1	3.14	3.30	3.65	3.38	0.16	0.51	0.24
BWLL-4447	53	77	6225241.5	19181222	7.96	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4126	53	77	6225329.5	19181226	7.98	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4407	53	77	6225604.5	19180932	7.98	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4282	54	77	6226062.5	19180444	8.00	1	3.14	3.30	3.65	3.38	0.16	0.51	0.24
6525105	62	65	6201528	19105630	8.04	1	1.08	1.23	1.62	1.29	0.14	0.53	0.21
BWLL-4228	53	77	6225853	19181346	8.07	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32
BWLL-4012	53	77	6226028.5	19181354	8.10	1	4.01	4.23	4.65	4.32	0.22	0.65	0.32

Table E-9
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 6 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4394	44	64	6139451.5	19175804	8.13	1	0.01	0.01	0.08	0.01	0.00	0.08	0.01
6518103	58	76	6234654	19157800	8.16	1	3.15	3.30	3.67	3.38	0.16	0.52	0.24
6518406	60	74	6232732	19142992	8.17	1	2.98	3.18	3.61	3.27	0.21	0.64	0.30
BAUS-5433	45	63	6137554	19171998	8.17	1	0.14	0.19	0.30	0.21	0.05	0.16	0.07
BWLL-4482	48	76	6202617.5	19198212	8.26	1	0.82	0.89	1.01	0.92	0.07	0.19	0.10
BAUS-5362	44	64	6139628	19178494	8.34	1	0.01	0.01	0.08	0.01	0.00	0.08	0.01
BAUS-4308	44	64	6137869	19175750	8.39	1	0.01	0.01	0.08	0.01	0.00	0.08	0.01
6615902	45	63	6136149	19171854	8.40	1	0.14	0.19	0.30	0.21	0.05	0.16	0.07
6509106	46	74	6188481	19200322	8.41	1	0.06	0.12	0.21	0.14	0.05	0.15	0.08
BWLL-5718	56	77	6233042.5	19172732	8.46	1	3.01	3.15	3.47	3.21	0.14	0.46	0.19
BWLL-4263	54	78	6229601	19179968	8.51	1	3.16	3.26	3.51	3.30	0.10	0.36	0.14
BAUS-4228	48	58	6129578	19140528	8.74	1	0.13	0.16	0.25	0.18	0.03	0.12	0.05
BAUS-4544	45	62	6133072	19169406	8.82	1	0.07	0.11	0.21	0.13	0.04	0.14	0.06
BWLL-4969	45	73	6182724.5	19203464	8.91	1	0.01	0.01	0.02	0.01	0.00	0.01	0.00
6518404	61	74	6235954	19138808	9.01	1	2.88	3.13	3.66	3.23	0.25	0.78	0.35
BAUS-4319	46	60	6129618	19154706	9.01	1	0.10	0.13	0.21	0.14	0.03	0.12	0.05
6518403	61	74	6235954	19138808	9.01	1	2.88	3.13	3.66	3.23	0.25	0.78	0.35
6525209	63	66	6208933	19104668	9.03	1	1.08	1.21	1.56	1.27	0.13	0.48	0.19
6525218	63	66	6208933	19104668	9.03	1	1.08	1.21	1.56	1.27	0.13	0.48	0.19
6525219	63	66	6208933	19104668	9.03	1	1.08	1.21	1.56	1.27	0.13	0.48	0.19
6525220	63	65	6204749.5	19101448	9.04	1	1.29	1.42	1.75	1.47	0.13	0.46	0.18
6525221	63	65	6204749.5	19101448	9.04	1	1.29	1.42	1.75	1.47	0.13	0.46	0.18
6525210	63	65	6204749.5	19101448	9.04	1	1.29	1.42	1.75	1.47	0.13	0.46	0.18
BAUS-4072	45	62	6131531.5	19168138	9.04	1	0.07	0.11	0.21	0.13	0.04	0.14	0.06
BAUS-4131	48	58	6128001.5	19140272	9.04	1	0.13	0.16	0.25	0.18	0.03	0.12	0.05
6525202	63	67	6213116	19107890	9.08	1	0.90	1.03	1.38	1.09	0.13	0.48	0.19
6525203	63	67	6213116	19107890	9.08	1	0.90	1.03	1.38	1.09	0.13	0.48	0.19
BAUS-4291	45	61	6130616.5	19166588	9.14	1	0.02	0.05	0.13	0.07	0.03	0.12	0.05
BWLL-5331	46	74	6188675.5	19204286	9.16	1	0.06	0.12	0.21	0.14	0.05	0.15	0.08
BAUS-4217	45	61	6130444.5	19166480	9.17	1	0.02	0.05	0.13	0.07	0.03	0.12	0.05
BAUS-4305	45	61	6130444.5	19166480	9.17	1	0.02	0.05	0.13	0.07	0.03	0.12	0.05
BAUS-4218	45	61	6130444.5	19166480	9.17	1	0.02	0.05	0.13	0.07	0.03	0.12	0.05
BAUS-4195	45	61	6130275.5	19166272	9.19	1	0.02	0.05	0.13	0.07	0.03	0.12	0.05
BWLL-4511	53	79	6228988.5	19186932	9.19	1	2.27	2.29	2.34	2.30	0.02	0.08	0.03
BAUS-5306	45	61	6130250.5	19166582	9.21	1	0.02	0.05	0.13	0.07	0.03	0.12	0.05
BAUS-5377	45	61	6130250.5	19166582	9.21	1	0.02	0.05	0.13	0.07	0.03	0.12	0.05
BAUS-4532	48	58	6127012.5	19140844	9.22	1	0.13	0.16	0.25	0.18	0.03	0.12	0.05
6525301	63	68	6217299	19111112	9.23	1	0.17	0.27	0.61	0.33	0.11	0.44	0.16
BAUS-5181	45	61	6130085.5	19166670	9.24	1	0.02	0.05	0.13	0.07	0.03	0.12	0.05
BAUS-4463	45	61	6129853.5	19165750	9.25	1	0.02	0.05	0.13	0.07	0.03	0.12	0.05
BWLL-5038	52	79	6226942.5	19189894	9.27	1	3.14	3.18	3.29	3.20	0.04	0.16	0.06
BAUS-5371	45	61	6129745	19166062	9.28	1	0.02	0.05	0.13	0.07	0.03	0.12	0.05
BWLL-4560	52	79	6225465	19191764	9.33	1	3.14	3.18	3.29	3.20	0.04	0.16	0.06
BWLL-5368	53	79	6229497	19187458	9.33	1	2.27	2.29	2.34	2.30	0.02	0.08	0.03
BAUS-5439	45	61	6129458.5	19166208	9.34	1	0.02	0.05	0.13	0.07	0.03	0.12	0.05
BAUS-4166	44	62	6129924.5	19168790	9.36	1	0.01	0.04	0.11	0.05	0.03	0.10	0.04
BWLL-5377	52	79	6225996	19191682	9.38	1	3.14	3.18	3.29	3.20	0.04	0.16	0.06
BWLL-4212	46	75	6189681.5	19205640	9.41	1	0.18	0.22	0.30	0.24	0.04	0.12	0.06
BAUS-4363	46	60	6127131	19155328	9.50	1	0.10	0.13	0.21	0.14	0.03	0.12	0.05
BAUS-4037	48	58	6125454	19142614	9.51	1	0.13	0.16	0.25	0.18	0.03	0.12	0.05
BWLL-4239	55	79	6237373	19176916	9.53	1	5.48	5.49	5.52	5.49	0.01	0.04	0.00
BWLL-4562	52	79	6227130.5	19191926	9.57	1	3.14	3.18	3.29	3.20	0.04	0.16	0.06
BWLL-4898	53	79	6232263	19186448	9.62	1	2.27	2.29	2.34	2.30	0.02	0.08	0.03
BWLL-5566	52	79	6227068	19192974	9.70	1	3.14	3.18	3.29	3.20	0.04	0.16	0.06
6623205	45	60	6126611.5	19158036	9.71	1	0.04	0.07	0.14	0.08	0.03	0.09	0.04
BWLL-5656	53	79	6232524.5	19187068	9.73	1	2.27	2.29	2.34	2.30	0.02	0.08	0.03
BWLL-5063	51	79	6224348	19195772	9.76	1	2.98	3.02	3.11	3.03	0.04	0.13	0.06
BWLL-5602	52	79	6228469	19192130	9.78	1	3.14	3.18	3.29	3.20	0.04	0.16	0.06
BWLL-5148	50	79	6221156.5	19198794	9.85	1	5.22	5.33	5.59	5.37	0.12	0.38	0.16
BAUS-5364	48	57	6123778	19139626	9.85	1	0.28	0.31	0.37	0.32	0.02	0.09	0.03
BWLL-5655	53	79	6233317.5	19187106	9.85	1	2.27	2.29	2.34	2.30	0.02	0.08	0.03
BWLL-5657	53	79	6233273	19187104	9.85	1	2.27	2.29	2.34	2.30	0.02	0.08	0.03

Table E-9
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - GAM
Page 7 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BWLL-5658	53	79	6233273	19187104	9.85	1	2.27	2.29	2.34	2.30	0.02	0.08	0.03
6510813	58	78	6243020.5	19164244	9.86	1	4.53	4.55	4.63	4.53	0.02	0.10	0.01
6510814	58	78	6243020.5	19164244	9.86	1	4.53	4.55	4.63	4.53	0.02	0.10	0.01
BWLL-4662	50	79	6221947	19198822	9.94	1	5.22	5.33	5.59	5.37	0.12	0.38	0.16
BWLL-4276	50	79	6221947	19198822	9.94	1	5.22	5.33	5.59	5.37	0.12	0.38	0.16
BWLL-5605	43	73	6173644.5	19209052	9.95	1	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BAUS-4189	43	62	6127509.5	19172454	9.99	1	0.00	0.01	0.04	0.01	0.00	0.04	0.00

Table E-10
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 1 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-5429	54	66	6180054.5	19142336	0.15	1	0.49	1.07	3.59	1.42	0.58	3.10	0.93
BAUS-5430	54	66	6180054.5	19142336	0.15	1	0.49	1.07	3.59	1.42	0.58	3.10	0.93
BWLL-5117	53	69	6191012.5	19154344	0.34	1	0.74	2.08	4.21	2.92	1.34	3.47	2.17
BWLL-5481	53	70	6191500	19157906	0.36	1	1.15	1.95	3.31	2.43	0.79	2.15	1.28
BWLL-5006	54	69	6190699	19153424	0.46	1	0.88	1.68	3.20	2.18	0.81	2.32	1.30
BAUS-4159	53	66	6177818.5	19144046	0.47	1	0.40	1.13	3.28	1.57	0.73	2.88	1.17
BAUS-4158	53	66	6177811.5	19144248	0.49	1	0.40	1.13	3.28	1.57	0.73	2.88	1.17
BWLL-5541	52	69	6186065.5	19157628	0.5	1	0.65	1.76	3.71	2.45	1.11	3.06	1.80
BWLL-5541	53	69	6188533	19157786	0.54	1	0.74	2.08	4.21	2.92	1.34	3.47	2.17
BWLL-5543	52	69	6186496.5	19157650	0.56	1	0.65	1.76	3.71	2.45	1.11	3.06	1.80
BAUS-4458	51	67	6175604	19159156	0.63	1	0.62	1.54	3.30	2.11	0.92	2.68	1.49
BWLL-4133	51	67	6175182.5	19158636	0.63	1	0.62	1.54	3.30	2.11	0.92	2.68	1.49
BAUS-5436	51	67	6174074	19157298	0.72	1	0.62	1.54	3.30	2.11	0.92	2.68	1.49
BAUS-5447	51	67	6173795	19157412	0.78	1	0.62	1.54	3.30	2.11	0.92	2.68	1.49
BAUS-4340	53	65	6171277.5	19142192	0.84	1	0.35	0.88	2.95	1.20	0.53	2.60	0.85
BWLL-4363	52	69	6186773	19159558	0.88	1	0.65	1.76	3.71	2.45	1.11	3.06	1.80
BAUS-5426	51	67	6173430.5	19159360	0.98	1	0.62	1.54	3.30	2.11	0.92	2.68	1.49
BAUS-5401	51	67	6172709	19157480	0.99	1	0.62	1.54	3.30	2.11	0.92	2.68	1.49
BAUS-5398	51	66	6171645	19154492	1.25	1	0.80	1.47	2.95	1.88	0.68	2.15	1.09
BAUS-4236	50	67	6173220	19161806	1.31	1	0.71	1.33	2.57	1.71	0.62	1.86	1.00
6517415	55	67	6187339.5	19141354	1.34	1	0.74	1.28	2.77	1.60	0.54	2.03	0.85
BAUS-4485	50	67	6172028.5	19160648	1.34	1	0.71	1.33	2.57	1.71	0.62	1.86	1.00
BAUS-4325	50	67	6172780	19161790	1.36	1	0.71	1.33	2.57	1.71	0.62	1.86	1.00
BAUS-4518	50	68	6174657	19163476	1.42	1	0.48	1.13	2.36	1.51	0.64	1.88	1.03
BAUS-5298	50	67	6172278	19161868	1.44	1	0.71	1.33	2.57	1.71	0.62	1.86	1.00
BAUS-4515	51	66	6170610	19153510	1.5	1	0.80	1.47	2.95	1.88	0.68	2.15	1.09
BAUS-4519	50	68	6175159	19164204	1.52	1	0.48	1.13	2.36	1.51	0.64	1.88	1.03
BAUS-5397	51	66	6169866.5	19155934	1.52	1	0.80	1.47	2.95	1.88	0.68	2.15	1.09
BAUS-0002A	50	68	6175328	19164412	1.54	1	0.48	1.13	2.36	1.51	0.64	1.88	1.03
BAUS-0002B	50	68	6175328	19164412	1.54	1	0.48	1.13	2.36	1.51	0.64	1.88	1.03
BAUS-5400	50	67	6171322	19161498	1.54	1	0.71	1.33	2.57	1.71	0.62	1.86	1.00
BAUS-5402	50	67	6170748.5	19160828	1.56	1	0.71	1.33	2.57	1.71	0.62	1.86	1.00
BWLL-5690	51	69	6184161	19164328	1.65	1	0.52	1.33	2.79	1.82	0.80	2.27	1.29
BAUS-4430	50	66	6168784	19157800	1.73	1	0.65	1.17	2.30	1.49	0.53	1.65	0.84
BAUS-4185	52	66	6170700	19150982	1.73	1	0.46	1.33	3.30	1.86	0.86	2.84	1.39
BAUS-5399	50	66	6168767	19157550	1.73	1	0.65	1.17	2.30	1.49	0.53	1.65	0.84
BWLL-4303	50	68	6177915	19165922	1.75	1	0.48	1.13	2.36	1.51	0.64	1.88	1.03
6509702	52	71	6193335.5	19165170	1.76	1	1.31	1.83	2.76	2.14	0.51	1.44	0.82
BAUS-4429	50	66	6168601	19157996	1.77	1	0.65	1.17	2.30	1.49	0.53	1.65	0.84
BAUS-5297	50	68	6173472	19165068	1.79	1	0.48	1.13	2.36	1.51	0.64	1.88	1.03
BAUS-4129	55	65	6178444	19131512	1.81	1	0.60	0.99	2.36	1.21	0.39	1.76	0.61
BWLL-4992	50	68	6177988.5	19166330	1.83	1	0.48	1.13	2.36	1.51	0.64	1.88	1.03
BWLL-4272	50	68	6177805.5	19166526	1.87	1	0.48	1.13	2.36	1.51	0.64	1.88	1.03
BAUS-0024	56	65	6179473	19131326	1.87	1	0.88	1.20	2.24	1.38	0.32	1.35	0.50
BWLL-5674	51	69	6184132.5	19165744	1.92	1	0.52	1.33	2.79	1.82	0.80	2.27	1.29
BWLL-4161	50	69	6177699	19167028	1.96	1	0.39	0.93	1.93	1.25	0.53	1.53	0.85
BAUS-4299	50	69	6178487	19167158	1.99	1	0.39	0.93	1.93	1.25	0.53	1.53	0.85
BWLL-5082	51	69	6183630	19166128	1.99	1	0.52	1.33	2.79	1.82	0.80	2.27	1.29
BAUS-4138	51	65	6166124	19148388	2.1	1	0.71	1.18	2.37	1.47	0.48	1.66	0.76
6624203	51	65	6166932	19150042	2.15	1	0.71	1.18	2.37	1.47	0.48	1.66	0.76
BWLL-4134	52	71	6197009.5	19166208	2.19	1	1.31	1.83	2.76	2.14	0.51	1.44	0.82
BAUS-4137	51	65	6165560.5	19149382	2.29	1	0.71	1.18	2.37	1.47	0.48	1.66	0.76
BAUS-5120	50	66	6166456	19161362	2.33	1	0.65	1.17	2.30	1.49	0.53	1.65	0.84
BAUS-4552	49	66	6166768	19162486	2.37	1	0.50	0.87	1.65	1.08	0.37	1.15	0.58
BAUS-4235	49	66	6166764.5	19162588	2.38	1	0.50	0.87	1.65	1.08	0.37	1.15	0.58
BAUS-4324	49	66	6166588.5	19162582	2.41	1	0.50	0.87	1.65	1.08	0.37	1.15	0.58
BAUS-4067	50	65	6165176.5	19155240	2.42	1	0.64	1.05	2.00	1.29	0.41	1.36	0.64
BAUS-5146	56	64	6177989	19128236	2.43	1	0.89	1.16	2.05	1.31	0.27	1.16	0.42
BAUS-4288	49	66	6166412.5	19162576	2.44	1	0.50	0.87	1.65	1.08	0.37	1.15	0.58
BAUS-5437	49	68	6171384	19168042	2.48	1	0.20	0.63	1.49	0.89	0.44	1.29	0.69
BAUS-4309	49	66	6166229.5	19162772	2.49	1	0.50	0.87	1.65	1.08	0.37	1.15	0.58
BAUS-4558	49	66	6166226	19162872	2.5	1	0.50	0.87	1.65	1.08	0.37	1.15	0.58

Table E-10
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 2 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4140	50	65	6164582	19154612	2.54	1	0.64	1.05	2.00	1.29	0.41	1.36	0.64
BAUS-5394	50	65	6164439	19155042	2.56	1	0.64	1.05	2.00	1.29	0.41	1.36	0.64
BAUS-5395C	50	65	6164439	19155042	2.56	1	0.64	1.05	2.00	1.29	0.41	1.36	0.64
BAUS-4321	49	66	6165863.5	19163164	2.58	1	0.50	0.87	1.65	1.08	0.37	1.15	0.58
BAUS-4314	49	66	6165765	19163464	2.63	1	0.50	0.87	1.65	1.08	0.37	1.15	0.58
BAUS-4495	49	66	6165427.5	19163046	2.64	1	0.50	0.87	1.65	1.08	0.37	1.15	0.58
BAUS-4541	49	66	6165427.5	19163046	2.64	1	0.50	0.87	1.65	1.08	0.37	1.15	0.58
6624102	51	64	6161925	19145490	2.65	1	0.66	1.02	1.98	1.23	0.36	1.31	0.56
BAUS-5425	51	65	6164243.5	19152214	2.71	1	0.71	1.18	2.37	1.47	0.48	1.66	0.76
BAUS-5344	49	67	6168874	19168294	2.78	1	0.48	0.92	1.81	1.18	0.44	1.33	0.70
BWLL-4987	53	72	6203934.5	19164638	2.85	1	1.86	2.23	2.92	2.45	0.37	1.06	0.58
BAUS-5251	49	66	6163571	19161666	2.86	1	0.50	0.87	1.65	1.08	0.37	1.15	0.58
BWLL-5574	53	72	6204376	19164880	2.95	1	1.86	2.23	2.92	2.45	0.37	1.06	0.58
BWLL-5666	53	72	6204376	19164880	2.95	1	1.86	2.23	2.92	2.45	0.37	1.06	0.58
BWLL-5671	53	72	6203411.5	19166926	3.05	1	1.86	2.23	2.92	2.45	0.37	1.06	0.58
BAUS-4315	50	65	6162008	19152698	3.09	1	0.64	1.05	2.00	1.29	0.41	1.36	0.64
6517418	57	67	6193783.5	19132988	3.16	1	1.15	1.48	2.36	1.67	0.33	1.21	0.51
6616810	48	67	6165870	19168340	3.17	1	0.28	0.57	1.16	0.73	0.29	0.89	0.46
BAUS-4001	50	64	6161187.5	19153480	3.21	1	0.55	0.84	1.57	1.01	0.29	1.02	0.46
BWLL-5144	54	72	6208083.5	19161954	3.32	1	2.68	3.11	3.93	3.35	0.43	1.25	0.67
6616808	48	67	6164696	19168372	3.33	1	0.28	0.57	1.16	0.73	0.29	0.89	0.46
BAUS-5369	50	64	6159339.5	19150220	3.4	1	0.55	0.84	1.57	1.01	0.29	1.02	0.46
6616807	48	67	6164759	19169286	3.44	1	0.28	0.57	1.16	0.73	0.29	0.89	0.46
BAUS-4165	50	64	6159584.5	19151498	3.47	1	0.55	0.84	1.57	1.01	0.29	1.02	0.46
BAUS-4332	56	63	6173628.5	19123240	3.49	1	1.13	1.35	2.09	1.48	0.23	0.96	0.35
BWLL-5283	54	73	6206956.5	19166268	3.5	1	2.01	2.22	2.62	2.33	0.21	0.61	0.32
BAUS-4272	49	65	6159772.5	19161124	3.53	1	0.45	0.75	1.43	0.92	0.30	0.99	0.47
BAUS-0025	48	67	6164912.5	19170116	3.53	1	0.28	0.57	1.16	0.73	0.29	0.89	0.46
6616905	49	70	6181892	19174892	3.54	1	0.41	0.75	1.38	0.94	0.33	0.96	0.53
6517416	57	68	6197967	19136210	3.56	1	1.22	1.56	2.40	1.75	0.34	1.18	0.53
BAUS-4251	48	66	6162705.5	19167810	3.56	1	0.36	0.63	1.21	0.78	0.27	0.85	0.43
BAUS-5354	50	64	6158858.5	19151168	3.56	1	0.55	0.84	1.57	1.01	0.29	1.02	0.46
BAUS-5388	57	63	6178570	19121956	3.62	1	1.50	1.69	2.31	1.80	0.20	0.81	0.30
BAUS-4446	56	63	6172414	19122690	3.65	1	1.13	1.35	2.09	1.48	0.23	0.96	0.35
BWLL-5099	50	71	6188851	19175126	3.66	1	0.84	1.19	1.83	1.39	0.35	0.99	0.55
BWLL-4914	48	69	6175618.5	19175966	3.68	1	0.17	0.42	0.99	0.59	0.26	0.82	0.42
BAUS-4103	48	66	6162497.5	19168714	3.7	1	0.36	0.63	1.21	0.78	0.27	0.85	0.43
BAUS-4482	48	65	6159595	19163650	3.7	1	0.31	0.55	1.08	0.68	0.24	0.77	0.37
BWLL-5083	51	72	6196246	19175092	3.72	1	1.48	1.78	2.35	1.96	0.31	0.87	0.48
BAUS-4046	49	65	6158552	19160778	3.74	1	0.45	0.75	1.43	0.92	0.30	0.99	0.47
6517506	57	70	6206333.5	19142652	3.77	1	1.61	1.91	2.58	2.08	0.30	0.98	0.48
BAUS-4330	56	63	6172527	19121986	3.77	1	1.13	1.35	2.09	1.48	0.23	0.96	0.35
BAUS-4499	50	64	6157484	19151120	3.79	1	0.55	0.84	1.57	1.01	0.29	1.02	0.46
BAUS-5172	49	65	6158516.5	19161790	3.79	1	0.45	0.75	1.43	0.92	0.30	0.99	0.47
BAUS-4197	48	69	6172692.5	19176572	3.89	1	0.17	0.42	0.99	0.59	0.26	0.82	0.42
BAUS-5427	48	65	6158124.5	19162332	3.89	1	0.31	0.55	1.08	0.68	0.24	0.77	0.37
BAUS-4554	50	64	6157482.5	19153652	3.9	1	0.55	0.84	1.57	1.01	0.29	1.02	0.46
BAUS-4244	48	69	6172513	19176666	3.92	1	0.17	0.42	0.99	0.59	0.26	0.82	0.42
BAUS-4245	48	69	6172513	19176666	3.92	1	0.17	0.42	0.99	0.59	0.26	0.82	0.42
BAUS-4381	48	65	6157883	19162274	3.93	1	0.31	0.55	1.08	0.68	0.24	0.77	0.37
BAUS-4161	56	63	6173447	19120904	3.93	1	1.13	1.35	2.09	1.48	0.23	0.96	0.35
BAUS-4377	50	64	6156590	19151494	3.97	1	0.55	0.84	1.57	1.01	0.29	1.02	0.46
BWLL-4902	51	72	6196194.5	19176508	3.98	1	1.48	1.78	2.35	1.96	0.31	0.87	0.48
BAUS-4002	49	64	6156882.5	19158188	3.98	1	0.31	0.55	1.12	0.68	0.24	0.81	0.37
BWLL-5712	52	73	6201356	19174950	4.03	1	1.97	2.23	2.72	2.38	0.26	0.76	0.41
BWLL-4901	51	72	6196531.5	19176924	4.07	1	1.48	1.78	2.35	1.96	0.31	0.87	0.48
BAUS-4106	48	69	6173004	19177696	4.09	1	0.17	0.42	0.99	0.59	0.26	0.82	0.42
BAUS-4326	49	64	6156076.5	19158564	4.14	1	0.31	0.55	1.12	0.68	0.24	0.81	0.37
6624105	49	64	6156073.5	19158552	4.14	1	0.31	0.55	1.12	0.68	0.24	0.81	0.37
BAUS-4130	50	63	6154803.5	19149710	4.17	1	0.37	0.60	1.19	0.72	0.23	0.82	0.35
BWLL-4479	54	73	6211756.5	19165026	4.18	1	2.01	2.22	2.62	2.33	0.21	0.61	0.32
BWLL-5046	48	70	6175780.5	19178808	4.21	1	0.33	0.58	1.08	0.73	0.26	0.75	0.40

Table E-10
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 3 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4440	56	62	6169492.5	19120560	4.22	1	1.23	1.42	2.01	1.52	0.19	0.78	0.28
BWLL-5107	50	72	6193152	19178698	4.31	1	0.99	1.26	1.77	1.42	0.28	0.79	0.43
BAUS-4478	50	63	6153445.5	19148244	4.34	1	0.37	0.60	1.19	0.72	0.23	0.82	0.35
6509803	55	73	6213403	19163354	4.36	1	1.29	1.43	1.68	1.50	0.13	0.39	0.20
BWLL-5036	50	72	6193462	19179040	4.37	1	0.99	1.26	1.77	1.42	0.28	0.79	0.43
BAUS-5365	49	64	6154709.5	19158668	4.4	1	0.31	0.55	1.12	0.68	0.24	0.81	0.37
BWLL-4586	50	72	6193187.5	19179334	4.43	1	0.99	1.26	1.77	1.42	0.28	0.79	0.43
BWLL-4957	50	72	6193187.5	19179334	4.43	1	0.99	1.26	1.77	1.42	0.28	0.79	0.43
BAUS-4231	49	64	6154315	19156072	4.46	1	0.31	0.55	1.12	0.68	0.24	0.81	0.37
BAUS-5178	54	61	6159714	19125378	4.47	1	0.43	0.59	1.10	0.68	0.16	0.66	0.24
BAUS-4433	47	68	6164433	19176176	4.48	1	0.10	0.27	0.71	0.39	0.17	0.61	0.29
BAUS-4555	49	64	6154125	19156470	4.49	1	0.31	0.55	1.12	0.68	0.24	0.81	0.37
BAUS-4323	49	64	6153822	19157574	4.55	1	0.31	0.55	1.12	0.68	0.24	0.81	0.37
BAUS-4215	49	64	6153833	19157270	4.55	1	0.31	0.55	1.12	0.68	0.24	0.81	0.37
BWLL-4273	49	72	6190162.5	19180238	4.6	1	0.91	1.14	1.57	1.27	0.23	0.66	0.36
BAUS-4100	47	67	6159614.5	19173068	4.64	1	0.04	0.20	0.64	0.31	0.16	0.59	0.27
BWLL-4020	50	72	6192689	19180938	4.72	1	0.99	1.26	1.77	1.42	0.28	0.79	0.43
BWLL-4510	54	74	6212934	19168918	4.72	1	1.69	1.81	2.06	1.88	0.13	0.38	0.20
BAUS-5408	57	62	6169281	19117216	4.82	1	1.55	1.72	2.25	1.81	0.17	0.69	0.25
BAUS-4331	54	60	6155456.5	19126140	4.96	1	0.74	0.87	1.26	0.93	0.13	0.52	0.19
BAUS-5307	55	61	6161433.5	19120750	4.97	1	0.88	1.04	1.56	1.13	0.16	0.68	0.25
BAUS-4322	49	63	6151606.5	19155470	4.98	1	0.27	0.46	0.95	0.57	0.19	0.68	0.30
BWLL-5404	49	72	6186798.5	19182242	5.05	1	0.91	1.14	1.57	1.27	0.23	0.66	0.36
BWLL-5720	48	70	6177109.5	19183434	5.07	1	0.33	0.58	1.08	0.73	0.26	0.75	0.40
BWLL-4968	52	74	6207057	19177918	5.08	1	1.60	1.73	1.99	1.80	0.14	0.39	0.21
BAUS-4151	47	64	6152060.5	19165106	5.14	1	0.25	0.39	0.73	0.47	0.15	0.48	0.22
BAUS-4240	47	66	6156685	19173776	5.15	1	0.14	0.33	0.77	0.44	0.20	0.63	0.31
BWLL-0046	50	73	6198713	19182270	5.15	1	1.43	1.64	2.04	1.76	0.21	0.61	0.33
BAUS-5332	46	67	6159231	19176600	5.17	1	0.01	0.01	0.22	0.05	0.00	0.20	0.03
BAUS-4095	46	67	6159387	19177010	5.2	1	0.01	0.01	0.22	0.05	0.00	0.20	0.03
BAUS-4361	48	64	6150553	19160396	5.22	1	0.22	0.42	0.88	0.52	0.20	0.66	0.31
BAUS-4252	46	66	6155967.5	19174154	5.3	1	0.02	0.12	0.41	0.18	0.11	0.39	0.16
BAUS-0023	58	62	6177353.5	19112740	5.37	1	1.79	1.94	2.39	2.01	0.15	0.60	0.22
6616701	46	66	6154947.5	19173422	5.37	1	0.02	0.12	0.41	0.18	0.11	0.39	0.16
BWLL-4175	47	70	6175471.5	19184974	5.38	1	0.22	0.40	0.76	0.50	0.18	0.54	0.28
BAUS-4157	55	60	6157945	19120556	5.39	1	1.15	1.28	1.67	1.34	0.13	0.51	0.19
BAUS-4229	52	60	6150139	19129496	5.45	1	0.35	0.47	0.83	0.53	0.12	0.49	0.18
BAUS-5374	47	64	6149640.5	19162492	5.46	1	0.25	0.39	0.73	0.47	0.15	0.48	0.22
BWLL-4391	50	73	6195988	19184602	5.48	1	1.43	1.64	2.04	1.76	0.21	0.61	0.33
BAUS-5320	46	66	6155757.5	19175638	5.51	1	0.02	0.12	0.41	0.18	0.11	0.39	0.16
BWLL-5619	49	73	6190846.5	19185114	5.51	1	1.29	1.47	1.82	1.57	0.18	0.53	0.28
6616408	46	67	6156879.5	19177938	5.66	1	0.01	0.01	0.22	0.05	0.00	0.20	0.03
BAUS-4533	49	61	6145912	19147068	5.7	1	0.27	0.38	0.69	0.44	0.11	0.42	0.17
BAUS-4441	46	66	6154841	19176140	5.71	1	0.02	0.12	0.41	0.18	0.11	0.39	0.16
6517505	59	70	6212777.5	19134288	5.75	1	1.58	1.81	2.34	1.93	0.23	0.76	0.35
BAUS-4312	47	65	6149991	19168882	5.76	1	0.23	0.40	0.78	0.49	0.17	0.55	0.26
BWLL-4388	47	71	6176538	19187140	5.78	1	0.30	0.48	0.81	0.57	0.17	0.51	0.27
BWLL-4841	55	75	6219268	19169050	5.79	1	1.66	1.76	1.96	1.82	0.10	0.31	0.16
BWLL-4199	48	72	6184208.5	19186706	5.81	1	0.67	0.86	1.21	0.96	0.19	0.55	0.29
BWLL-4019	48	72	6188877	19186572	5.81	1	0.67	0.86	1.21	0.96	0.19	0.55	0.29
BWLL-4198	48	72	6184296.5	19186710	5.82	1	0.67	0.86	1.21	0.96	0.19	0.55	0.29
BWLL-4271	54	75	6216897.5	19173622	5.84	1	1.37	1.46	1.61	1.50	0.08	0.24	0.12
BWLL-4668	46	69	6164915.5	19184902	5.88	1	0.05	0.16	0.43	0.22	0.11	0.38	0.18
BAUS-5321	46	66	6155203.5	19177898	5.88	1	0.02	0.12	0.41	0.18	0.11	0.39	0.16
BAUS-4209	47	64	6148873	19168134	5.9	1	0.25	0.39	0.73	0.47	0.15	0.48	0.22
BWLL-4844	54	75	6219097.5	19171272	5.96	1	1.37	1.46	1.61	1.50	0.08	0.24	0.12
BAUS-5366	59	62	6179431	19109360	6.01	1	2.08	2.22	2.62	2.28	0.14	0.54	0.20
BAUS-4284	46	67	6156156.5	19179906	6.02	1	0.01	0.01	0.22	0.05	0.00	0.20	0.03
BWLL-4146	47	71	6177018	19188474	6.03	1	0.30	0.48	0.81	0.57	0.17	0.51	0.27
6525104	60	65	6195083.5	19113996	6.05	1	1.76	1.94	2.43	2.02	0.18	0.67	0.27
BAUS-4111	49	62	6145119.5	19152104	6.05	1	0.19	0.35	0.75	0.43	0.15	0.55	0.23
6517806	60	67	6203449.5	19120438	6.1	1	1.56	1.76	2.29	1.87	0.21	0.74	0.31

Table E-10
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 4 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4320	46	67	6155152.5	19179796	6.14	1	0.01	0.01	0.22	0.05	0.00	0.20	0.03
BAUS-5210	46	66	6152520	19177072	6.16	1	0.02	0.12	0.41	0.18	0.11	0.39	0.16
BWLL-5048	50	74	6201355	19187026	6.16	1	1.81	1.98	2.28	2.06	0.16	0.47	0.25
BWLL-5244	47	71	6176659	19189290	6.18	1	0.30	0.48	0.81	0.57	0.17	0.51	0.27
BAUS-4219	47	63	6146183.5	19164496	6.18	1	0.23	0.35	0.63	0.41	0.12	0.40	0.18
BWLL-4997	48	73	6191791	19188702	6.19	1	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BAUS-4179	51	60	6142840	19136634	6.33	1	0.37	0.48	0.81	0.54	0.11	0.44	0.17
BWLL-4481	51	75	6207214	19185620	6.34	1	1.73	1.84	2.04	1.89	0.11	0.31	0.16
BAUS-4501	47	63	6144274	19161188	6.42	1	0.23	0.35	0.63	0.41	0.12	0.40	0.18
BAUS-4546	45	66	6152776	19179814	6.46	1	0.01	0.01	0.09	0.01	0.00	0.08	0.00
BAUS-4096	45	66	6152178.5	19179288	6.48	1	0.01	0.01	0.09	0.01	0.00	0.08	0.00
BWLL-4362	53	59	6146703.5	19124416	6.5	1	0.69	0.79	1.10	0.84	0.10	0.41	0.15
BAUS-4194	45	66	6152336.5	19179800	6.52	1	0.01	0.01	0.09	0.01	0.00	0.08	0.00
BWLL-5633	46	72	6178922	19191884	6.67	1	0.34	0.45	0.67	0.51	0.11	0.33	0.17
BWLL-5316	48	73	6188437.5	19191416	6.73	1	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-0050	54	76	6221764	19175320	6.78	1	1.78	1.86	2.03	1.91	0.08	0.25	0.13
6517615	59	73	6225327	19143954	6.79	1	1.90	2.01	2.25	2.06	0.11	0.35	0.17
6517612	59	73	6225327	19143954	6.79	1	1.90	2.01	2.25	2.06	0.11	0.35	0.17
BAUS-4058	55	59	6152213	19115596	6.8	1	1.32	1.42	1.72	1.47	0.10	0.40	0.14
BAUS-4317	53	59	6144949.5	19124152	6.81	1	0.69	0.79	1.10	0.84	0.10	0.41	0.15
BWLL-5218	47	73	6186841.5	19191764	6.83	1	0.65	0.77	1.01	0.84	0.13	0.37	0.19
BWLL-0014B	54	76	6222610.5	19174580	6.85	1	1.78	1.86	2.03	1.91	0.08	0.25	0.13
BAUS-4456	53	59	6145351.5	19122748	6.89	1	0.69	0.79	1.10	0.84	0.10	0.41	0.15
BAUS-4329	53	59	6145263	19122744	6.9	1	0.69	0.79	1.10	0.84	0.10	0.41	0.15
BWLL-4529	50	75	6206447	19189744	6.98	1	1.27	1.35	1.50	1.39	0.08	0.23	0.12
BWLL-4524	50	75	6206447	19189744	6.98	1	1.27	1.35	1.50	1.39	0.08	0.23	0.12
6623602	49	60	6138788.5	19144204	6.99	1	0.37	0.45	0.69	0.50	0.09	0.32	0.13
BWLL-5229	48	73	6190403.5	19193006	7.01	1	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-5228	48	73	6190403.5	19193006	7.01	1	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-5230	48	73	6190403.5	19193006	7.01	1	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-5231	48	73	6190403.5	19193006	7.01	1	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-5234	48	73	6190403.5	19193006	7.01	1	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-5235	48	73	6190403.5	19193006	7.01	1	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-5236	48	73	6190403.5	19193006	7.01	1	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-5278	48	73	6190403.5	19193006	7.01	1	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-0056	48	73	6190403.5	19193006	7.01	1	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-4098	46	72	6180351	19193656	7.02	1	0.34	0.45	0.67	0.51	0.11	0.33	0.17
BAUS-4254	48	61	6139071	19148754	7.02	1	0.37	0.46	0.71	0.51	0.10	0.34	0.14
BAUS-4202	45	65	6145386.5	19174694	7.03	1	0.03	0.10	0.28	0.14	0.07	0.25	0.11
6525106	61	65	6198306	19109812	7.05	1	2.18	2.34	2.78	2.42	0.16	0.60	0.24
6616305	46	71	6175255.5	19193866	7.06	1	0.18	0.29	0.53	0.35	0.11	0.35	0.17
BWLL-0001D	54	76	6224553	19173702	7.08	1	1.78	1.86	2.03	1.91	0.08	0.25	0.13
BWLL-5560	50	76	6207148	19189986	7.08	1	1.26	1.32	1.43	1.35	0.06	0.16	0.08
BWLL-5583	50	76	6207148	19189986	7.08	1	1.26	1.32	1.43	1.35	0.06	0.16	0.08
BWLL-5705	50	76	6207148	19189986	7.08	1	1.26	1.32	1.43	1.35	0.06	0.16	0.08
BAUS-4287	48	61	6139321	19151700	7.09	1	0.37	0.46	0.71	0.51	0.10	0.34	0.14
BWLL-5093	50	76	6206153.5	19190542	7.1	1	1.26	1.32	1.43	1.35	0.06	0.16	0.08
BWLL-4001	50	76	6206776	19190364	7.11	1	1.26	1.32	1.43	1.35	0.06	0.16	0.08
BWLL-5523	49	75	6202579.5	19192032	7.13	1	1.77	1.88	2.10	1.94	0.11	0.33	0.17
BWLL-4387	46	71	6173820.5	19194232	7.15	1	0.18	0.29	0.53	0.35	0.11	0.35	0.17
BWLL-5260	49	75	6202931	19192046	7.15	1	1.77	1.88	2.10	1.94	0.11	0.33	0.17
BWLL-4427	47	73	6189667.5	19193892	7.18	1	0.65	0.77	1.01	0.84	0.13	0.37	0.19
BWLL-5047	49	75	6203183.5	19192358	7.22	1	1.77	1.88	2.10	1.94	0.11	0.33	0.17
BAUS-4164	54	58	6147398	19117150	7.23	1	1.09	1.17	1.42	1.21	0.08	0.33	0.12
BAUS-4369	49	60	6137283	19144440	7.28	1	0.37	0.45	0.69	0.50	0.09	0.32	0.13
BWLL-4753	54	77	6223802.5	19177320	7.31	1	2.06	2.14	2.30	2.18	0.08	0.24	0.12
BWLL-4655	49	75	6202275.5	19193136	7.32	1	1.77	1.88	2.10	1.94	0.11	0.33	0.17
BAUS-4313	48	60	6137047.5	19146152	7.34	1	0.36	0.44	0.65	0.48	0.08	0.28	0.11
BWLL-4599	49	75	6202890.5	19193158	7.35	1	1.77	1.88	2.10	1.94	0.11	0.33	0.17
BWLL-4656	49	75	6201913	19193426	7.35	1	1.77	1.88	2.10	1.94	0.11	0.33	0.17
BAUS-5288	54	58	6148317	19114972	7.39	1	1.09	1.17	1.42	1.21	0.08	0.33	0.12
BAUS-4078	48	61	6137790.5	19152660	7.42	1	0.37	0.46	0.71	0.51	0.10	0.34	0.14

Table E-10
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 5 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BWLL-4660	49	75	6202868	19193764	7.46	1	1.77	1.88	2.10	1.94	0.11	0.33	0.17
BWLL-4227	53	77	6222451.5	19180512	7.46	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4113	53	77	6222902.5	19180224	7.5	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4304	53	77	6222433	19181016	7.52	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4181	53	77	6222891	19180528	7.53	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-5210	49	75	6202498.5	19194258	7.53	1	1.77	1.88	2.10	1.94	0.11	0.33	0.17
BWLL-4297	45	71	6169373.5	19195592	7.54	1	0.11	0.18	0.36	0.22	0.07	0.25	0.11
BWLL-4405	54	77	6224743	19178064	7.54	1	2.06	2.14	2.30	2.18	0.08	0.24	0.12
BAUS-4066	47	62	6138023	19158642	7.55	1	0.18	0.28	0.53	0.33	0.10	0.34	0.15
BWLL-4265	53	77	6222608.5	19181024	7.55	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4570	53	77	6223437	19180042	7.55	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BAUS-4075	47	62	6138002	19159248	7.56	1	0.18	0.28	0.53	0.33	0.10	0.34	0.15
BAUS-4297	46	72	6178346	19196654	7.57	1	0.34	0.45	0.67	0.51	0.11	0.33	0.17
BWLL-4590	49	75	6202934	19194374	7.58	1	1.77	1.88	2.10	1.94	0.11	0.33	0.17
BAUS-4230	47	61	6136978	19153238	7.59	1	0.29	0.37	0.57	0.41	0.08	0.28	0.12
BWLL-4127	53	77	6223052	19180938	7.6	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4299	54	77	6225373.5	19177684	7.6	1	2.06	2.14	2.30	2.18	0.08	0.24	0.12
BWLL-4114	53	77	6222864.5	19181236	7.61	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-5339	53	77	6222956.5	19181138	7.61	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4128	53	77	6223876.5	19180058	7.62	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4017	53	77	6224063.5	19179760	7.62	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4014	53	77	6223972	19179858	7.62	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
6510715	57	76	6231432	19161984	7.63	1	3.22	3.38	3.71	3.46	0.16	0.49	0.24
BWLL-4264	53	77	6223319	19180848	7.63	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4262	54	77	6225736	19177392	7.63	1	2.06	2.14	2.30	2.18	0.08	0.24	0.12
6517614	60	73	6228549	19139770	7.65	1	2.27	2.40	2.69	2.47	0.13	0.42	0.20
BWLL-4308	53	77	6224144	19179966	7.65	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BAUS-4472	48	60	6135298.5	19145788	7.67	1	0.36	0.44	0.65	0.48	0.08	0.28	0.11
BWLL-4614	49	75	6202556.5	19195070	7.68	1	1.77	1.88	2.10	1.94	0.11	0.33	0.17
BWLL-4180	53	77	6224041	19180368	7.68	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4294	53	77	6223671	19180860	7.68	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BAUS-5154	47	62	6137316	19158718	7.69	1	0.18	0.28	0.53	0.33	0.10	0.34	0.15
BWLL-4058	53	77	6224133	19180270	7.69	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4266	54	77	6224686.5	19179582	7.69	1	2.06	2.14	2.30	2.18	0.08	0.24	0.12
BWLL-4179	53	77	6224030	19180672	7.72	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4034	54	77	6224862.5	19179588	7.72	1	2.06	2.14	2.30	2.18	0.08	0.24	0.12
BWLL-5165	49	76	6202725	19195278	7.73	1	0.98	1.03	1.11	1.05	0.04	0.12	0.06
BWLL-4225	54	77	6224847	19179992	7.76	1	2.06	2.14	2.30	2.18	0.08	0.24	0.12
BWLL-4279	53	77	6224477	19180486	7.76	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4380	53	77	6223831.5	19181272	7.76	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4566	53	77	6223831.5	19181272	7.76	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4797	55	77	6227917.5	19175550	7.81	1	1.41	1.45	1.55	1.48	0.05	0.14	0.07
BWLL-4916	53	77	6224271	19181288	7.82	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-5324	47	73	6186384	19197114	7.83	1	0.65	0.77	1.01	0.84	0.13	0.37	0.19
BWLL-4990	52	77	6218864.5	19187062	7.83	1	2.65	2.74	2.92	2.79	0.09	0.27	0.14
BWLL-4018	54	77	6225195	19180106	7.83	1	2.06	2.14	2.30	2.18	0.08	0.24	0.12
BWLL-4359	53	77	6224450.5	19181194	7.84	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4226	54	77	6225096	19180408	7.85	1	2.06	2.14	2.30	2.18	0.08	0.24	0.12
BWLL-4016	53	77	6224813.5	19180902	7.86	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4059	54	77	6225271.5	19180414	7.88	1	2.06	2.14	2.30	2.18	0.08	0.24	0.12
BWLL-4060	54	77	6225271.5	19180414	7.88	1	2.06	2.14	2.30	2.18	0.08	0.24	0.12
BWLL-0014A	55	77	6229109.5	19174278	7.9	1	1.41	1.45	1.55	1.48	0.05	0.14	0.07
BAUS-5159	47	61	6136060	19156852	7.91	1	0.29	0.37	0.57	0.41	0.08	0.28	0.12
BAUS-4356	49	59	6133777	19141382	7.94	1	0.43	0.50	0.69	0.54	0.07	0.26	0.10
BWLL-4088	54	77	6225898	19180134	7.94	1	2.06	2.14	2.30	2.18	0.08	0.24	0.12
BWLL-4447	53	77	6225241.5	19181222	7.96	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4126	53	77	6225329.5	19181226	7.98	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4407	53	77	6225604.5	19180932	7.98	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4282	54	77	6226062.5	19180444	8	1	2.06	2.14	2.30	2.18	0.08	0.24	0.12
6525105	62	65	6201528	19105630	8.04	1	2.30	2.44	2.82	2.51	0.14	0.52	0.20
BWLL-4228	53	77	6225853	19181346	8.07	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13
BWLL-4012	53	77	6226028.5	19181354	8.1	1	2.39	2.47	2.64	2.52	0.09	0.25	0.13

Table E-10
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 6 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BAUS-4394	44	64	6139451.5	19175804	8.13	1	0.23	0.29	0.42	0.32	0.06	0.20	0.09
6518103	58	76	6234654	19157800	8.16	1	2.65	2.76	2.99	2.81	0.11	0.34	0.16
6518406	60	74	6232732	19142992	8.17	1	2.36	2.48	2.75	2.54	0.12	0.39	0.19
BAUS-5433	45	63	6137554	19171998	8.17	1	0.49	0.56	0.72	0.59	0.07	0.24	0.11
BWLL-4482	48	76	6202617.5	19198212	8.26	1	1.57	1.64	1.77	1.67	0.07	0.20	0.10
BAUS-5362	44	64	6139628	19178494	8.34	1	0.23	0.29	0.42	0.32	0.06	0.20	0.09
BAUS-4308	44	64	6137869	19175750	8.39	1	0.23	0.29	0.42	0.32	0.06	0.20	0.09
6615902	45	63	6136149	19171854	8.4	1	0.49	0.56	0.72	0.59	0.07	0.24	0.11
6509106	46	74	6188481	19200322	8.41	1	0.65	0.73	0.89	0.77	0.08	0.23	0.12
BWLL-5718	56	77	6233042.5	19172732	8.46	1	2.82	2.93	3.15	2.98	0.11	0.33	0.16
BWLL-4263	54	78	6229601	19179968	8.51	1	2.15	2.21	2.34	2.24	0.07	0.19	0.10
BAUS-4228	48	58	6129578	19140528	8.74	1	0.49	0.54	0.67	0.56	0.05	0.18	0.07
BAUS-4544	45	62	6133072	19169406	8.82	1	0.44	0.51	0.65	0.53	0.06	0.21	0.09
BWLL-4969	45	73	6182724.5	19203464	8.91	1	0.30	0.37	0.51	0.41	0.07	0.21	0.11
6518404	61	74	6235954	19138808	9.01	1	2.66	2.79	3.07	2.84	0.13	0.41	0.18
BAUS-4319	46	60	6129618	19154706	9.01	1	0.49	0.54	0.67	0.56	0.05	0.18	0.07
6518403	61	74	6235954	19138808	9.01	1	2.66	2.79	3.07	2.84	0.13	0.41	0.18
6525209	63	66	6208933	19104668	9.03	1	2.31	2.45	2.80	2.51	0.14	0.49	0.20
6525218	63	66	6208933	19104668	9.03	1	2.31	2.45	2.80	2.51	0.14	0.49	0.20
6525219	63	66	6208933	19104668	9.03	1	2.31	2.45	2.80	2.51	0.14	0.49	0.20
6525220	63	65	6204749.5	19101448	9.04	1	2.50	2.63	2.97	2.69	0.13	0.46	0.18
6525221	63	65	6204749.5	19101448	9.04	1	2.50	2.63	2.97	2.69	0.13	0.46	0.18
6525210	63	65	6204749.5	19101448	9.04	1	2.50	2.63	2.97	2.69	0.13	0.46	0.18
BAUS-4072	45	62	6131531.5	19168138	9.04	1	0.44	0.51	0.65	0.53	0.06	0.21	0.09
BAUS-4131	48	58	6128001.5	19140272	9.04	1	0.49	0.54	0.67	0.56	0.05	0.18	0.07
6525202	63	67	6213116	19107890	9.08	1	2.15	2.29	2.64	2.35	0.14	0.49	0.20
6525203	63	67	6213116	19107890	9.08	1	2.15	2.29	2.64	2.35	0.14	0.49	0.20
BAUS-4291	45	61	6130616.5	19166588	9.14	1	0.38	0.43	0.56	0.45	0.05	0.18	0.07
BWLL-5331	46	74	6188675.5	19204286	9.16	1	0.65	0.73	0.89	0.77	0.08	0.23	0.12
BAUS-4217	45	61	6130444.5	19166480	9.17	1	0.38	0.43	0.56	0.45	0.05	0.18	0.07
BAUS-4305	45	61	6130444.5	19166480	9.17	1	0.38	0.43	0.56	0.45	0.05	0.18	0.07
BAUS-4218	45	61	6130444.5	19166480	9.17	1	0.38	0.43	0.56	0.45	0.05	0.18	0.07
BAUS-4195	45	61	6130275.5	19166272	9.19	1	0.38	0.43	0.56	0.45	0.05	0.18	0.07
BWLL-4511	53	79	6228988.5	19186932	9.19	1	1.25	1.28	1.34	1.29	0.03	0.08	0.04
BAUS-5306	45	61	6130250.5	19166582	9.21	1	0.38	0.43	0.56	0.45	0.05	0.18	0.07
BAUS-5377	45	61	6130250.5	19166582	9.21	1	0.38	0.43	0.56	0.45	0.05	0.18	0.07
BAUS-4532	48	58	6127012.5	19140844	9.22	1	0.49	0.54	0.67	0.56	0.05	0.18	0.07
6525301	63	68	6217299	19111112	9.23	1	1.44	1.59	1.94	1.65	0.14	0.50	0.21
BAUS-5181	45	61	6130085.5	19166670	9.24	1	0.38	0.43	0.56	0.45	0.05	0.18	0.07
BAUS-4463	45	61	6129853.5	19165750	9.25	1	0.38	0.43	0.56	0.45	0.05	0.18	0.07
BWLL-5038	52	79	6226942.5	19189894	9.27	1	2.11	2.15	2.23	2.17	0.04	0.12	0.06
BAUS-5371	45	61	6129745	19166062	9.28	1	0.38	0.43	0.56	0.45	0.05	0.18	0.07
BWLL-4560	52	79	6225465	19191764	9.33	1	2.11	2.15	2.23	2.17	0.04	0.12	0.06
BWLL-5368	53	79	6229497	19187458	9.33	1	1.25	1.28	1.34	1.29	0.03	0.08	0.04
BAUS-5439	45	61	6129458.5	19166208	9.34	1	0.38	0.43	0.56	0.45	0.05	0.18	0.07
BAUS-4166	44	62	6129924.5	19168790	9.36	1	0.36	0.41	0.52	0.43	0.05	0.16	0.07
BWLL-5377	52	79	6225996	19191682	9.38	1	2.11	2.15	2.23	2.17	0.04	0.12	0.06
BWLL-4212	46	75	6189681.5	19205640	9.41	1	0.85	0.92	1.05	0.95	0.07	0.19	0.10
BAUS-4363	46	60	6127131	19155328	9.5	1	0.49	0.54	0.67	0.56	0.05	0.18	0.07
BAUS-4037	48	58	6125454	19142614	9.51	1	0.49	0.54	0.67	0.56	0.05	0.18	0.07
BWLL-4239	55	79	6237373	19176916	9.53	1	1.75	1.78	1.84	1.79	0.03	0.09	0.04
BWLL-4562	52	79	6227130.5	19191926	9.57	1	2.11	2.15	2.23	2.17	0.04	0.12	0.06
BWLL-4898	53	79	6232263	19186448	9.62	1	1.25	1.28	1.34	1.29	0.03	0.08	0.04
BWLL-5566	52	79	6227068	19192974	9.7	1	2.11	2.15	2.23	2.17	0.04	0.12	0.06
6623205	45	60	6126611.5	19158036	9.71	1	0.42	0.46	0.57	0.48	0.04	0.15	0.06
BWLL-5656	53	79	6232524.5	19187068	9.73	1	1.25	1.28	1.34	1.29	0.03	0.08	0.04
BWLL-5063	51	79	6224348	19195772	9.76	1	2.06	2.10	2.17	2.11	0.04	0.11	0.06
BWLL-5602	52	79	6228469	19192130	9.78	1	2.11	2.15	2.23	2.17	0.04	0.12	0.06
BWLL-5148	50	79	6221156.5	19198794	9.85	1	2.18	2.22	2.29	2.24	0.04	0.12	0.06
BAUS-5364	48	57	6123778	19139626	9.85	1	0.65	0.69	0.79	0.70	0.04	0.14	0.05
BWLL-5655	53	79	6233317.5	19187106	9.85	1	1.25	1.28	1.34	1.29	0.03	0.08	0.04
BWLL-5657	53	79	6233273	19187104	9.85	1	1.25	1.28	1.34	1.29	0.03	0.08	0.04

Table E-10
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Chicot Aquifer (Layer 1) - HAGM
Page 7 of 7

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BWLL-5658	53	79	6233273	19187104	9.85	1	1.25	1.28	1.34	1.29	0.03	0.08	0.04
6510813	58	78	6243020.5	19164244	9.86	1	2.22	2.25	2.29	2.25	0.02	0.07	0.03
6510814	58	78	6243020.5	19164244	9.86	1	2.22	2.25	2.29	2.25	0.02	0.07	0.03
BWLL-4662	50	79	6221947	19198822	9.94	1	2.18	2.22	2.29	2.24	0.04	0.12	0.06
BWLL-4276	50	79	6221947	19198822	9.94	1	2.18	2.22	2.29	2.24	0.04	0.12	0.06
BWLL-5605	43	73	6173644.5	19209052	9.95	1	0.10	0.13	0.19	0.14	0.03	0.09	0.04
BAUS-4189	43	62	6127509.5	19172454	9.99	1	0.30	0.34	0.41	0.35	0.03	0.11	0.05

Table E-11
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Evangeline Aquifer (Layer 2) - GAM
Page 1 of 2

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
6517417	55	69	6195706	19147798	1.74	2	0.21	0.64	1.89	0.98	0.43	1.68	0.77
BWLL-5065	50	69	6182473	19168922	2.48	2	0.02	0.31	1.23	0.57	0.29	1.22	0.56
BWLL-4269	50	69	6182649	19168928	2.49	2	0.02	0.31	1.23	0.57	0.29	1.22	0.56
BWLL-5609	50	70	6183010	19170292	2.76	2	0.02	0.30	1.03	0.51	0.28	1.01	0.50
BAUS-0022B	48	68	6169273	19172252	3.37	2	0.01	0.02	0.41	0.10	0.00	0.40	0.08
BAUS-0022A	48	68	6169273	19172252	3.37	2	0.01	0.02	0.41	0.10	0.00	0.40	0.08
BWLL-0001C	51	72	6197378.5	19173006	3.4	2	0.62	0.93	1.50	1.11	0.31	0.88	0.49
6509704	51	72	6197392	19173010	3.4	2	0.62	0.93	1.50	1.11	0.31	0.88	0.49
BWLL-4555	49	71	6182775.5	19177642	4.08	2	0.05	0.27	0.70	0.39	0.21	0.64	0.34
BWLL-0001A	52	73	6202960	19174426	4.1	2	1.00	1.27	1.75	1.41	0.27	0.75	0.42
BWLL-5067	49	71	6184782.5	19178120	4.26	2	0.05	0.27	0.70	0.39	0.21	0.64	0.34
6624805	56	62	6169529	19119842	4.34	2	0.29	0.46	1.11	0.56	0.17	0.82	0.27
BAUS-0005B	56	61	6168258	19118458	4.68	2	0.39	0.56	1.07	0.64	0.16	0.68	0.24
6624801	57	62	6169900.5	19116538	4.91	2	0.52	0.71	1.28	0.80	0.19	0.76	0.28
BWLL-5211	48	71	6180275.5	19183526	5.11	2	0.01	0.07	0.38	0.17	0.06	0.37	0.15
BWLL-4682	47	70	6173949	19185730	5.55	2	0.01	0.01	0.24	0.05	0.00	0.23	0.04
BWLL-5517	49	73	6190934.5	19185634	5.61	2	0.44	0.61	0.94	0.71	0.18	0.50	0.27
BWLL-00043	54	75	6217397	19172020	5.75	2	3.98	4.40	5.20	4.60	0.42	1.21	0.62
BWLL-4200	48	72	6184472	19186716	5.83	2	0.05	0.19	0.44	0.27	0.14	0.39	0.21
BWLL-4201	48	72	6184556.5	19186820	5.85	2	0.05	0.19	0.44	0.27	0.14	0.39	0.21
BAUS-5057	46	66	6154201	19176826	5.88	2	0.01	0.01	0.05	0.01	0.00	0.04	0.00
BWLL-0007	53	75	6216934	19174876	5.98	2	1.85	2.03	2.37	2.12	0.18	0.52	0.27
BWLL-4535	46	69	6165758	19185944	6	2	0.01	0.01	0.05	0.01	0.00	0.04	0.00
6509403	48	73	6189086	19187984	6.07	2	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-4649	47	71	6177179.5	19188884	6.1	2	0.01	0.01	0.23	0.06	0.00	0.22	0.05
6509404	48	73	6191004	19188382	6.13	2	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-5646	48	73	6188683.5	19188736	6.22	2	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-00049	55	75	6222004.5	19168848	6.25	2	4.22	4.67	5.52	4.87	0.45	1.30	0.65
BAUS-0013A	46	64	6147113	19169048	6.28	2	0.01	0.01	0.17	0.03	0.00	0.16	0.02
BAUS-0013B	46	64	6147113	19169048	6.28	2	0.01	0.01	0.17	0.03	0.00	0.16	0.02
BWLL-4937	45	68	6158954	19184286	6.34	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BAUS-4034	45	67	6154157	19180572	6.37	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-4147	47	72	6183378	19190220	6.44	2	0.01	0.10	0.30	0.16	0.09	0.28	0.14
BWLL-5314	45	68	6162103.5	19187042	6.48	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
6615906	46	63	6144477	19165654	6.55	2	0.01	0.06	0.21	0.09	0.05	0.20	0.08
BWLL-4928	45	68	6159076	19185808	6.56	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BAUS-0007A	45	67	6154188.5	19182116	6.58	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BAUS-0007C	45	67	6154188.5	19182116	6.58	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-0012B	54	76	6222034	19172800	6.58	2	3.00	3.21	3.61	3.31	0.21	0.61	0.31
BWLL-5084	46	71	6178037	19191952	6.68	2	0.01	0.01	0.07	0.01	0.00	0.06	0.00
BWLL-4891	46	71	6176356.5	19192196	6.73	2	0.01	0.01	0.07	0.01	0.00	0.06	0.00
BWLL-4351	48	73	6190630.5	19191596	6.74	2	0.25	0.36	0.59	0.41	0.11	0.34	0.17
BWLL-4166	47	73	6187526	19192294	6.91	2	0.04	0.13	0.29	0.17	0.09	0.25	0.13
BWLL-00058	50	75	6206661	19189554	6.96	2	1.13	1.25	1.47	1.31	0.12	0.34	0.18
BAUS-0003C	45	64	6144379	19171800	6.96	2	0.01	0.01	0.09	0.01	0.00	0.08	0.00
BWLL-4152	46	71	6175947.5	19193802	7.04	2	0.01	0.01	0.07	0.01	0.00	0.06	0.00
BWLL-4302	46	72	6180256	19193856	7.06	2	0.01	0.01	0.12	0.02	0.00	0.11	0.01
BWLL-5713	50	76	6207148	19189986	7.08	2	1.51	1.62	1.82	1.67	0.11	0.31	0.16
BWLL-5382	50	76	6208567	19189518	7.11	2	1.51	1.62	1.82	1.67	0.11	0.31	0.16
BWLL-5648	47	72	6182773	19193958	7.12	2	0.01	0.10	0.30	0.16	0.09	0.28	0.14
BWLL-5649	47	72	6182773	19193958	7.12	2	0.01	0.10	0.30	0.16	0.09	0.28	0.14
6616407	45	67	6152008	19184036	7.13	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-4982	45	71	6171283.5	19193838	7.15	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-5004	47	72	6183327	19194068	7.16	2	0.01	0.10	0.30	0.16	0.09	0.28	0.14
BWLL-4998	45	71	6173553.5	19194324	7.18	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-4485	47	72	6183144	19194264	7.19	2	0.01	0.10	0.30	0.16	0.09	0.28	0.14
BWLL-5598	46	72	6176661.5	19194946	7.25	2	0.01	0.01	0.12	0.02	0.00	0.11	0.01
BWLL-5066	46	72	6176694.5	19195044	7.27	2	0.01	0.01	0.12	0.02	0.00	0.11	0.01
BWLL-5623	45	70	6167395	19193756	7.3	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-5706	45	71	6171943	19195126	7.37	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-4685	45	71	6171848	19195276	7.4	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-4940	45	71	6171936	19195278	7.4	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00

Table E-12
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Evangeline Aquifer (Layer 2) - HAGM
Page 1 of 2

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
6517417	55	69	6195706	19147798	1.74	2	1.14	1.69	2.84	2.02	0.55	1.70	0.88
BWLL-5065	50	69	6182473	19168922	2.48	2	0.39	0.93	1.93	1.25	0.53	1.53	0.85
BWLL-4269	50	69	6182649	19168928	2.49	2	0.39	0.93	1.93	1.25	0.53	1.53	0.85
BWLL-5609	50	70	6183010	19170292	2.76	2	0.52	0.98	1.82	1.24	0.45	1.29	0.72
BAUS-0022B	48	68	6169273	19172252	3.37	2	0.11	0.36	0.94	0.53	0.25	0.84	0.42
BAUS-0022A	48	68	6169273	19172252	3.37	2	0.11	0.36	0.94	0.53	0.25	0.84	0.42
BWLL-0001C	51	72	6197378.5	19173006	3.4	2	1.48	1.78	2.35	1.96	0.31	0.87	0.48
6509704	51	72	6197392	19173010	3.4	2	1.48	1.78	2.35	1.96	0.31	0.87	0.48
BWLL-4555	49	71	6182775.5	19177642	4.08	2	0.66	0.93	1.45	1.09	0.28	0.80	0.43
BWLL-0001A	52	73	6202960	19174426	4.1	2	1.97	2.23	2.72	2.38	0.26	0.76	0.41
BWLL-5067	49	71	6184782.5	19178120	4.26	2	0.66	0.93	1.45	1.09	0.28	0.80	0.43
6624805	56	62	6169529	19119842	4.34	2	1.23	1.42	2.01	1.52	0.19	0.78	0.28
BAUS-0005B	56	61	6168258	19118458	4.68	2	1.32	1.47	1.94	1.54	0.15	0.62	0.23
6624801	57	62	6169900.5	19116538	4.91	2	1.55	1.72	2.25	1.81	0.17	0.69	0.25
BWLL-5211	48	71	6180275.5	19183526	5.11	2	0.40	0.62	1.04	0.74	0.22	0.64	0.34
BWLL-4682	47	70	6173949	19185730	5.55	2	0.22	0.40	0.76	0.50	0.18	0.54	0.28
BWLL-5517	49	73	6190934.5	19185634	5.61	2	1.29	1.47	1.82	1.57	0.18	0.53	0.28
BWLL-00043	54	75	6217397	19172020	5.75	2	1.37	1.46	1.61	1.50	0.08	0.24	0.12
BWLL-4200	48	72	6184472	19186716	5.83	2	0.67	0.86	1.21	0.96	0.19	0.55	0.29
BWLL-4201	48	72	6184556.5	19186820	5.85	2	0.67	0.86	1.21	0.96	0.19	0.55	0.29
BAUS-5057	46	66	6154201	19176826	5.88	2	0.02	0.12	0.41	0.18	0.11	0.39	0.16
BWLL-0007	53	75	6216934	19174876	5.98	2	1.85	1.96	2.18	2.02	0.11	0.33	0.17
BWLL-4535	46	69	6165758	19185944	6	2	0.05	0.16	0.43	0.22	0.11	0.38	0.18
6509403	48	73	6189086	19187984	6.07	2	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-4649	47	71	6177179.5	19188884	6.1	2	0.30	0.48	0.81	0.57	0.17	0.51	0.27
6509404	48	73	6191004	19188382	6.13	2	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-5646	48	73	6188683.5	19188736	6.22	2	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-00049	55	75	6222004.5	19168848	6.25	2	1.66	1.76	1.96	1.82	0.10	0.31	0.16
BAUS-0013A	46	64	6147113	19169048	6.28	2	0.21	0.33	0.59	0.39	0.12	0.38	0.17
BAUS-0013B	46	64	6147113	19169048	6.28	2	0.21	0.33	0.59	0.39	0.12	0.38	0.17
BWLL-4937	45	68	6158954	19184286	6.34	2	0.01	0.01	0.08	0.01	0.00	0.07	0.00
BAUS-4034	45	67	6154157	19180572	6.37	2	0.01	0.01	0.13	0.01	0.00	0.11	0.00
BWLL-4147	47	72	6183378	19190220	6.44	2	0.54	0.70	0.98	0.77	0.15	0.44	0.23
BWLL-5314	45	68	6162103.5	19187042	6.48	2	0.01	0.01	0.08	0.01	0.00	0.07	0.00
6615906	46	63	6144477	19165654	6.55	2	0.31	0.40	0.63	0.45	0.10	0.32	0.14
BWLL-4928	45	68	6159076	19185808	6.56	2	0.01	0.01	0.08	0.01	0.00	0.07	0.00
BAUS-0007A	45	67	6154188.5	19182116	6.58	2	0.01	0.01	0.13	0.01	0.00	0.11	0.00
BAUS-0007C	45	67	6154188.5	19182116	6.58	2	0.01	0.01	0.13	0.01	0.00	0.11	0.00
BWLL-0012B	54	76	6222034	19172800	6.58	2	1.78	1.86	2.03	1.91	0.08	0.25	0.13
BWLL-5084	46	71	6178037	19191952	6.68	2	0.18	0.29	0.53	0.35	0.11	0.35	0.17
BWLL-4891	46	71	6176356.5	19192196	6.73	2	0.18	0.29	0.53	0.35	0.11	0.35	0.17
BWLL-4351	48	73	6190630.5	19191596	6.74	2	0.99	1.14	1.43	1.22	0.15	0.44	0.23
BWLL-4166	47	73	6187526	19192294	6.91	2	0.65	0.77	1.01	0.84	0.13	0.37	0.19
BWLL-0058	50	75	6206661	19189554	6.96	2	1.27	1.35	1.50	1.39	0.08	0.23	0.12
BAUS-0003C	45	64	6144379	19171800	6.96	2	0.18	0.25	0.44	0.29	0.07	0.26	0.11
BWLL-4152	46	71	6175947.5	19193802	7.04	2	0.18	0.29	0.53	0.35	0.11	0.35	0.17
BWLL-4302	46	72	6180256	19193856	7.06	2	0.34	0.45	0.67	0.51	0.11	0.33	0.17
BWLL-5713	50	76	6207148	19189986	7.08	2	1.26	1.32	1.43	1.35	0.06	0.16	0.08
BWLL-5382	50	76	6208567	19189518	7.11	2	1.26	1.32	1.43	1.35	0.06	0.16	0.08
BWLL-5648	47	72	6182773	19193958	7.12	2	0.54	0.70	0.98	0.77	0.15	0.44	0.23
BWLL-5649	47	72	6182773	19193958	7.12	2	0.54	0.70	0.98	0.77	0.15	0.44	0.23
6616407	45	67	6152008	19184036	7.13	2	0.01	0.01	0.13	0.01	0.00	0.11	0.00
BWLL-4982	45	71	6171283.5	19193838	7.15	2	0.11	0.18	0.36	0.22	0.07	0.25	0.11
BWLL-5004	47	72	6183327	19194068	7.16	2	0.54	0.70	0.98	0.77	0.15	0.44	0.23
BWLL-4998	45	71	6173553.5	19194324	7.18	2	0.11	0.18	0.36	0.22	0.07	0.25	0.11
BWLL-4485	47	72	6183144	19194264	7.19	2	0.54	0.70	0.98	0.77	0.15	0.44	0.23
BWLL-5598	46	72	6176661.5	19194946	7.25	2	0.34	0.45	0.67	0.51	0.11	0.33	0.17
BWLL-5066	46	72	6176694.5	19195044	7.27	2	0.34	0.45	0.67	0.51	0.11	0.33	0.17
BWLL-5623	45	70	6167395	19193756	7.3	2	0.02	0.10	0.27	0.14	0.08	0.25	0.12
BWLL-5706	45	71	6171943	19195126	7.37	2	0.11	0.18	0.36	0.22	0.07	0.25	0.11
BWLL-4685	45	71	6171848	19195276	7.4	2	0.11	0.18	0.36	0.22	0.07	0.25	0.11
BWLL-4940	45	71	6171936	19195278	7.4	2	0.11	0.18	0.36	0.22	0.07	0.25	0.11

Table E-12
Simulated Subsidence and Subsidence Due to Electro Purification Pumping
Evangeline Aquifer (Layer 2) - HAGM
Page 2 of 2

Well Number	Model Row	Model Column	X-Coordinate	Y-Coordinate	Distance to Closest EP Well (mi)	Layer	Simulated Subsidence 1891 to 2009 (ft)				Subsidence Due to EP Pumping (ft)		
							Base	Scen 3	Scen 10	Scen 31	Scen 3	Scen 10	Scen 31
BWLL-4941	45	71	6171936	19195278	7.4	2	0.11	0.18	0.36	0.22	0.07	0.25	0.11
BWLL-4164	45	71	6171936	19195278	7.4	2	0.11	0.18	0.36	0.22	0.07	0.25	0.11
BAUS-4296	45	71	6170790	19195340	7.44	2	0.11	0.18	0.36	0.22	0.07	0.25	0.11
BWLL-4096	44	69	6159234.5	19191282	7.44	2	0.01	0.01	0.02	0.01	0.00	0.01	0.00
BWLL-4557	45	71	6170340	19195626	7.51	2	0.11	0.18	0.36	0.22	0.07	0.25	0.11
BWLL-4188	46	72	6180329.5	19196694	7.59	2	0.34	0.45	0.67	0.51	0.11	0.33	0.17
6615905	45	63	6139754.5	19169318	7.6	2	0.49	0.56	0.72	0.59	0.07	0.24	0.11
6510714	57	76	6231432	19161984	7.63	2	3.22	3.38	3.71	3.46	0.16	0.49	0.24
BWLL-5428	45	72	6174327	19197288	7.72	2	0.16	0.22	0.37	0.25	0.06	0.22	0.10
BWLL-4842	44	70	6165153	19195544	7.75	2	0.01	0.01	0.10	0.02	0.00	0.09	0.01
BWLL-5068	45	71	6173269	19197352	7.75	2	0.11	0.18	0.36	0.22	0.07	0.25	0.11
BWLL-4404	45	72	6174839.5	19197712	7.79	2	0.16	0.22	0.37	0.25	0.06	0.22	0.10
BWLL-4145	45	72	6173935.5	19198388	7.94	2	0.16	0.22	0.37	0.25	0.06	0.22	0.10
BWLL-5045	46	73	6183174	19198316	7.95	2	0.50	0.60	0.79	0.65	0.10	0.29	0.15
BWLL-4434	45	72	6173577	19198578	7.98	2	0.16	0.22	0.37	0.25	0.06	0.22	0.10
BWLL-5248	44	69	6157248.5	19193780	8.04	2	0.01	0.01	0.02	0.01	0.00	0.01	0.00
BWLL-4365	45	73	6179715.5	19199102	8.04	2	0.30	0.37	0.51	0.41	0.07	0.21	0.11
BWLL-5255	46	73	6182713	19198906	8.05	2	0.50	0.60	0.79	0.65	0.10	0.29	0.15
BWLL-5143	45	72	6174957.5	19199336	8.1	2	0.16	0.22	0.37	0.25	0.06	0.22	0.10
BWLL-5217	45	72	6172929.5	19199466	8.16	2	0.16	0.22	0.37	0.25	0.06	0.22	0.10
BWLL-5017	45	72	6174939	19199842	8.2	2	0.16	0.22	0.37	0.25	0.06	0.22	0.10
BAUS-4483	44	65	6141571	19180638	8.23	2	0.01	0.06	0.17	0.08	0.05	0.17	0.07
BWLL-4581	45	72	6174000	19199980	8.23	2	0.16	0.22	0.37	0.25	0.06	0.22	0.10
BWLL-5225	45	72	6172915	19199870	8.23	2	0.16	0.22	0.37	0.25	0.06	0.22	0.10
BAUS-0003A	45	63	6136187.5	19171654	8.39	2	0.49	0.56	0.72	0.59	0.07	0.24	0.11
BWLL-4908	45	72	6175953.5	19200992	8.4	2	0.16	0.22	0.37	0.25	0.06	0.22	0.10
6615904	44	63	6136146.5	19171926	8.41	2	0.26	0.32	0.44	0.34	0.05	0.18	0.08
BAUS-4029	43	67	6147313	19190054	8.57	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
6615901	44	63	6135112	19171600	8.57	2	0.26	0.32	0.44	0.34	0.05	0.18	0.08
BWLL-5026	45	73	6177685.5	19203824	8.93	2	0.30	0.37	0.51	0.41	0.07	0.21	0.11
BAUS-4107	43	65	6139922	19185036	8.97	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
6509107	46	74	6189158	19203482	9	2	0.65	0.73	0.89	0.77	0.08	0.23	0.12
BWLL-4522	44	73	6176617	19204560	9.07	2	0.16	0.20	0.28	0.22	0.04	0.12	0.06
6623201	46	60	6129544	19156642	9.12	2	0.49	0.54	0.67	0.56	0.05	0.18	0.07
BWLL-5007	43	70	6158884	19201194	9.17	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BAUS-4557	43	65	6139605.5	19186544	9.19	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-4709	45	74	6183010.5	19205296	9.26	2	0.49	0.55	0.67	0.58	0.06	0.18	0.09
BWLL-5112	44	73	6176844	19205582	9.27	2	0.16	0.20	0.28	0.22	0.04	0.12	0.06
BWLL-4193	44	73	6175768.5	19206150	9.38	2	0.16	0.20	0.28	0.22	0.04	0.12	0.06
BWLL-4531	47	76	6198845	19205162	9.41	2	1.57	1.64	1.76	1.67	0.07	0.19	0.10
BWLL-4347	53	79	6230849	19186596	9.42	2	1.25	1.28	1.34	1.29	0.03	0.08	0.04
BWLL-4320	44	73	6176800.5	19206796	9.5	2	0.16	0.20	0.28	0.22	0.04	0.12	0.06
BWLL-4994	47	76	6198823	19205770	9.52	2	1.57	1.64	1.76	1.67	0.07	0.19	0.10
BWLL-4439	44	73	6176617.5	19206992	9.53	2	0.16	0.20	0.28	0.22	0.04	0.12	0.06
BWLL-5689	46	75	6190976.5	19207002	9.66	2	0.85	0.92	1.05	0.95	0.07	0.19	0.10
BAUS-4170	42	65	6138874.5	19189860	9.7	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BAUS-4174	42	65	6138449	19189440	9.71	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
6509201	47	76	6200188.5	19206618	9.72	2	1.57	1.64	1.76	1.67	0.07	0.19	0.10
BAUS-4177	42	65	6139117	19190476	9.74	2	0.01	0.01	0.01	0.01	0.00	0.00	0.00
BWLL-5709	44	73	6176275.5	19208486	9.82	2	0.16	0.20	0.28	0.22	0.04	0.12	0.06
BWLL-5329	46	76	6193732	19207914	9.84	2	1.19	1.25	1.35	1.27	0.06	0.16	0.08
6518209	58	78	6243020.5	19164244	9.86	2	2.22	2.25	2.29	2.25	0.02	0.07	0.03
BAUS-4050	42	64	6132258.5	19182744	9.95	2	0.06	0.08	0.13	0.09	0.02	0.08	0.03

Appendix E - Subsidence Graphs

Figure Number	Average or Maximum Subsidence	Location	Scenario	Model	Page Number
E1	Average	Austin County	EP Pumping Plus MAG	GAM	1
E2	Average	Austin County	EP Pumping Plus MAG	HAGM	1
E3	Average	Fort Bend County	EP Pumping Plus MAG	GAM	2
E4	Average	Fort Bend County	EP Pumping Plus MAG	HAGM	2
E5	Average	Waller County	EP Pumping Plus MAG	GAM	3
E6	Average	Waller County	EP Pumping Plus MAG	HAGM	3
E7	Average	Project Area	EP Pumping Plus MAG	GAM	4
E8	Average	Project Area	EP Pumping Plus MAG	HAGM	4
E9	Average	Austin County	EP Pumping Within MAG	GAM	5
E10	Average	Austin County	EP Pumping Within MAG	HAGM	5
E11	Average	Fort Bend County	EP Pumping Within MAG	GAM	6
E12	Average	Fort Bend County	EP Pumping Within MAG	HAGM	6
E13	Average	Waller County	EP Pumping Within MAG	GAM	7
E14	Average	Waller County	EP Pumping Within MAG	HAGM	7
E15	Average	Project Area	EP Pumping Within MAG	GAM	8
E16	Average	Project Area	EP Pumping Within MAG	HAGM	8
E17	Average	Austin County	Evangeline/Jasper Scenarios	GAM	9
E18	Average	Austin County	Evangeline/Jasper Scenarios	HAGM	9
E19	Average	Fort Bend County	Evangeline/Jasper Scenarios	GAM	10
E20	Average	Fort Bend County	Evangeline/Jasper Scenarios	HAGM	10
E21	Average	Waller County	Evangeline/Jasper Scenarios	GAM	11
E22	Average	Waller County	Evangeline/Jasper Scenarios	HAGM	11
E23	Average	Project Area	Evangeline/Jasper Scenarios	GAM	12
E24	Average	Project Area	Evangeline/Jasper Scenarios	HAGM	12
E25	Average	Austin County	Conversion Schedule	GAM	13
E26	Average	Austin County	Conversion Schedule	HAGM	13
E27	Average	Fort Bend County	Conversion Schedule	GAM	14
E28	Average	Fort Bend County	Conversion Schedule	HAGM	14
E29	Average	Waller County	Conversion Schedule	GAM	15
E30	Average	Waller County	Conversion Schedule	HAGM	15
E31	Average	Project Area	Conversion Schedule	GAM	16
E32	Average	Project Area	Conversion Schedule	HAGM	16
E33	Maximum	Austin County	EP Pumping Plus MAG	GAM	17
E34	Maximum	Austin County	EP Pumping Plus MAG	HAGM	17
E35	Maximum	Fort Bend County	EP Pumping Plus MAG	GAM	18
E36	Maximum	Fort Bend County	EP Pumping Plus MAG	HAGM	18
E37	Maximum	Waller County	EP Pumping Plus MAG	GAM	19
E38	Maximum	Waller County	EP Pumping Plus MAG	HAGM	19
E39	Maximum	Project Area	EP Pumping Plus MAG	GAM	20
E40	Maximum	Project Area	EP Pumping Plus MAG	HAGM	20
E41	Maximum	Austin County	EP Pumping Within MAG	GAM	21
E42	Maximum	Austin County	EP Pumping Within MAG	HAGM	21
E43	Maximum	Fort Bend County	EP Pumping Within MAG	GAM	22
E44	Maximum	Fort Bend County	EP Pumping Within MAG	HAGM	22
E45	Maximum	Waller County	EP Pumping Within MAG	GAM	23
E46	Maximum	Waller County	EP Pumping Within MAG	HAGM	23
E47	Maximum	Project Area	EP Pumping Within MAG	GAM	24
E48	Maximum	Project Area	EP Pumping Within MAG	HAGM	24
E49	Maximum	Austin County	Evangeline/Jasper Scenarios	GAM	25
E50	Maximum	Austin County	Evangeline/Jasper Scenarios	HAGM	25
E51	Maximum	Fort Bend County	Evangeline/Jasper Scenarios	GAM	26
E52	Maximum	Fort Bend County	Evangeline/Jasper Scenarios	HAGM	26
E53	Maximum	Waller County	Evangeline/Jasper Scenarios	GAM	27
E54	Maximum	Waller County	Evangeline/Jasper Scenarios	HAGM	27
E55	Maximum	Project Area	Evangeline/Jasper Scenarios	GAM	28
E56	Maximum	Project Area	Evangeline/Jasper Scenarios	HAGM	28
E57	Maximum	Austin County	Conversion Schedule	GAM	29
E58	Maximum	Austin County	Conversion Schedule	HAGM	29
E59	Maximum	Fort Bend County	Conversion Schedule	GAM	30
E60	Maximum	Fort Bend County	Conversion Schedule	HAGM	30
E61	Maximum	Waller County	Conversion Schedule	GAM	31
E62	Maximum	Waller County	Conversion Schedule	HAGM	31
E63	Maximum	Project Area	Conversion Schedule	GAM	32
E64	Maximum	Project Area	Conversion Schedule	HAGM	32

Figure E-1
Austin County - Average Subsidence
Electro Purification Pumping in Addition to MAG (GAM)

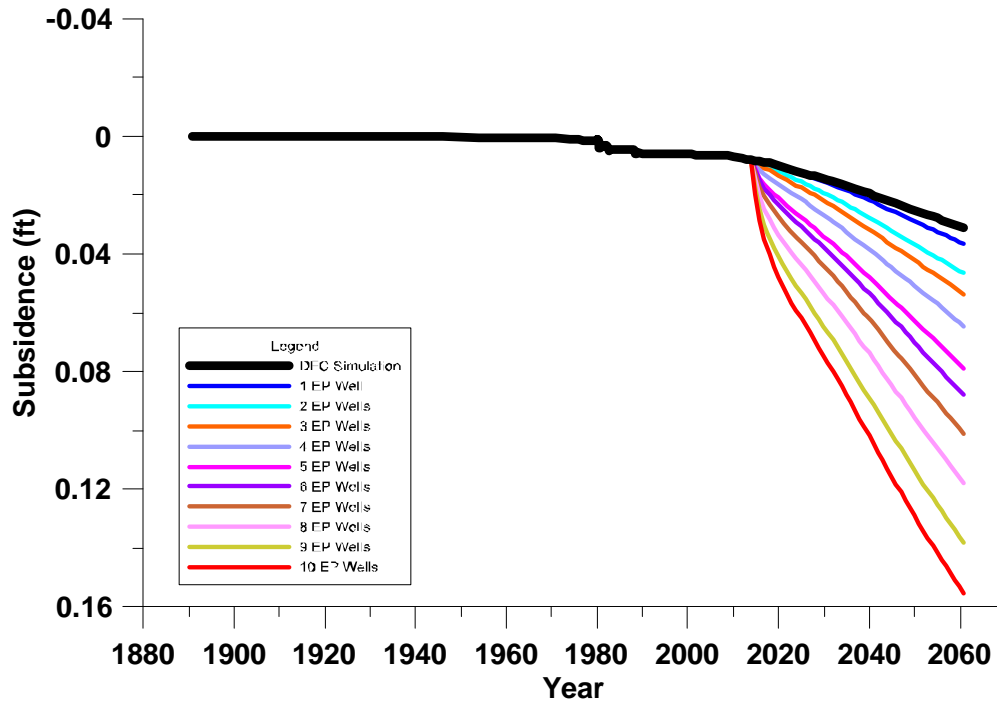


Figure E-2
Austin County - Average Subsidence
Electro Purification Pumping in Addition to MAG (HAGM)

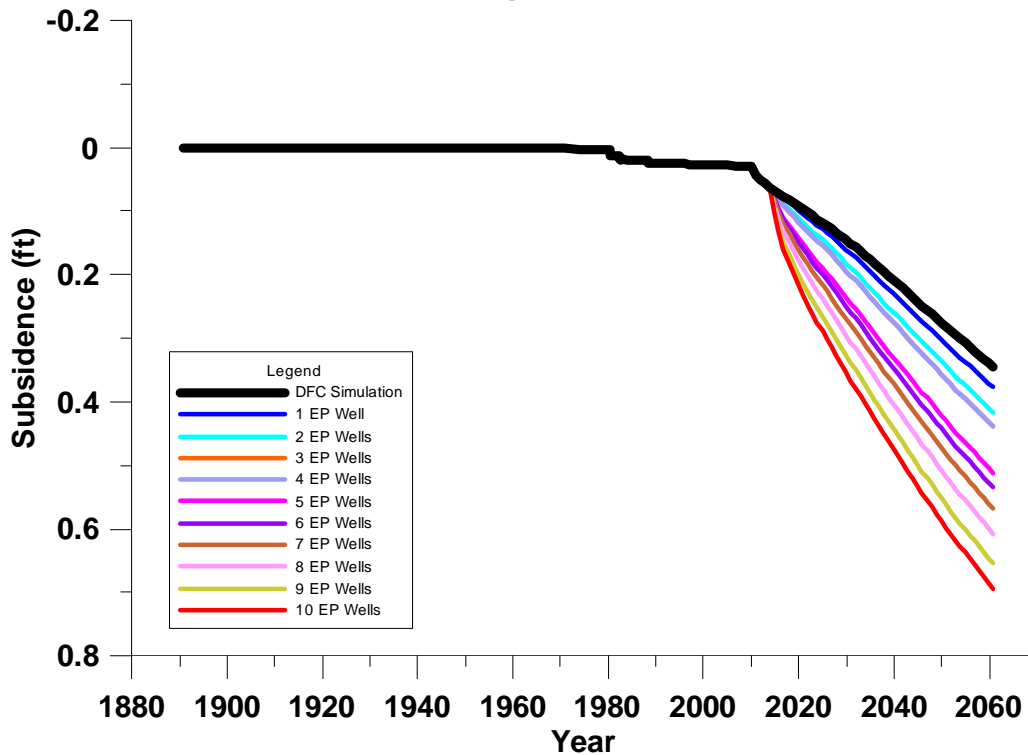


Figure E-3
Fort Bend County - Average Subsidence
Electro Purification Pumping in Addition to MAG (GAM)

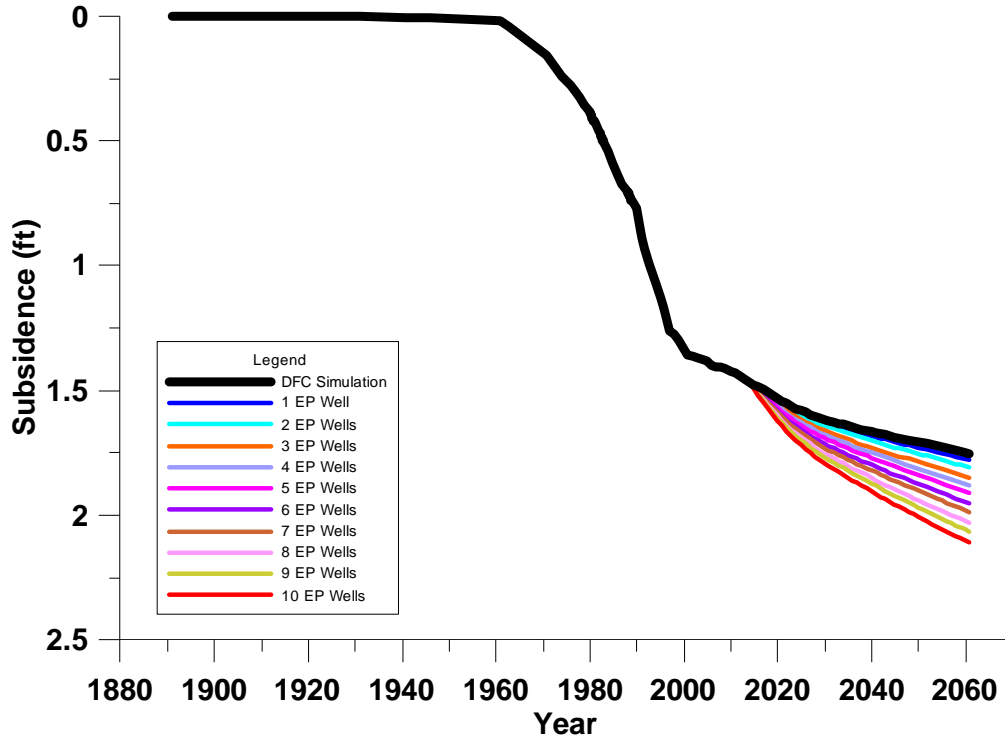
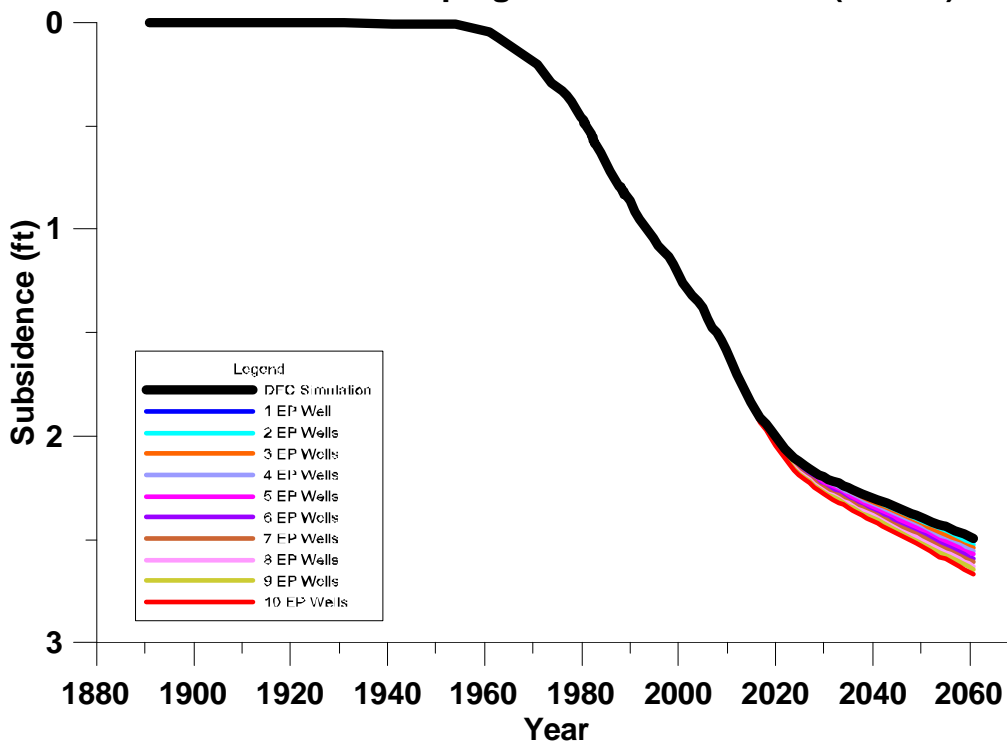
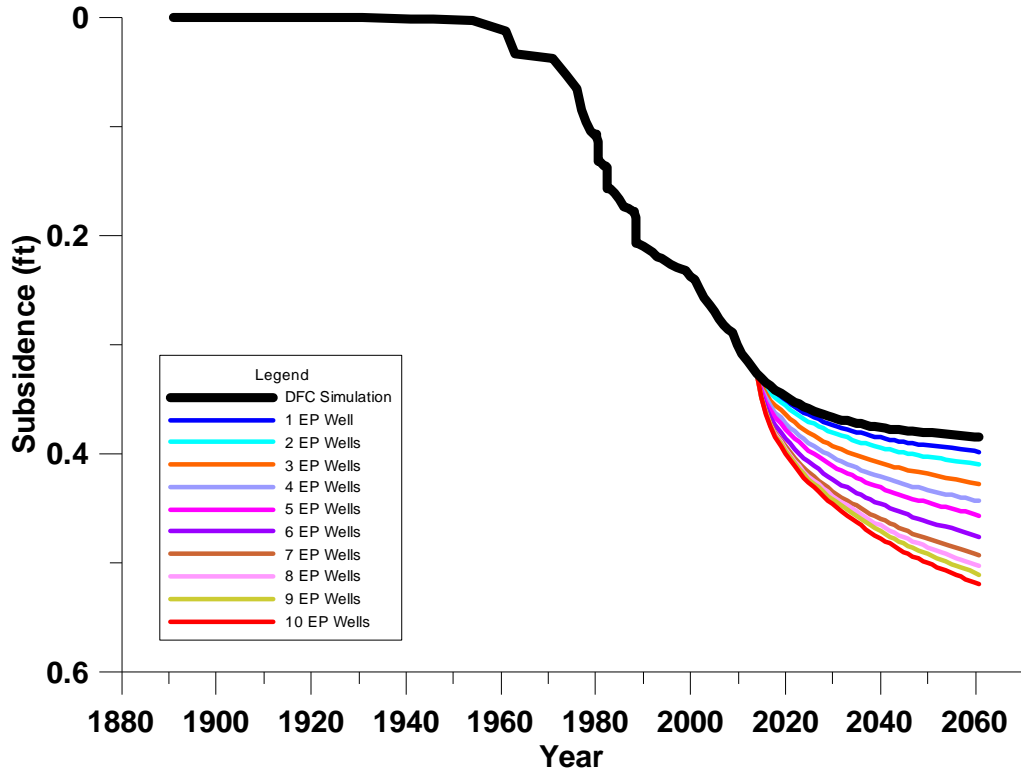


Figure E-4
Fort Bend County - Average Subsidence
Electro Purification Pumping in Addition to MAG (HAGM)



**Figure E-5
Waller County - Average Subsidence
Electro Purification Pumping in Addition to MAG (GAM)**



**Figure E-6
Waller County - Average Subsidence
Electro Purification Pumping in Addition to MAG (HAGM)**

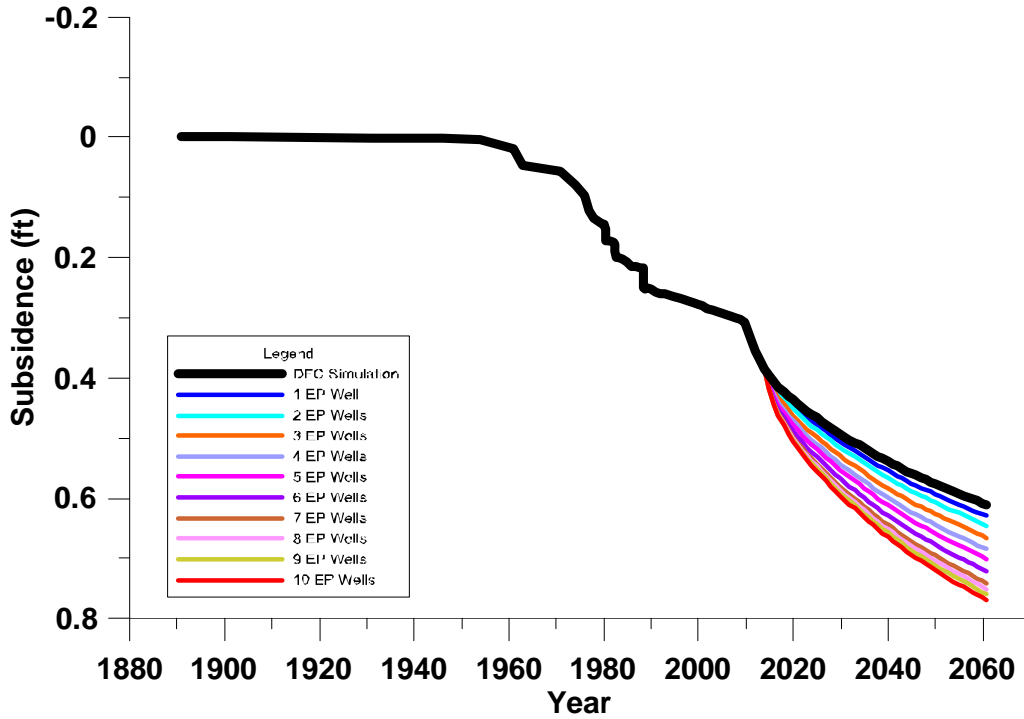


Figure E-7
Project Area - Average Subsidence
Electro Purification Pumping in Addition to MAG (GAM)

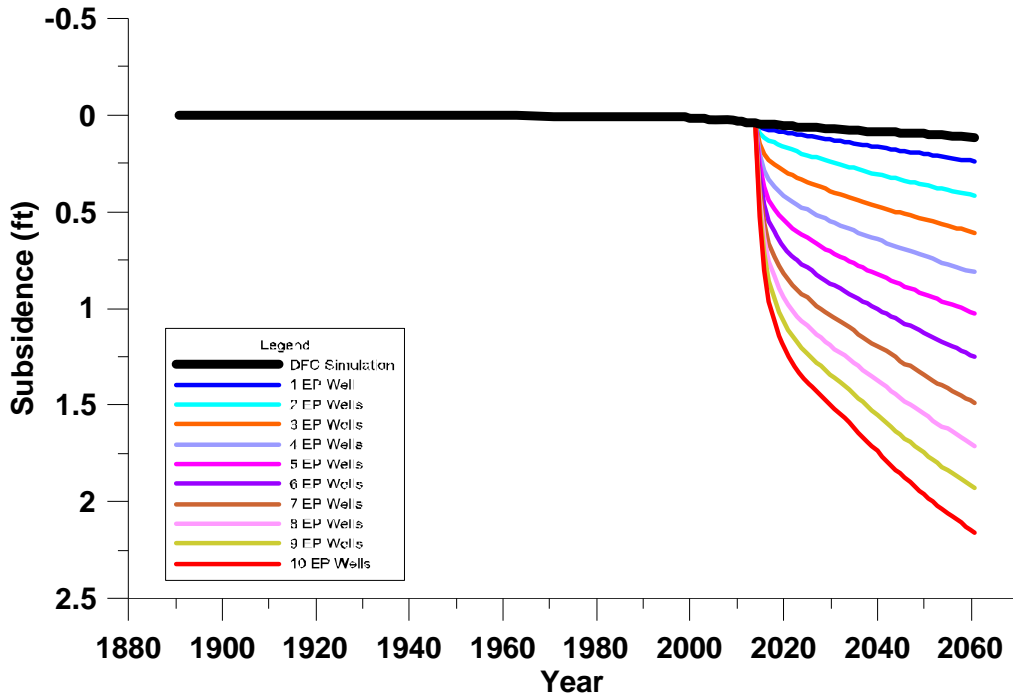


Figure E-8
Project Area - Average Subsidence
Electro Purification Pumping in Addition to MAG (HAGM)

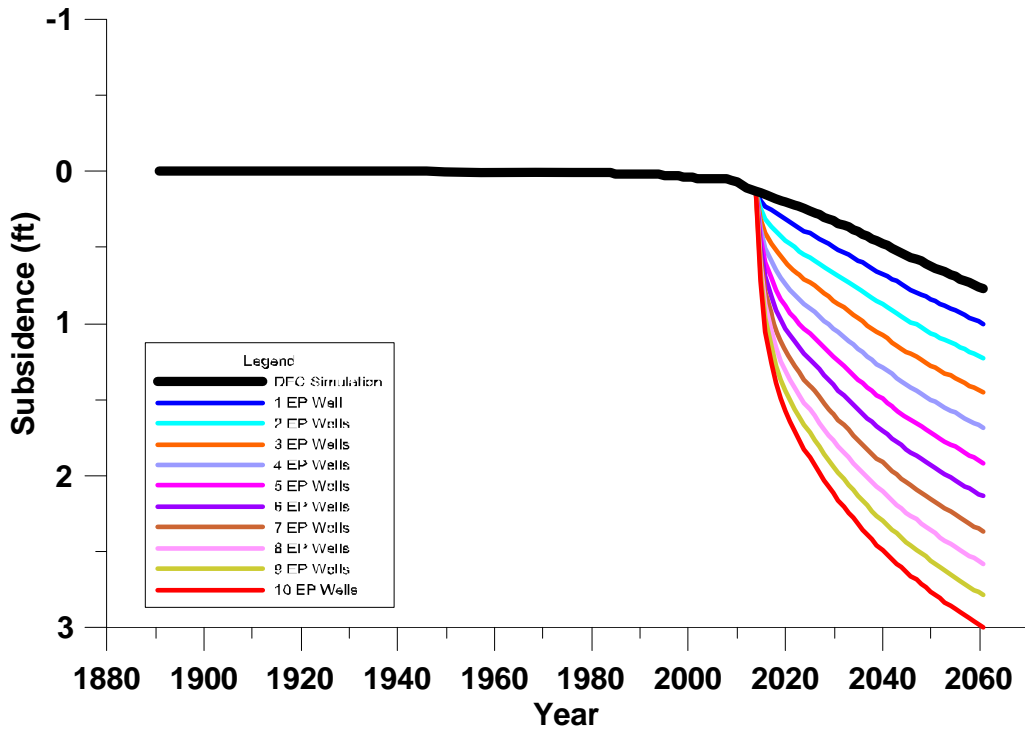


Figure E-9
Austin County - Average Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

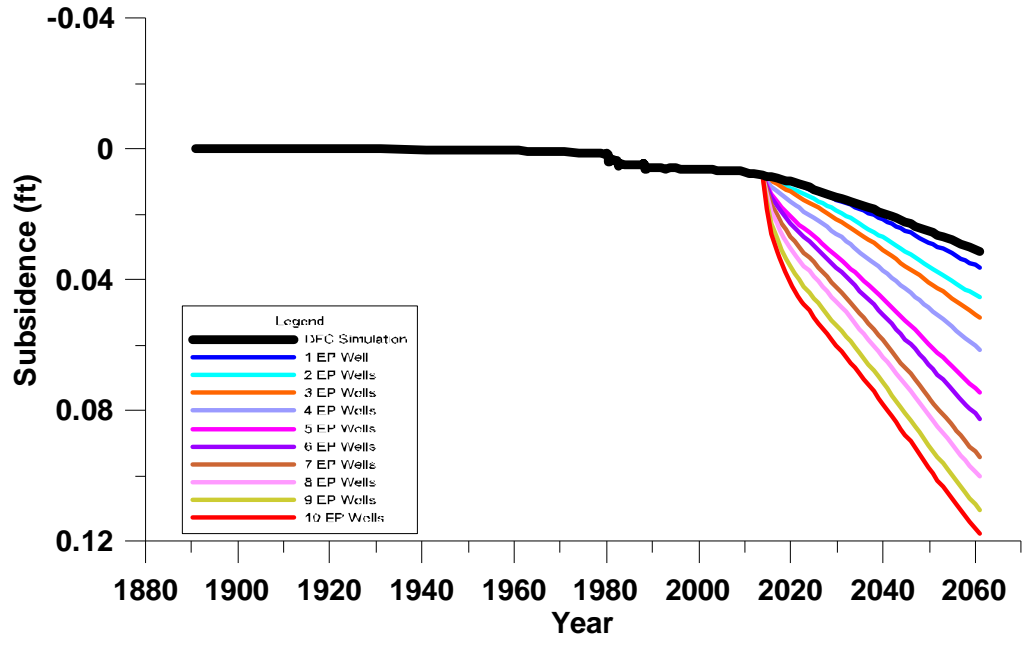


Figure E-10
Austin County - Average Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

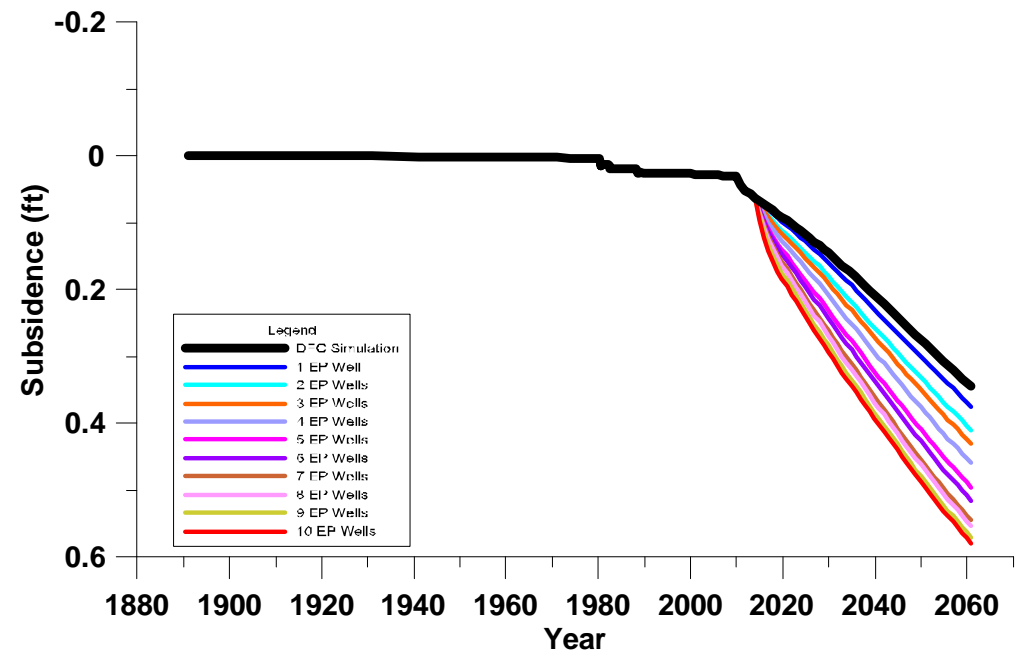


Figure E-11
Fort Bend County - Average Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

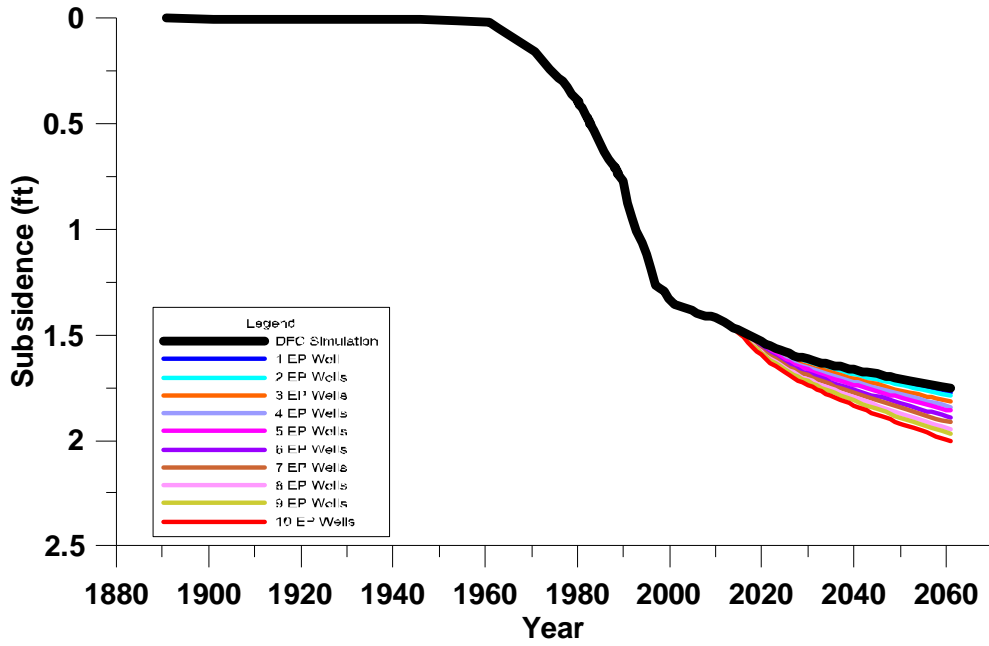


Figure E-12
Fort Bend County - Average Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

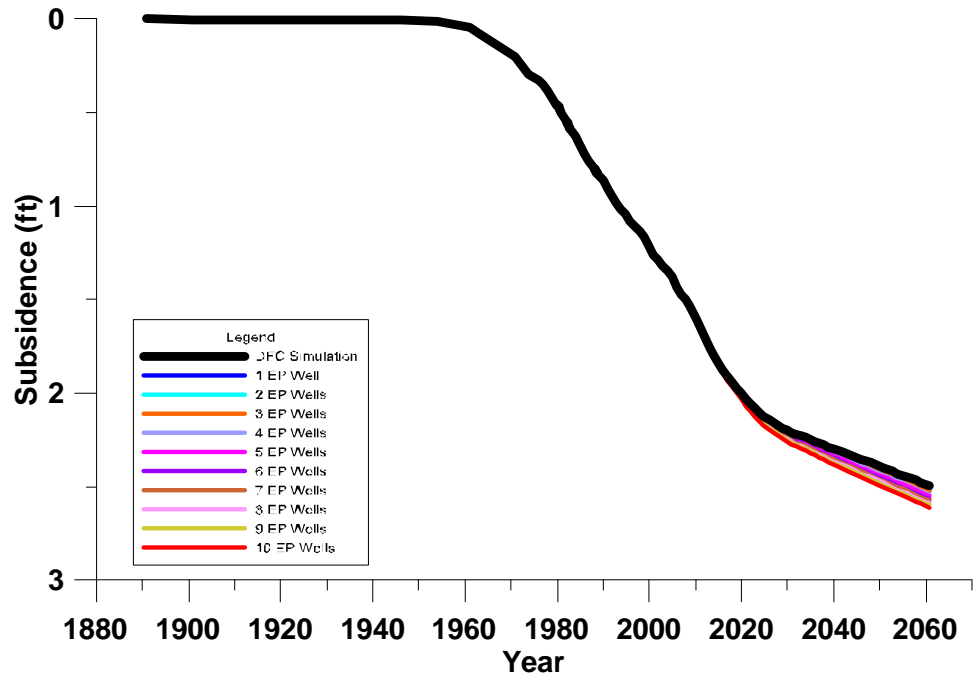


Figure E-13
Waller County - Average Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

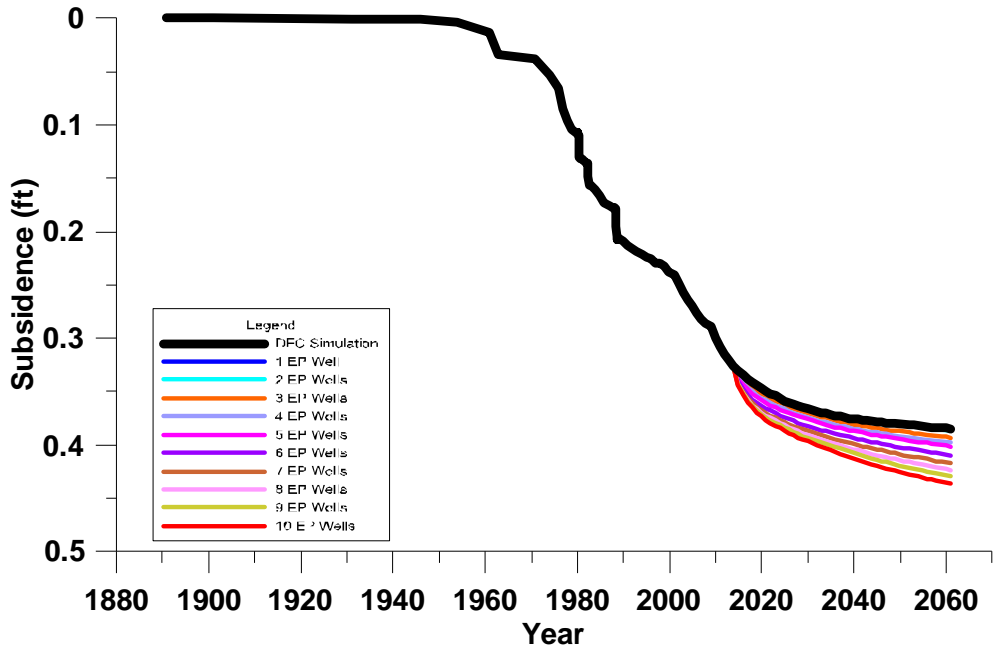


Figure E-14
Waller County - Average Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

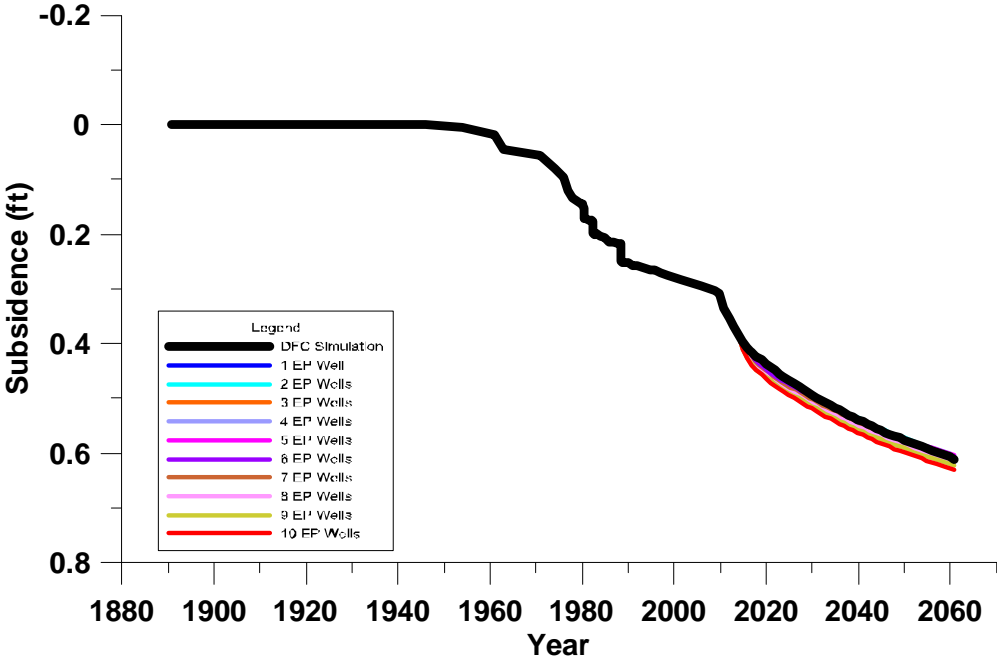


Figure E-15
Project Area - Average Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

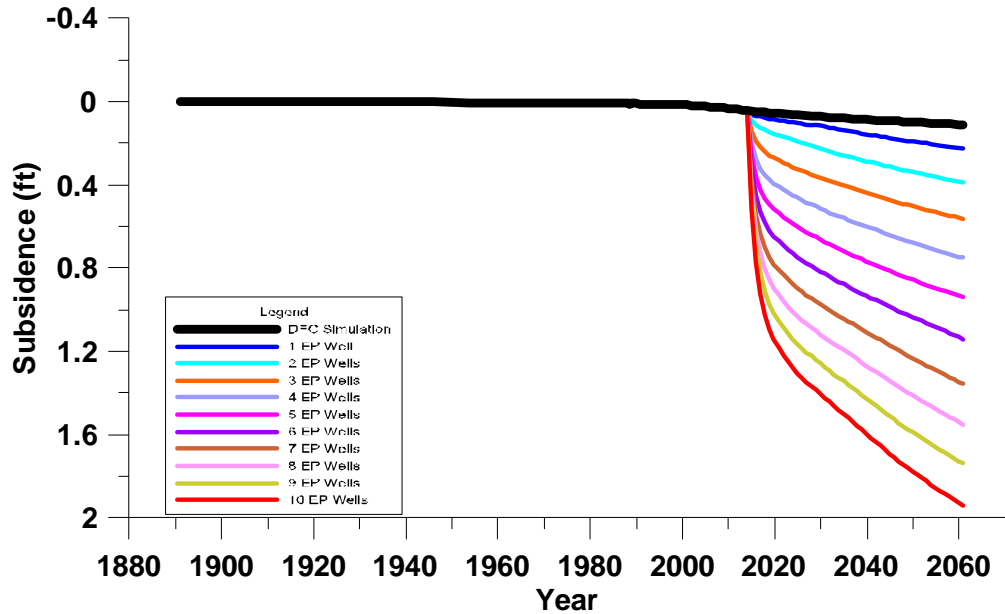


Figure E-16
Project Area - Average Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

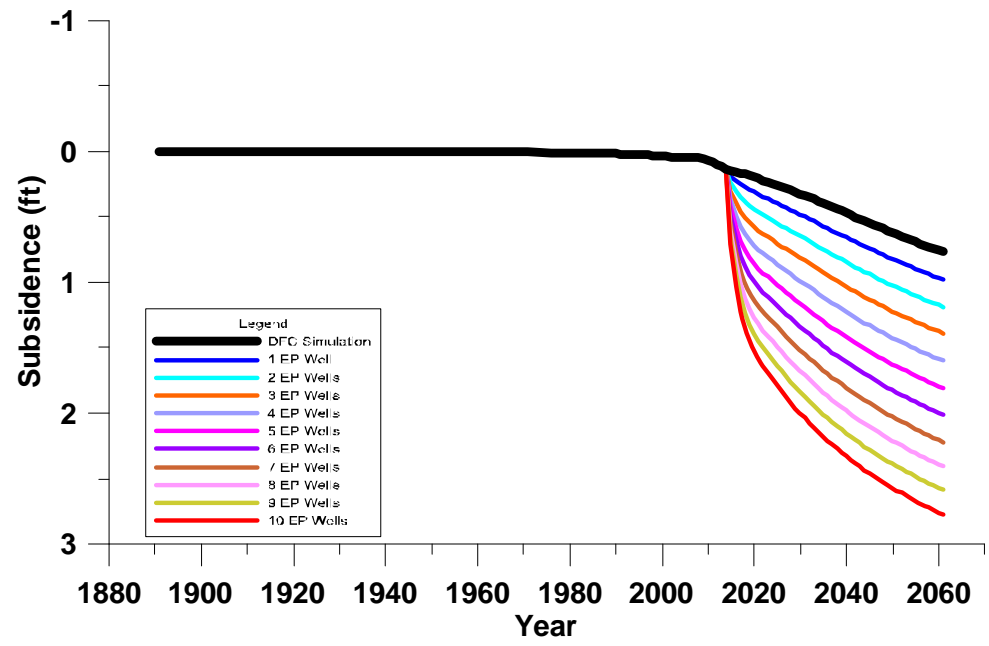


Figure E-17
Austin County - Average Subsidence
Electro Purification Pumping - Evangeline/Jasper (GAM)

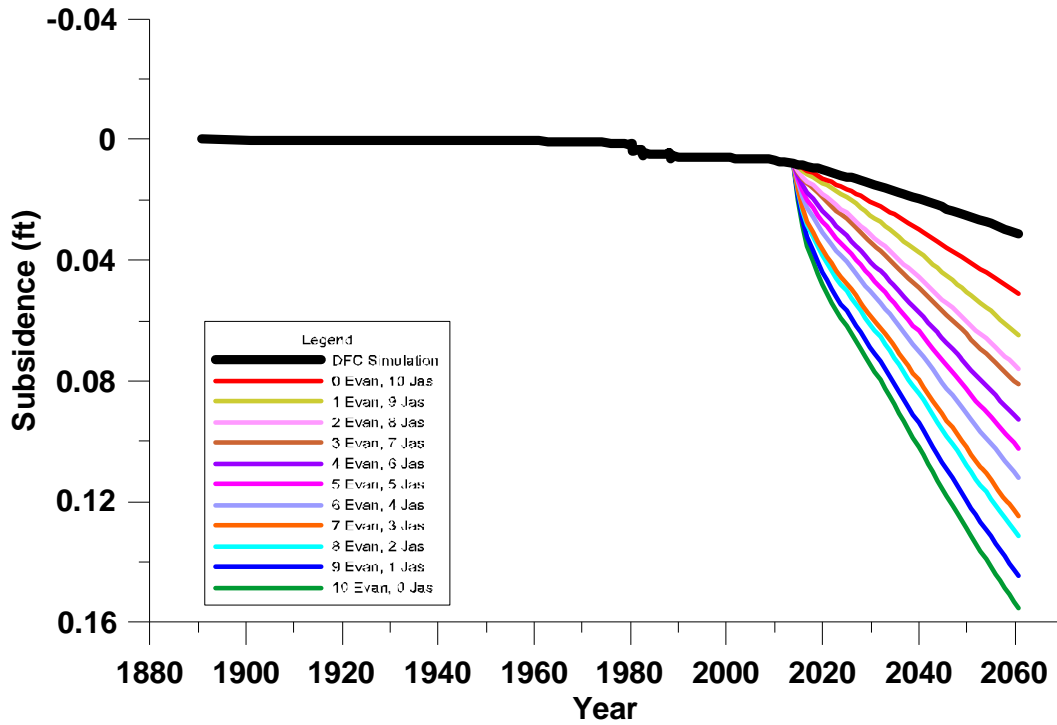


Figure E-18
Austin County - Average Subsidence
Electro Purification Pumping - Evangeline/Jasper (HAGM)

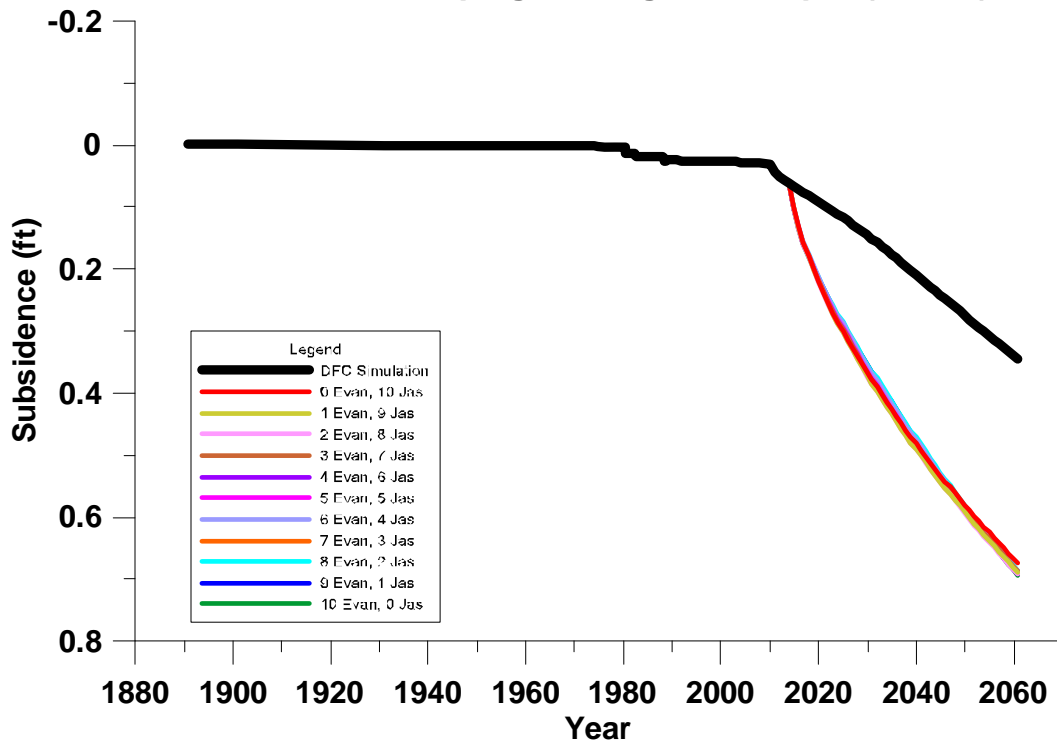


Figure E-19
Fort Bend County - Average Subsidence
Electro Purification Pumping - Evangeline/Jasper (GAM)

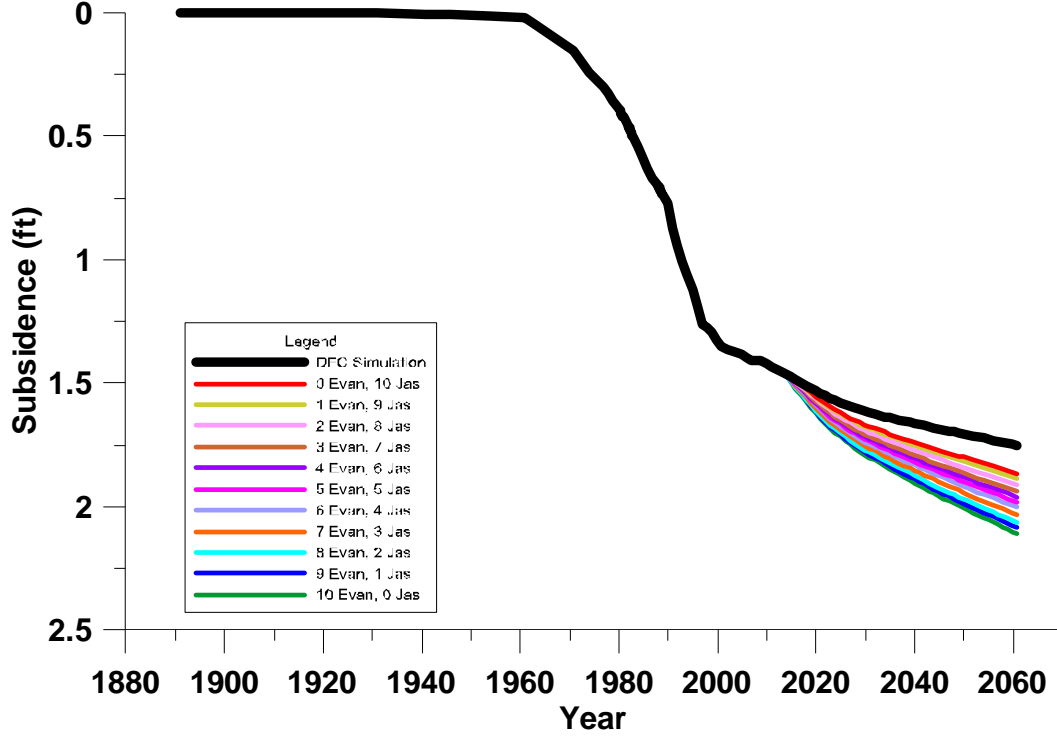


Figure E-20
Fort Bend County - Average Subsidence
Electro Purification Pumping - Evangeline/Jasper (HAGM)

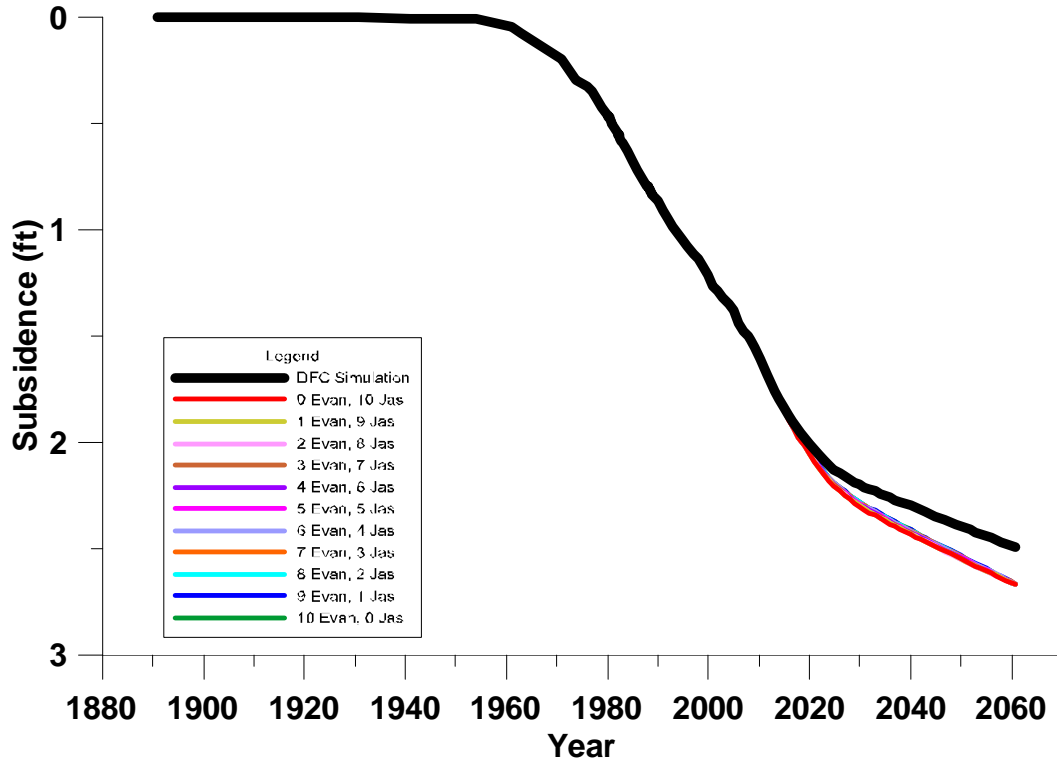


Figure E-21
Waller County - Average Subsidence
Electro Purification Pumping - Evangeline/Jasper
GAM

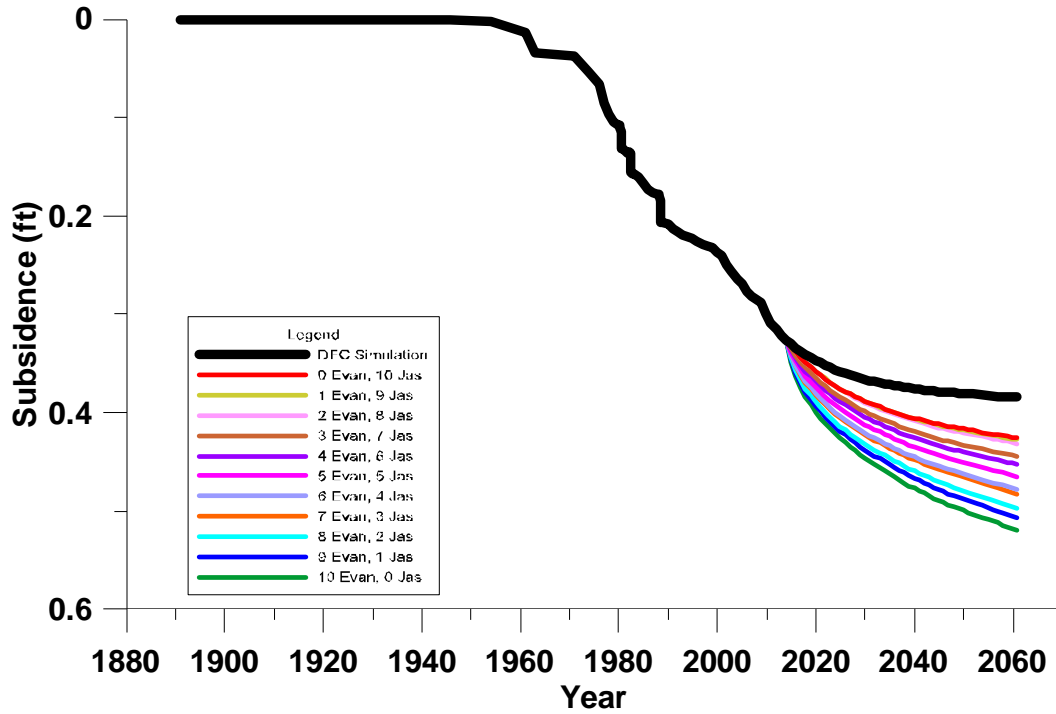


Figure E-22
Waller County - Average Subsidence
Electro Purification Pumping - Evangeline/Jasper
HAGM

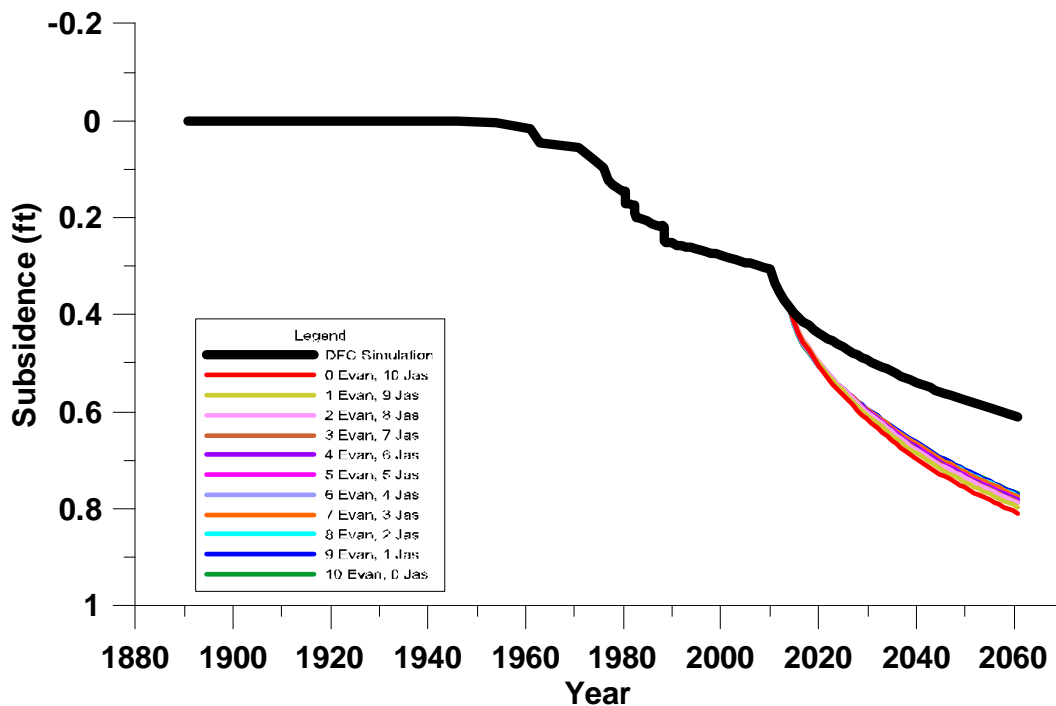


Figure E-23
Project Area - Average Subsidence
Electro Purification Pumping - Evangeline/Jasper (GAM)

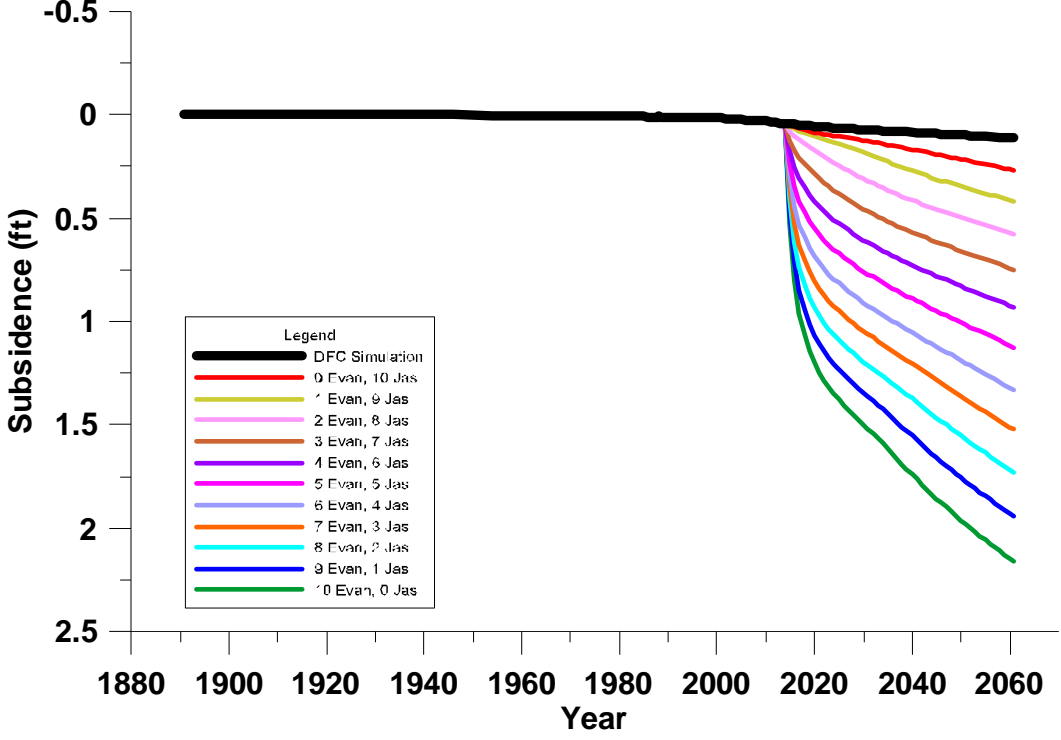


Figure E-24
Project Area - Average Subsidence
Electro Purification Pumping - Evangeline/Jasper (HAGM)

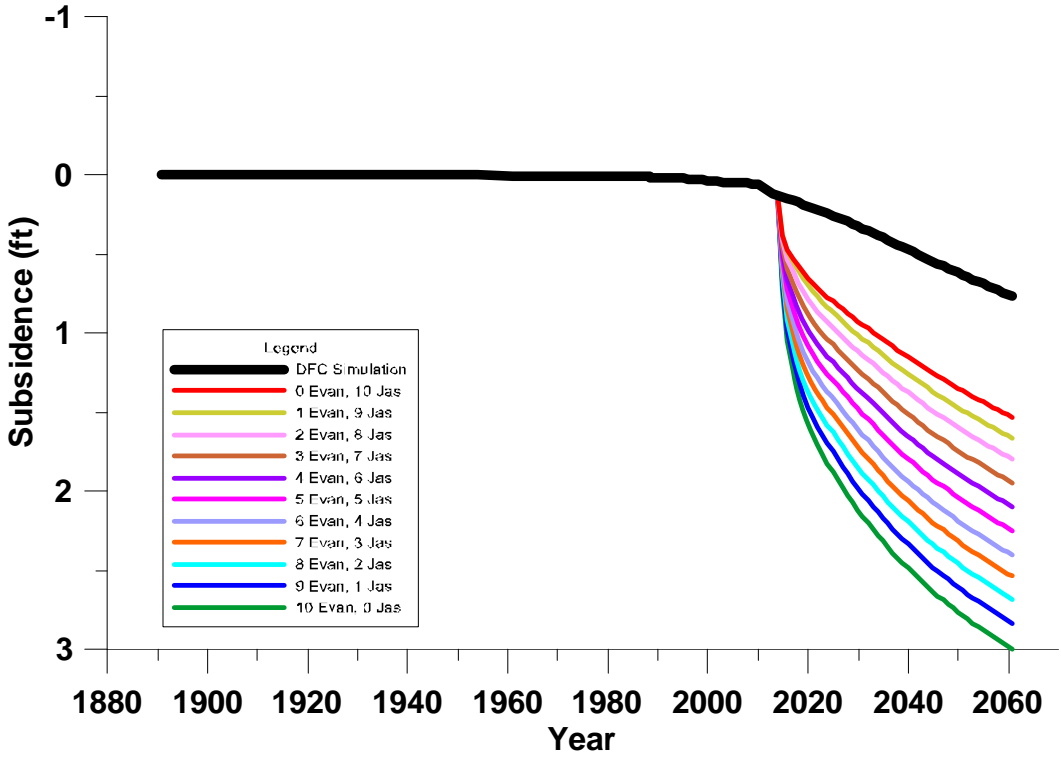


Figure E-25
Austin County - Average Subsidence
Electro Purification Pumping - Conversion Schedule (GAM)

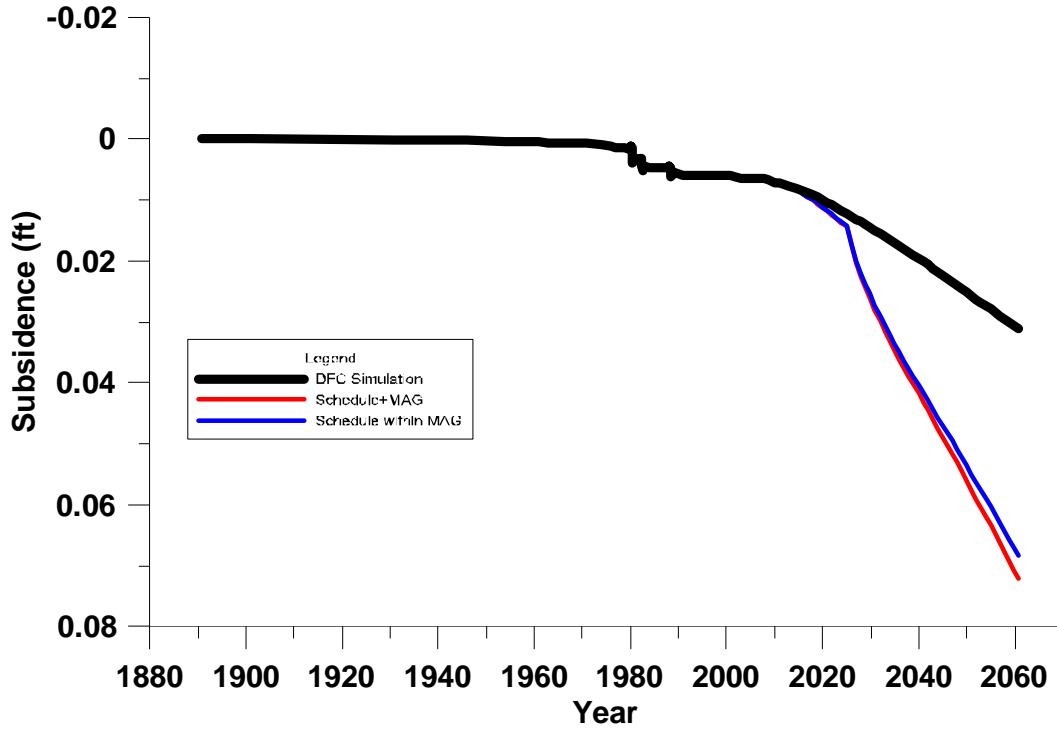
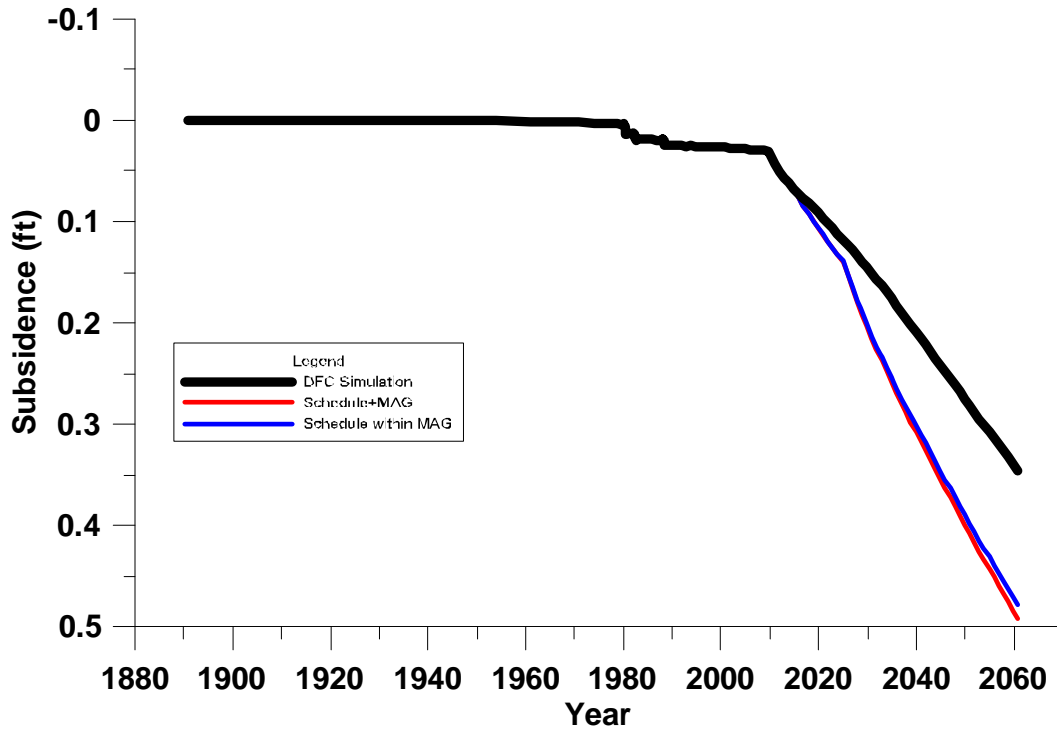
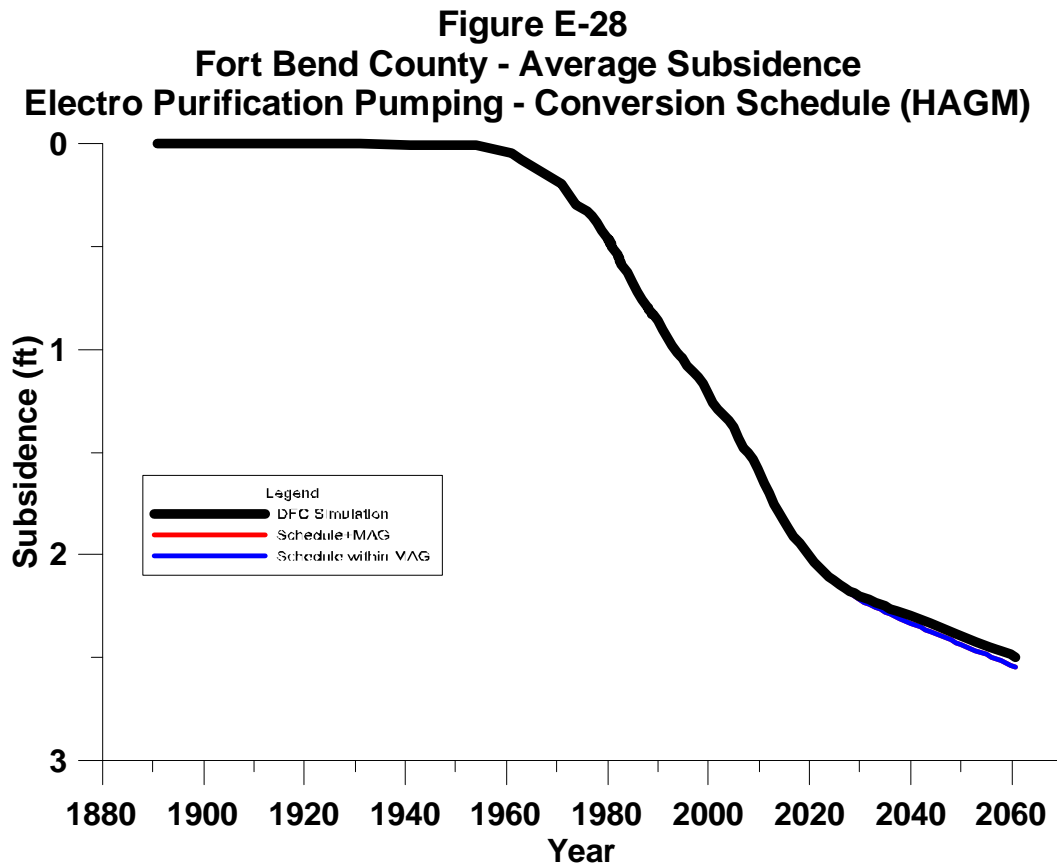
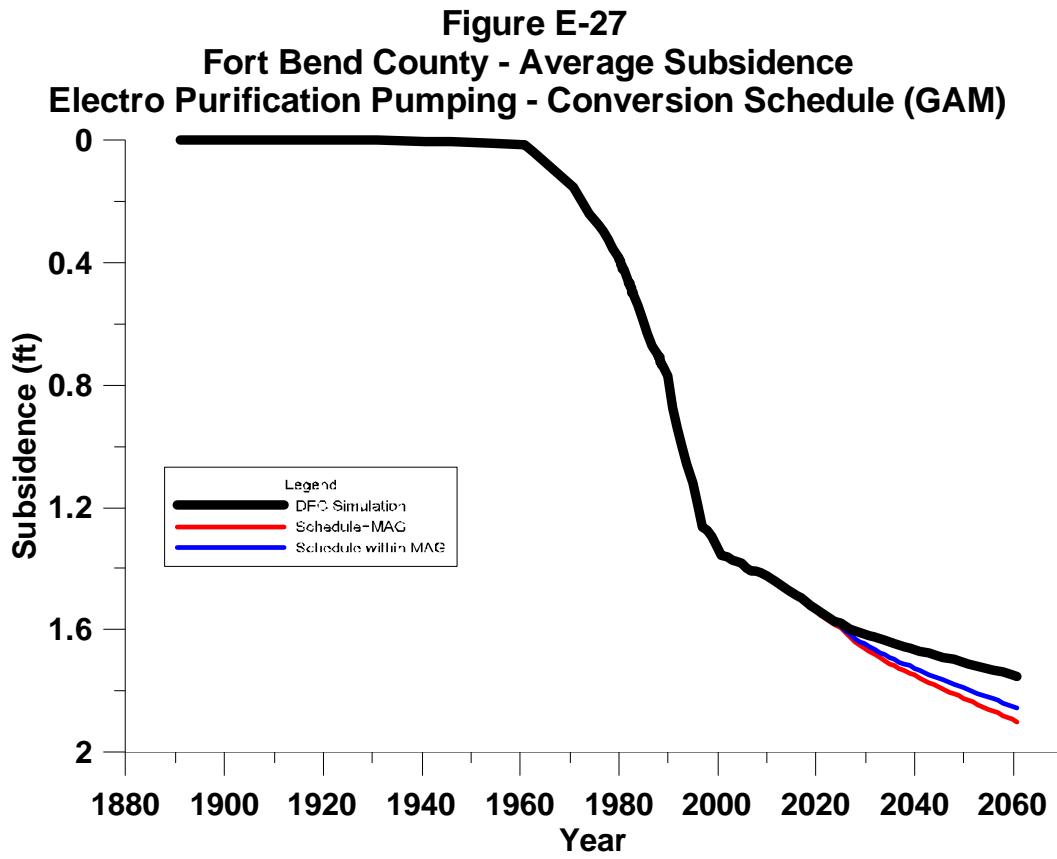
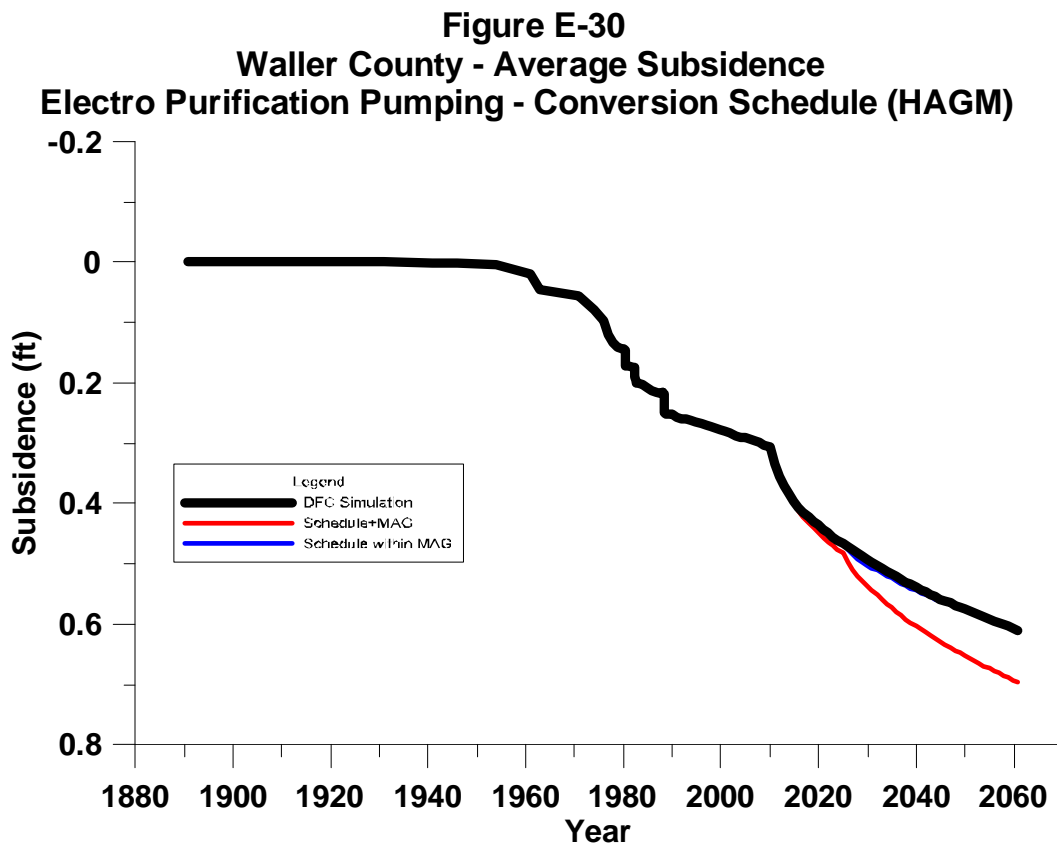
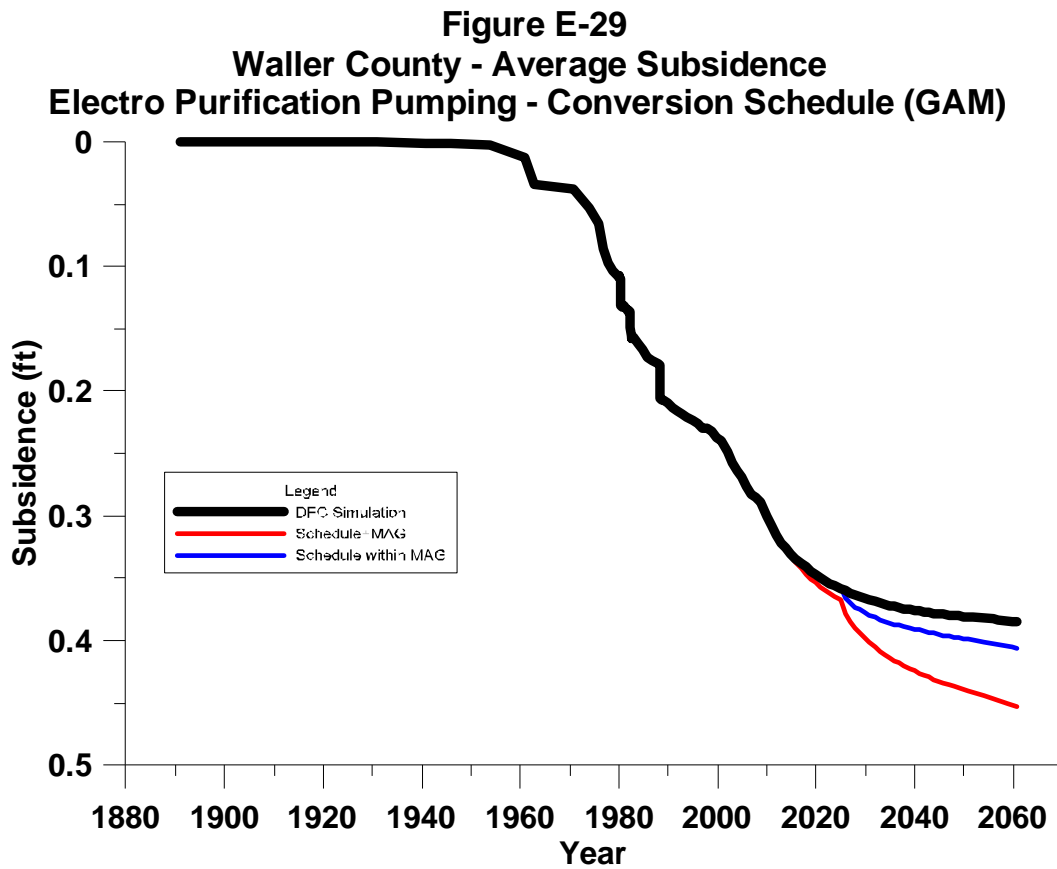


Figure E-26
Austin County - Average Subsidence
Electro Purification Pumping - Conversion Schedule (HAGM)







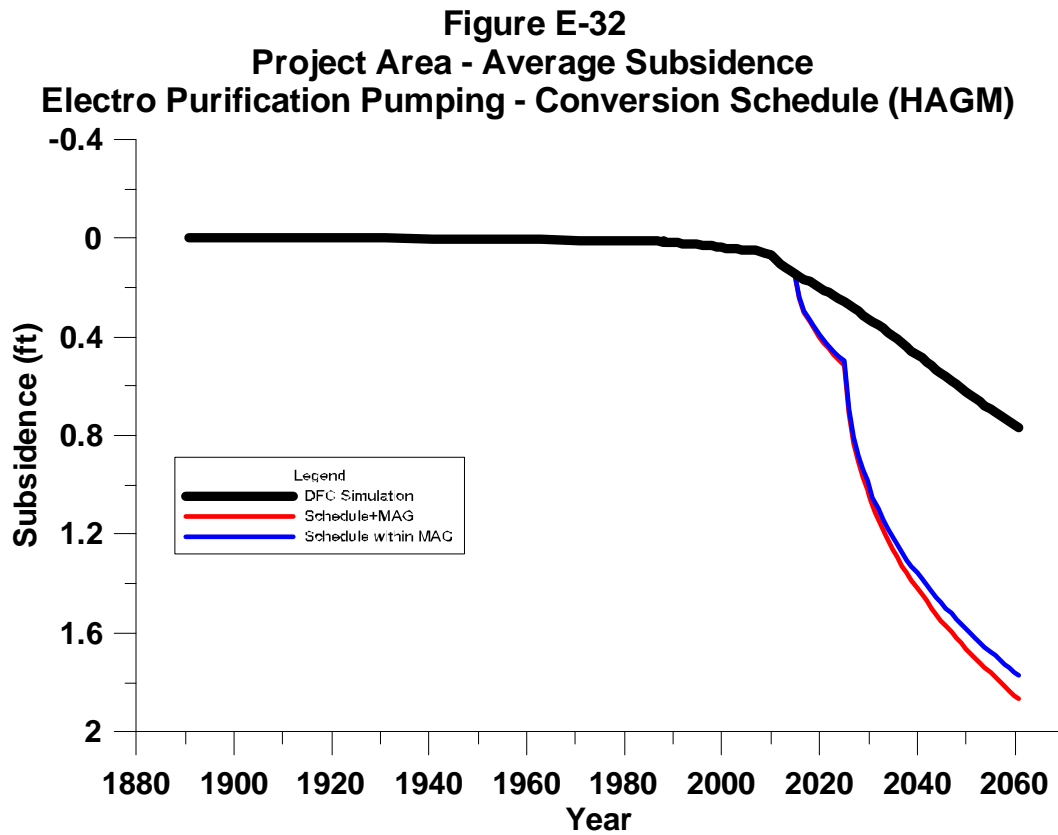
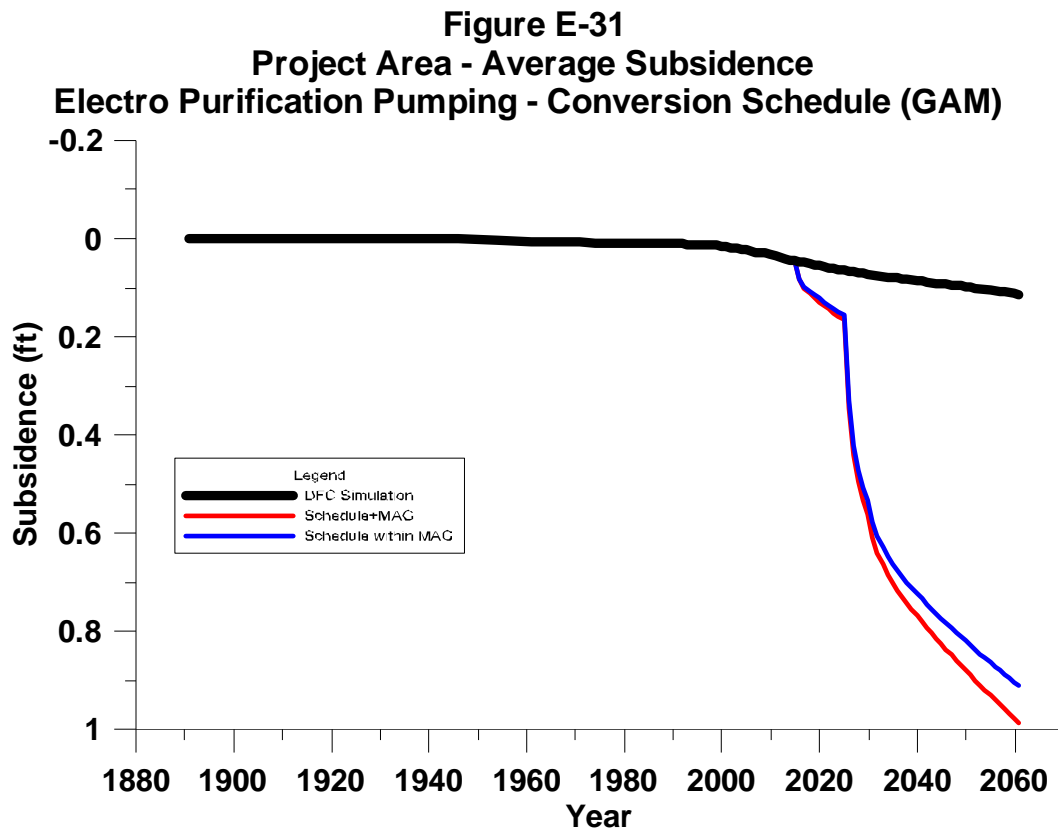


Figure E-33
Austin County - Maximum Subsidence
Electro Purification Pumping in Addition to MAG (GAM)

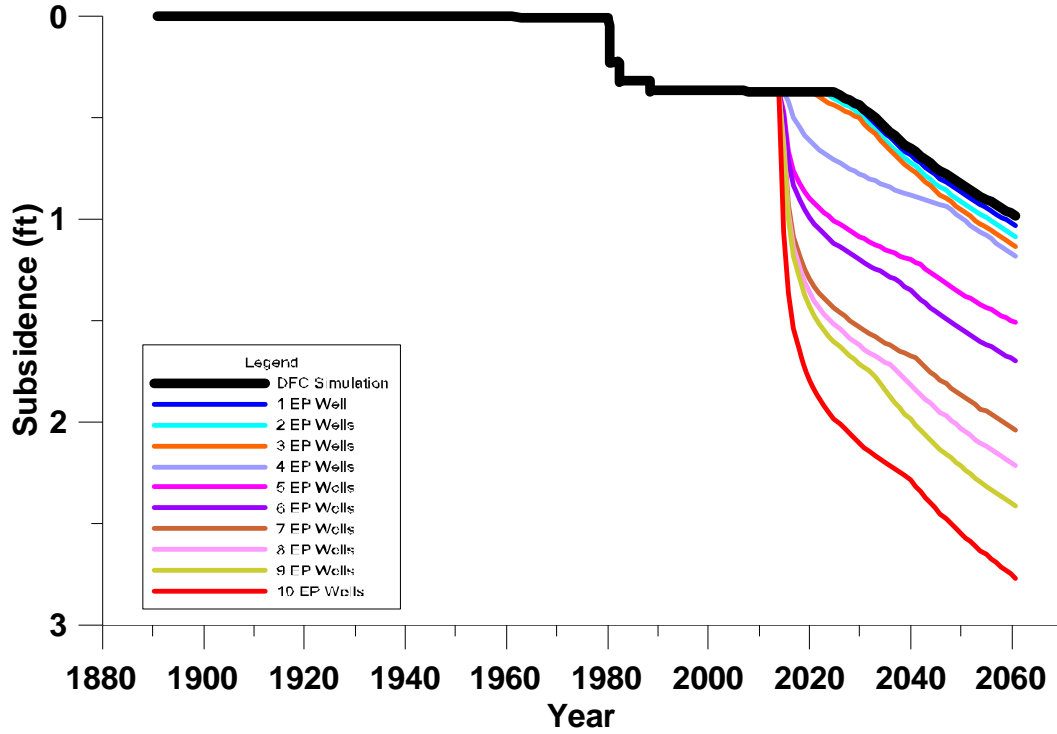


Figure E-34
Austin County - Maximum Subsidence
Electro Purification Pumping in Addition to MAG (HAGM)

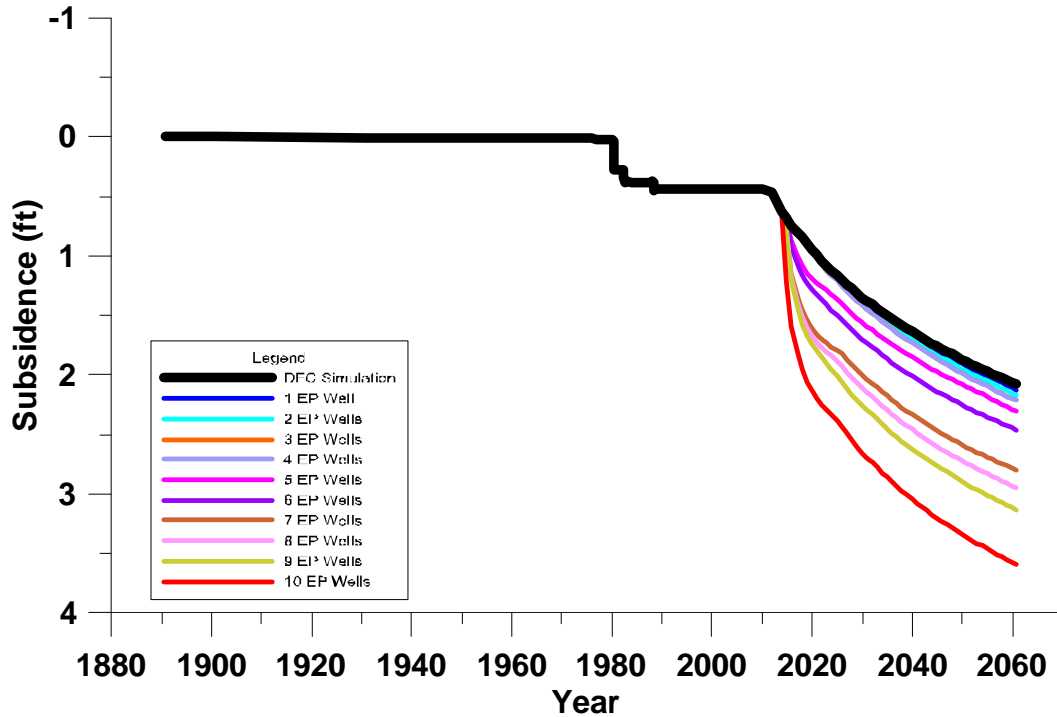


Figure E-35
Fort Bend County - Maximum Subsidence
Electro Purification Pumping in Addition to MAG (GAM)

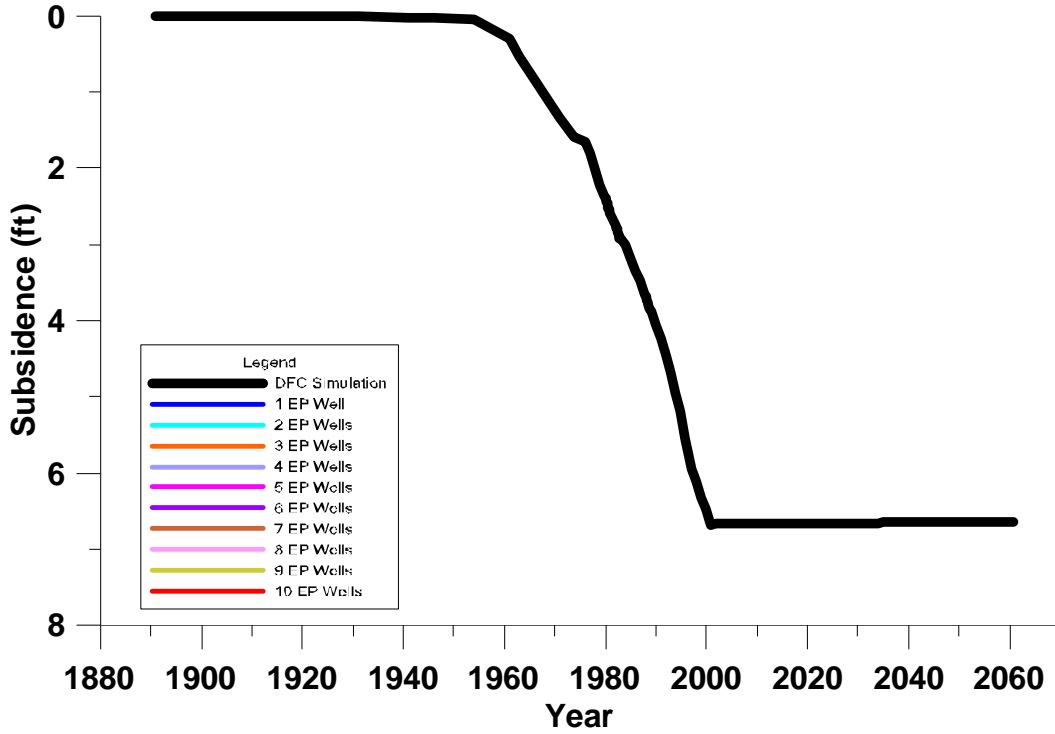


Figure E-36
Fort Bend County - Maximum Subsidence
Electro Purification Pumping in Addition to MAG (HAGM)

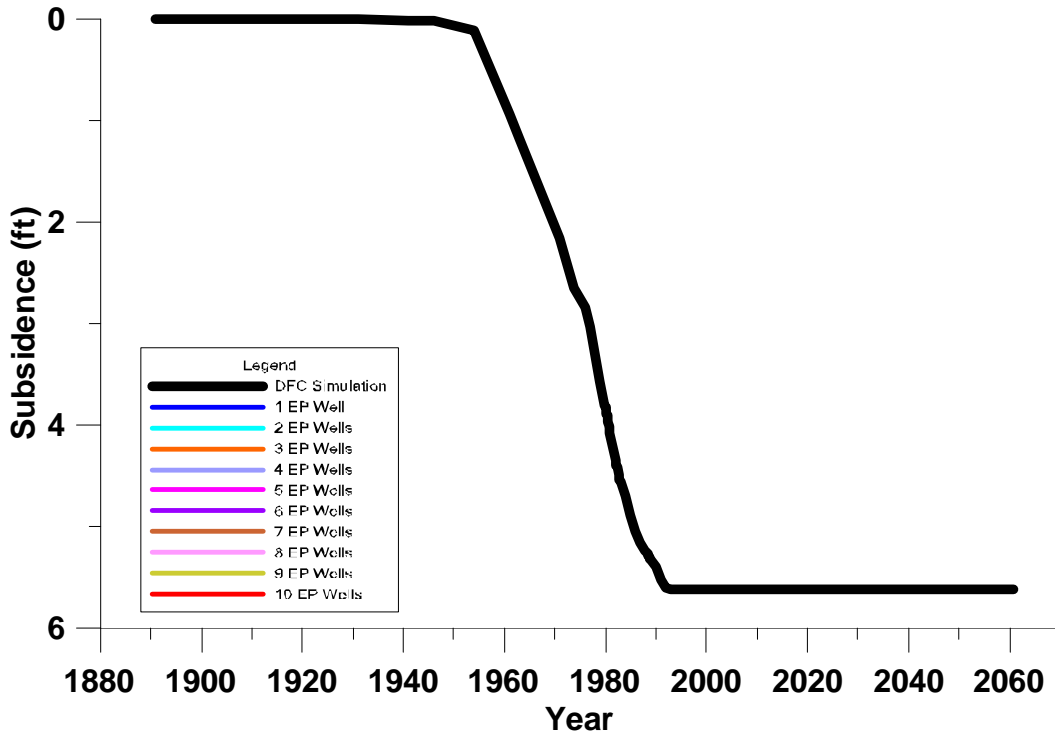


Figure E-37
Waller County - Maximum Subsidence
Electro Purification Pumping in Addition to MAG (GAM)

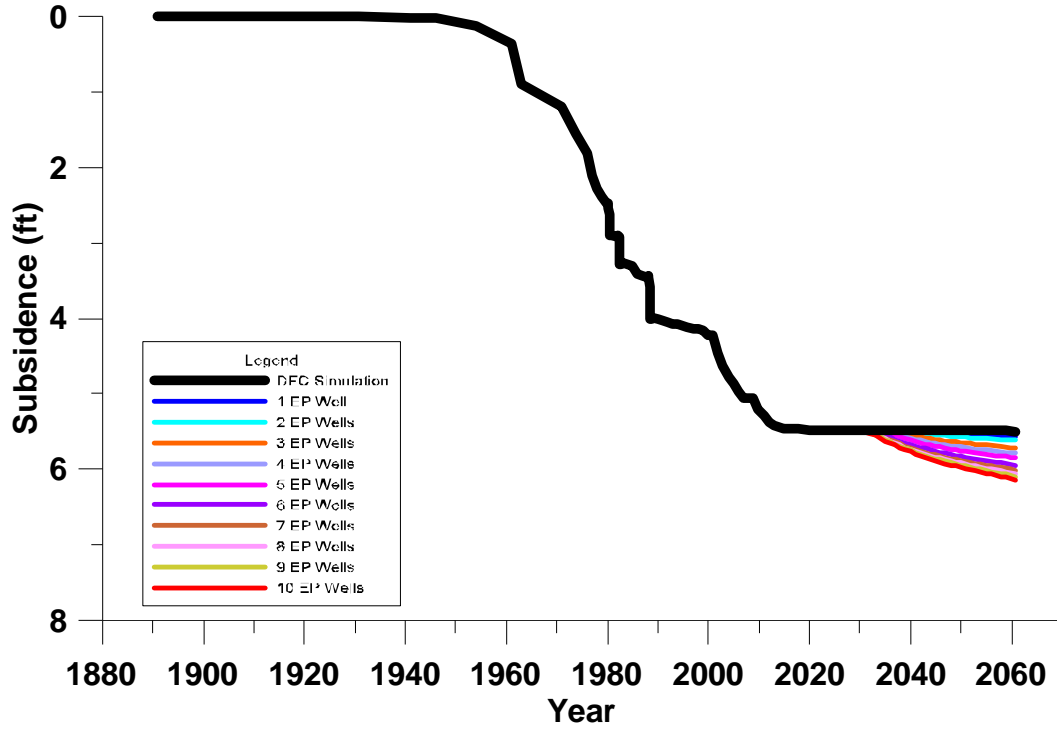


Figure E-38
Waller County - Maximum Subsidence
Electro Purification Pumping in Addition to MAG (HAGM)

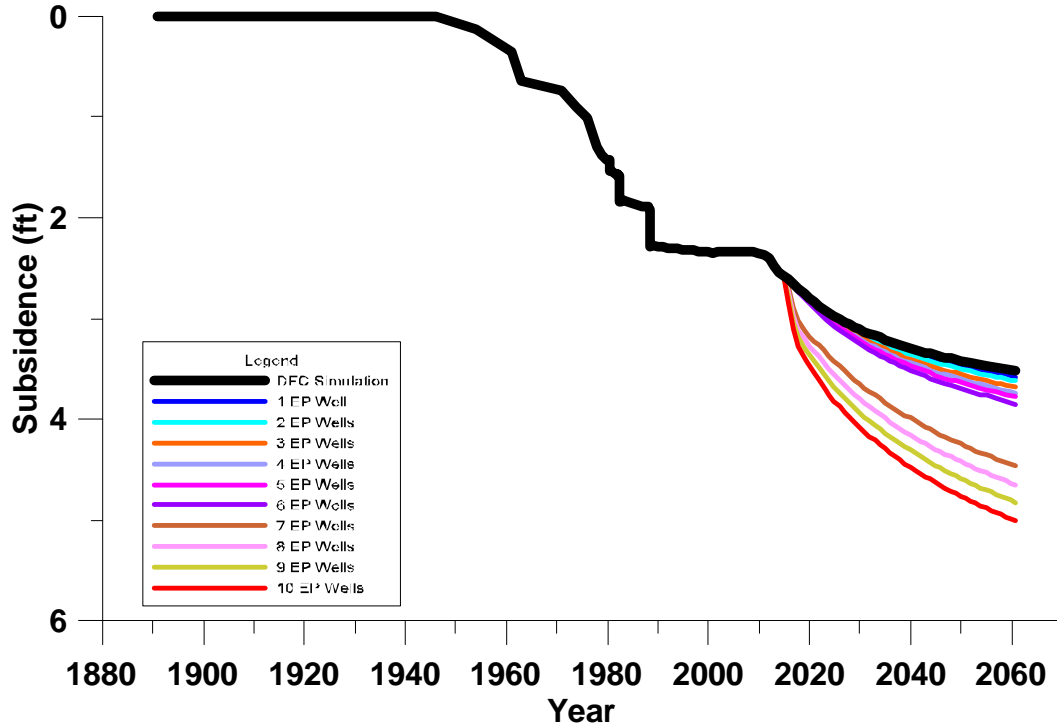


Figure E-39
Project Area - Maximum Subsidence
Electro Purification Pumping in Addition to MAG (GAM)

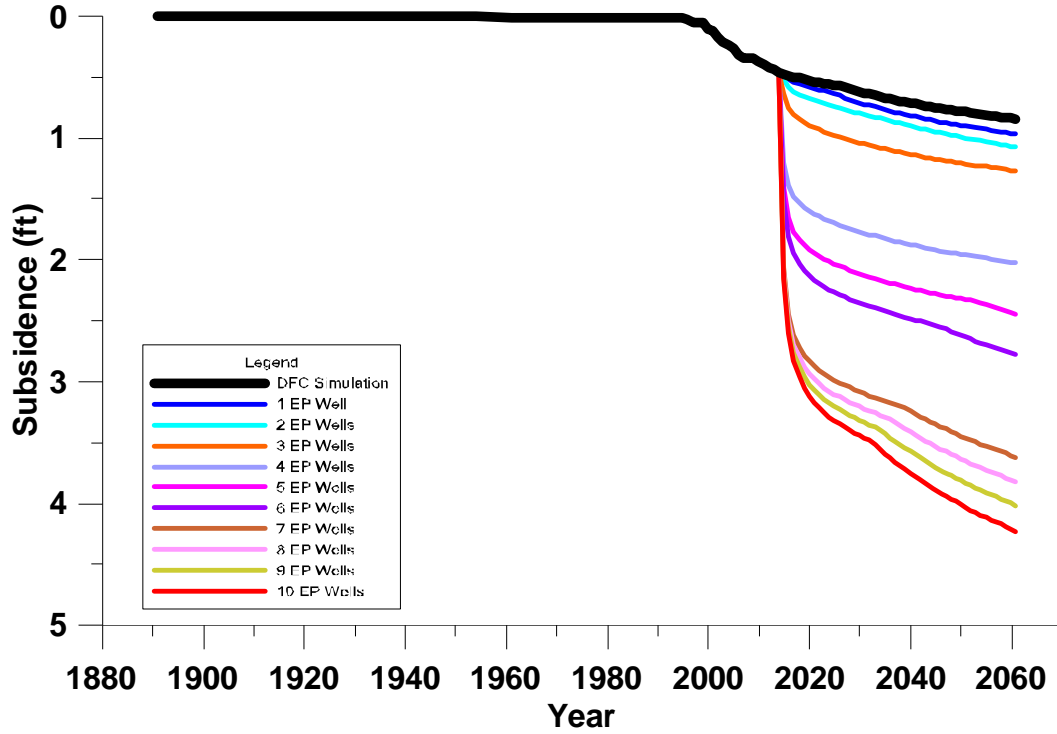


Figure E-40
Project Area - Maximum Subsidence
Electro Purification Pumping in Addition to MAG (HAGM)

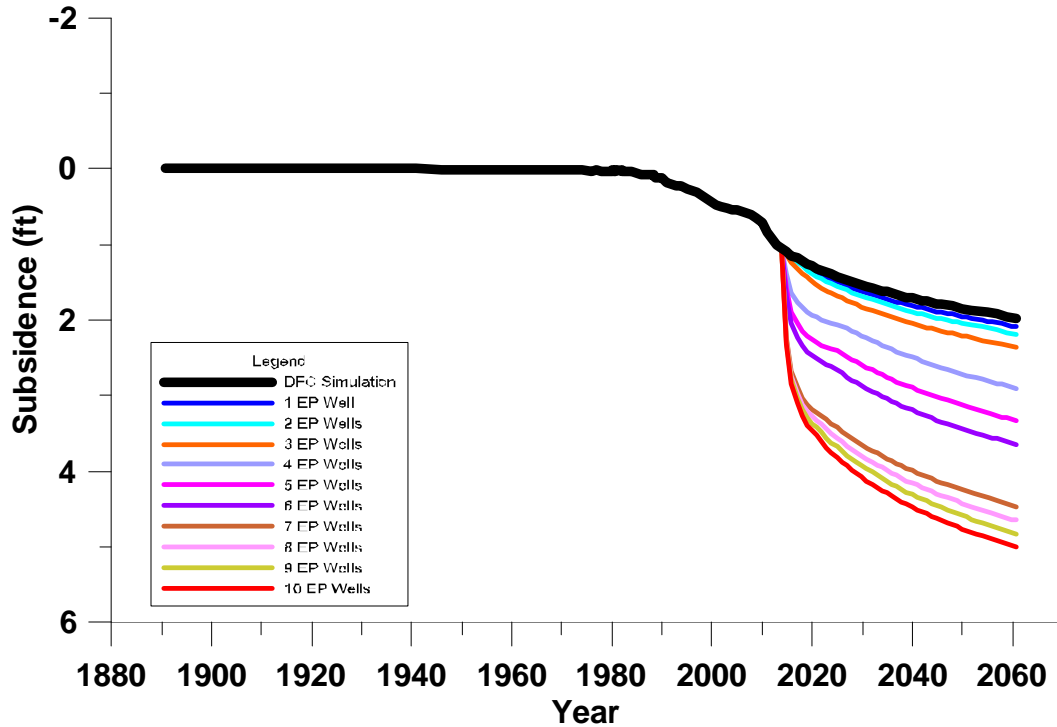


Figure E-41
Austin County - Maximum Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

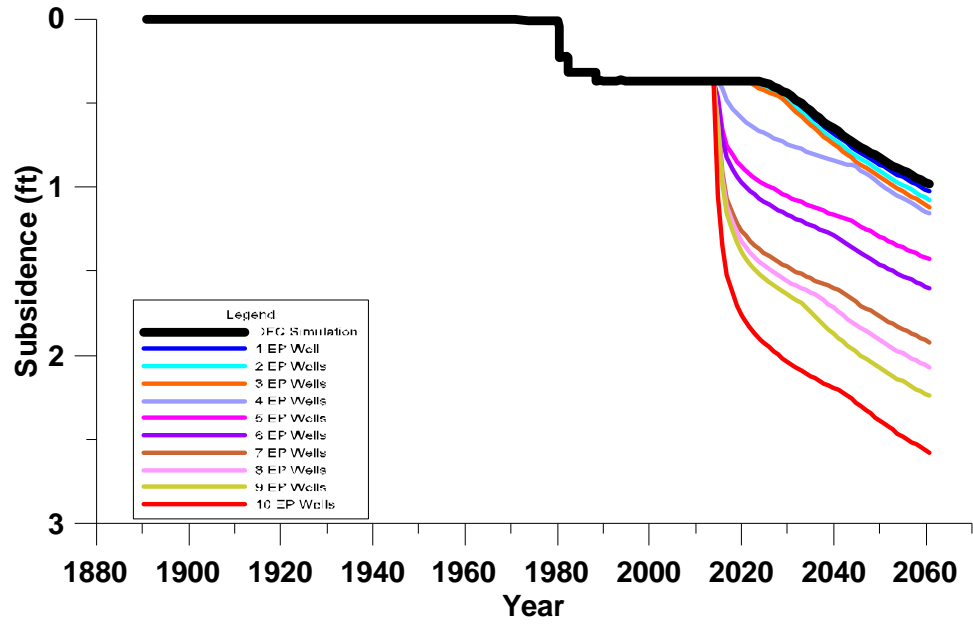


Figure E-42
Austin County - Maximum Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

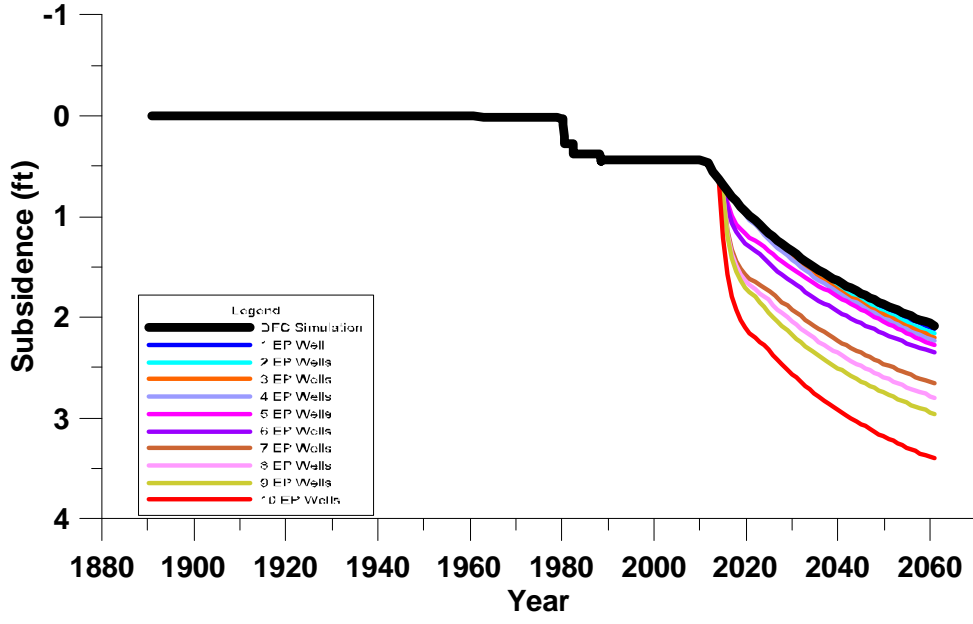


Figure E-43
Fort Bend County - Maximum Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

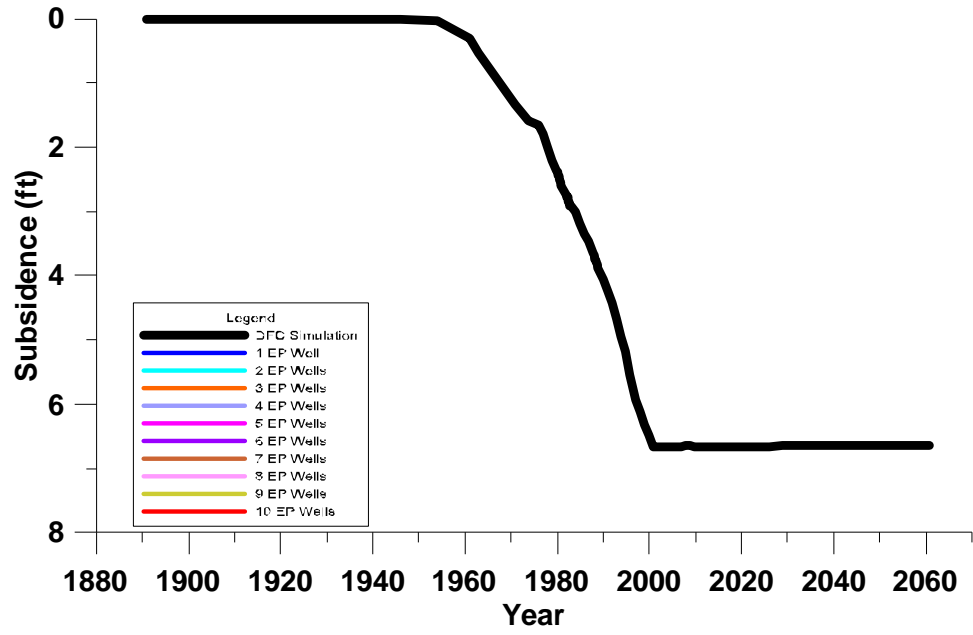


Figure E-44
Fort Bend County - Maximum Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

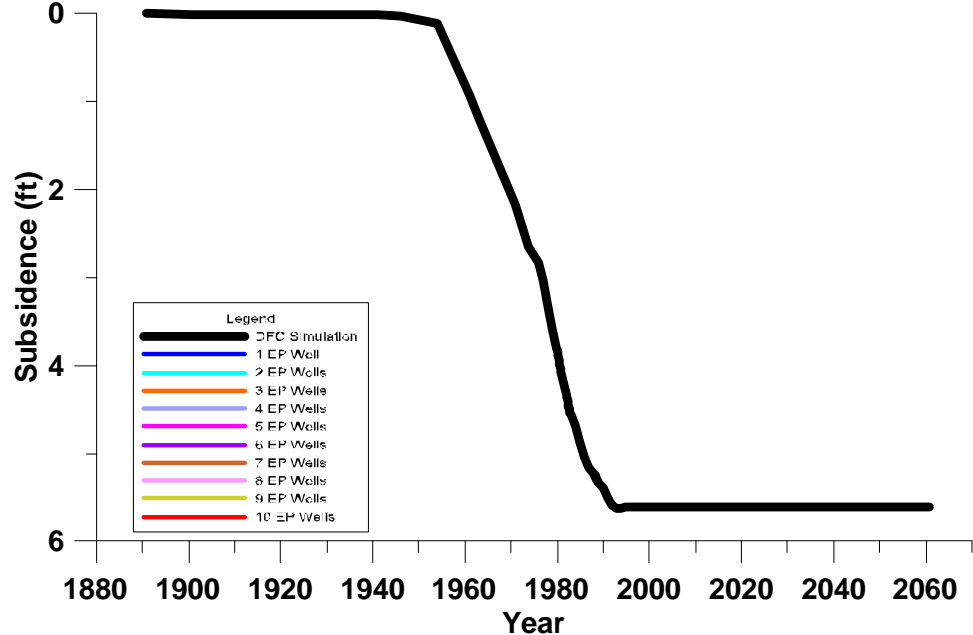


Figure E-45
Waller County - Maximum Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

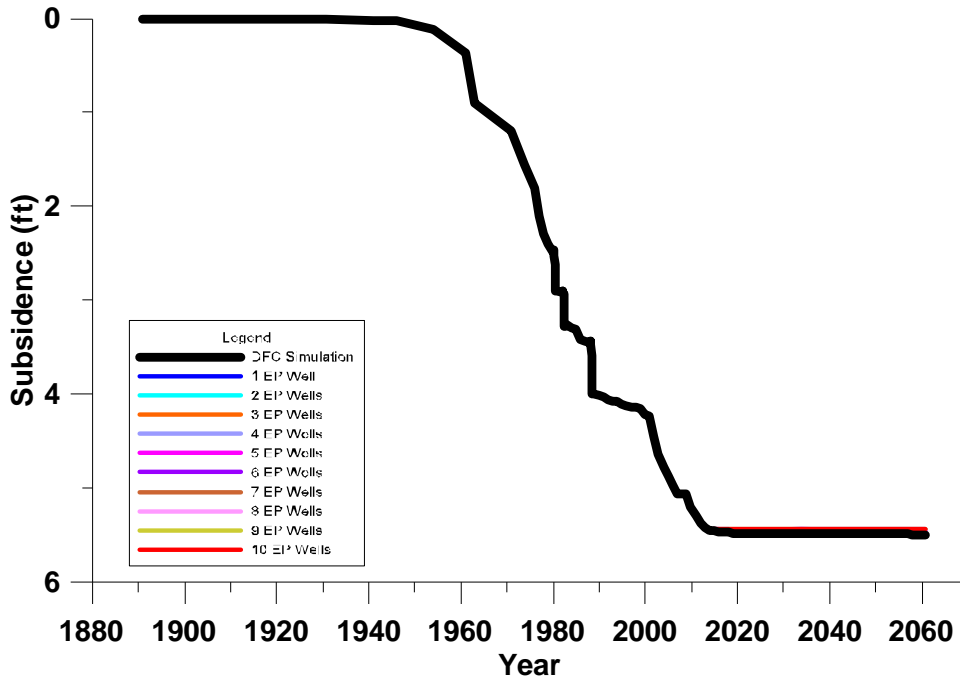


Figure E-46
Waller County - Maximum Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

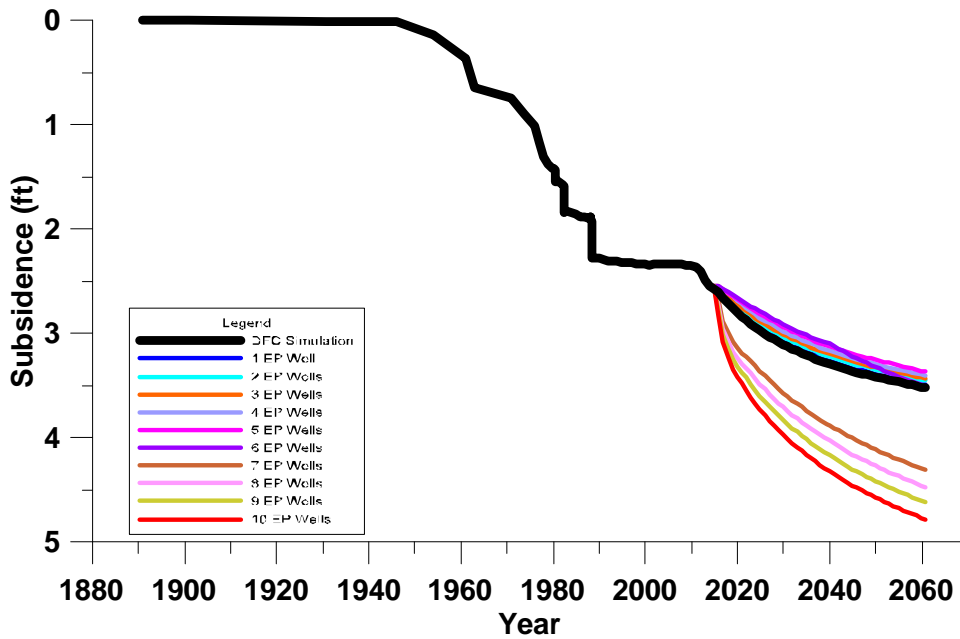


Figure E-47
Project Area - Maximum Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
GAM

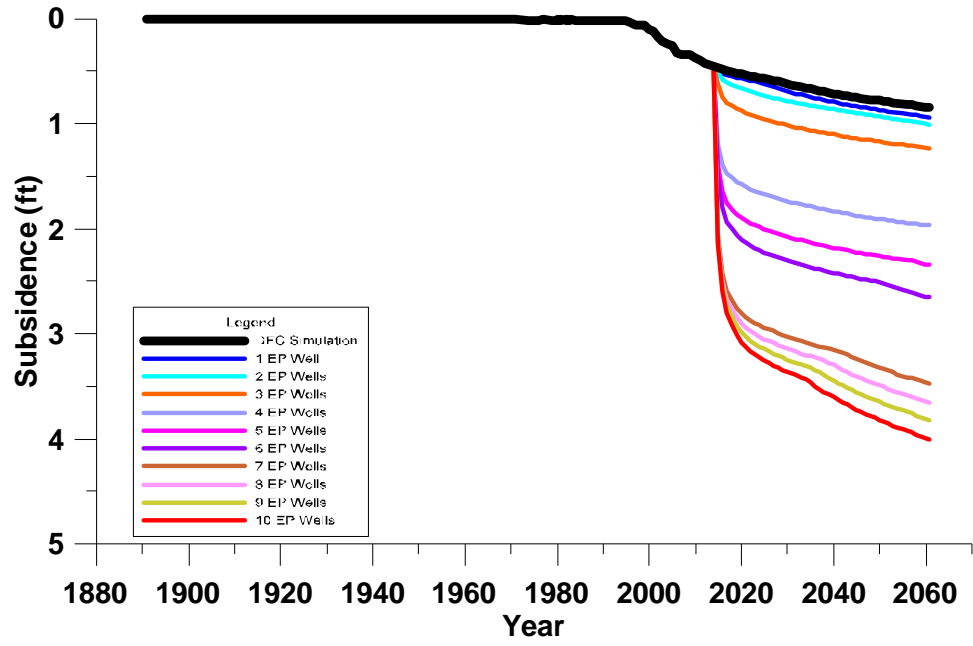


Figure E-48
Project Area - Maximum Subsidence
Electro Purification Pumping Within MAG (Other Pumping Reduced)
HAGM

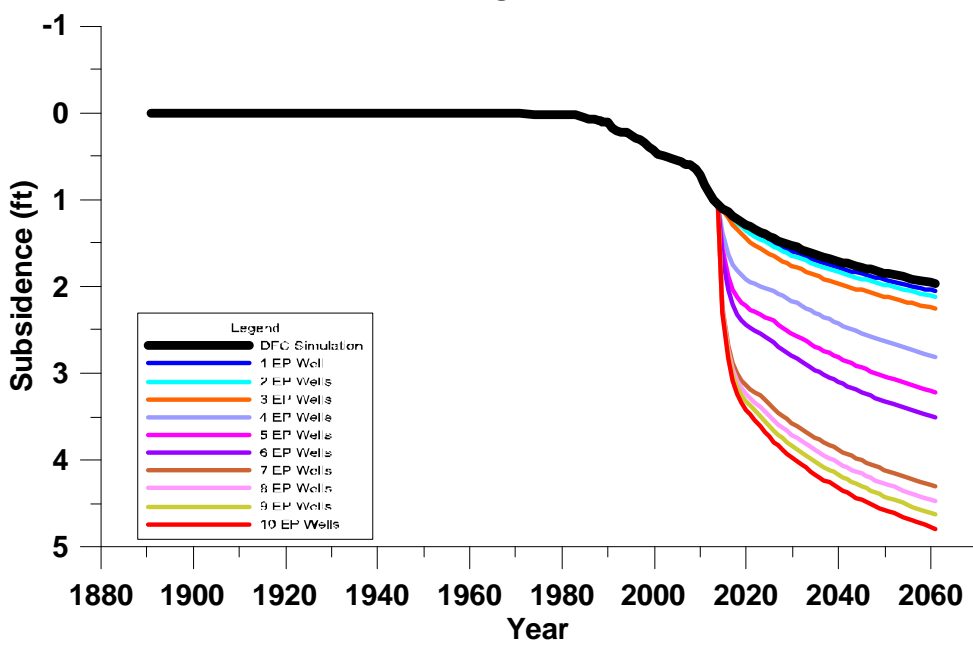


Figure E-49
Austin County - Maximum Subsidence
Electro Purification Pumping - Evangeline/Jasper (GAM)

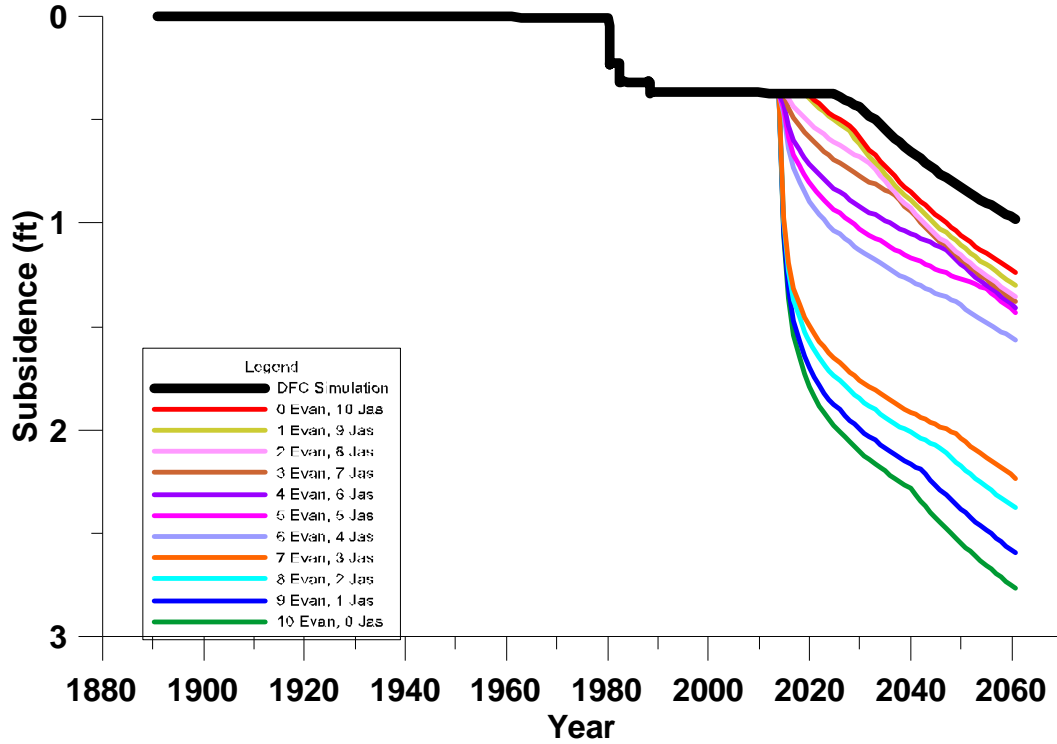


Figure E-50
Austin County - Maximum Subsidence
Electro Purification Pumping - Evangeline/Jasper (HAGM)

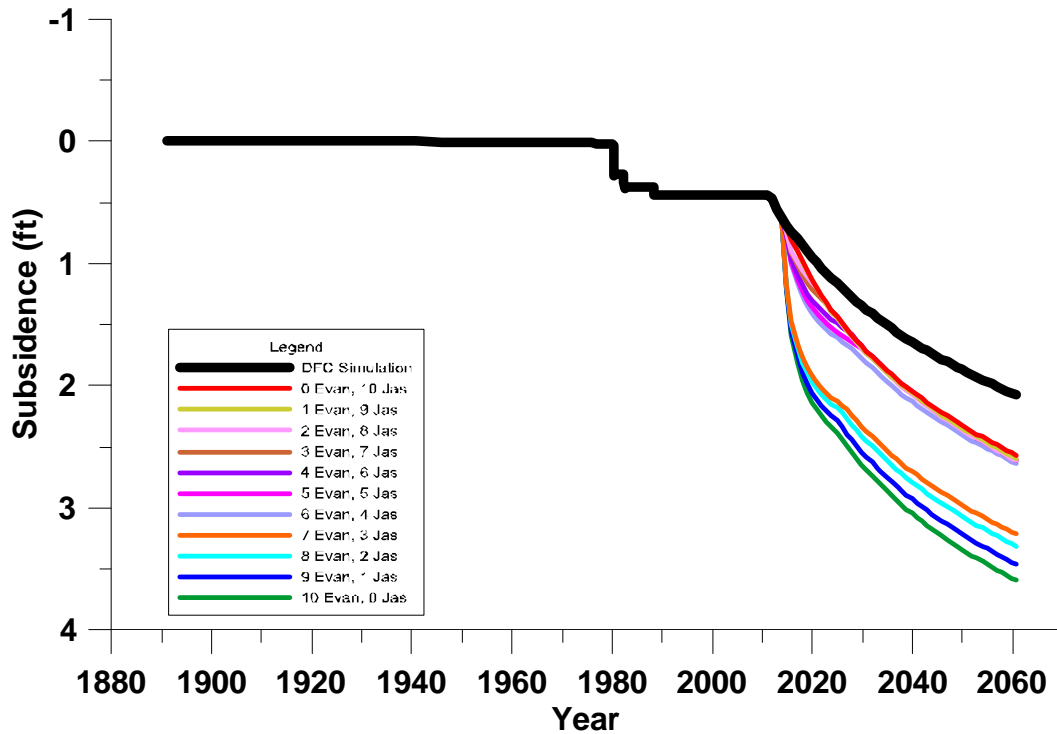


Figure E-51
Fort Bend County - Maximum Subsidence
Electro Purification Pumping - Evangeline/Jasper (GAM)

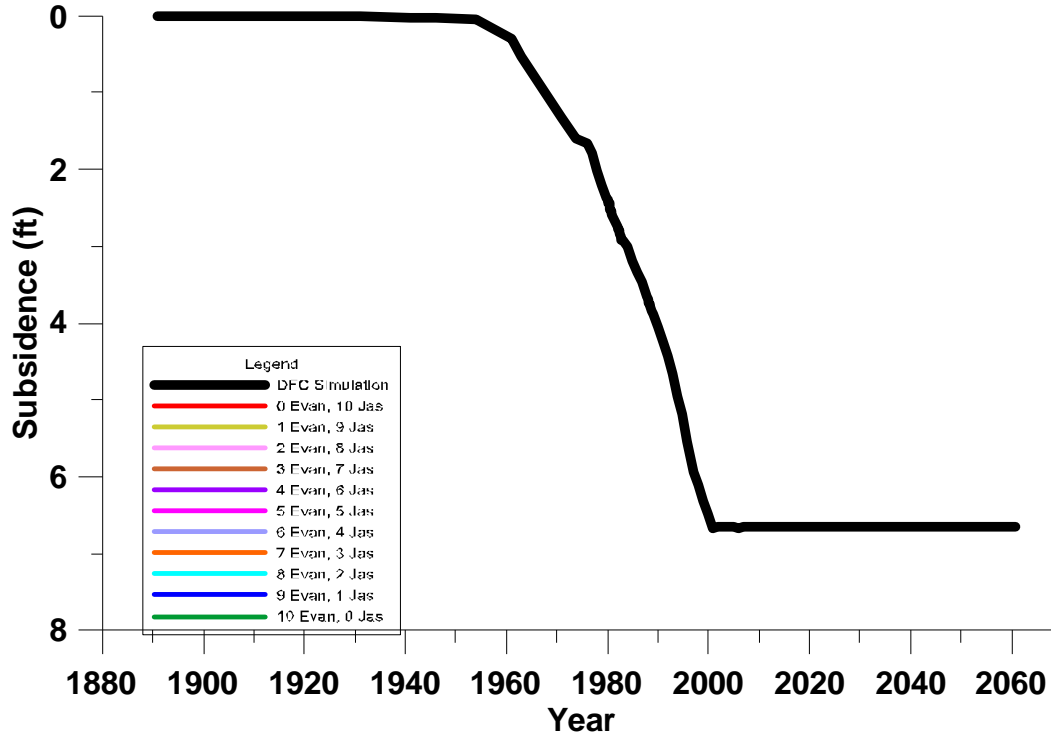


Figure E-52
Fort Bend County - Maximum Subsidence
Electro Purification Pumping - Evangeline/Jasper (HAGM)

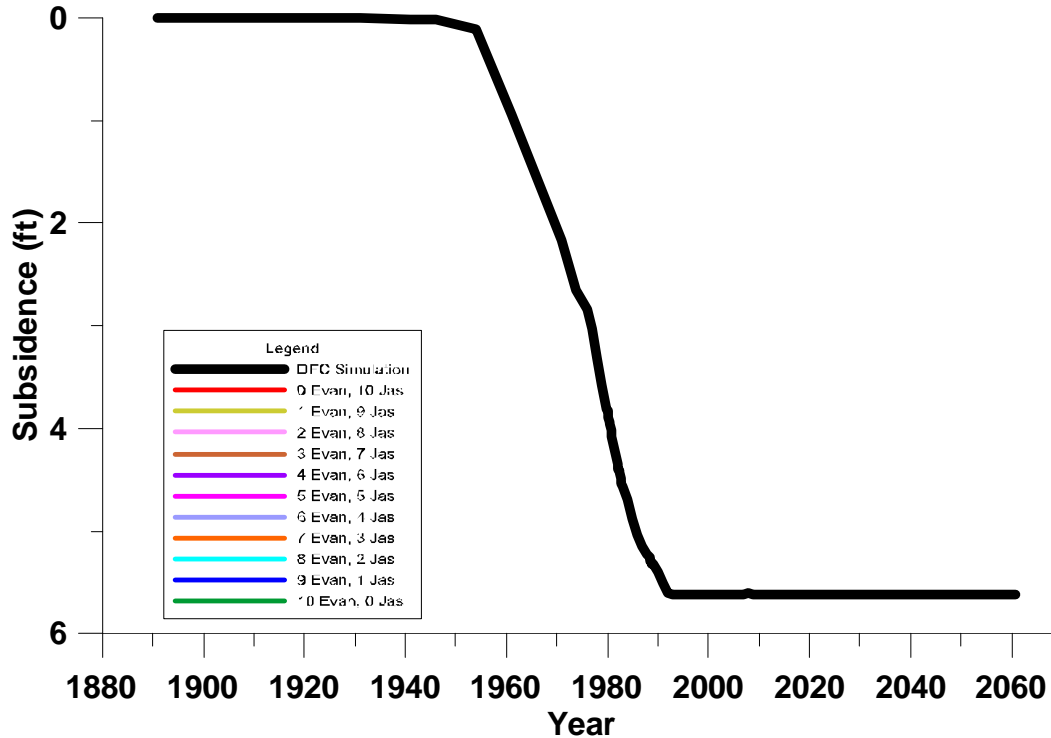


Figure E-53
Waller County - Maximum Subsidence
Electro Purification Pumping - Evangeline/Jasper (GAM)

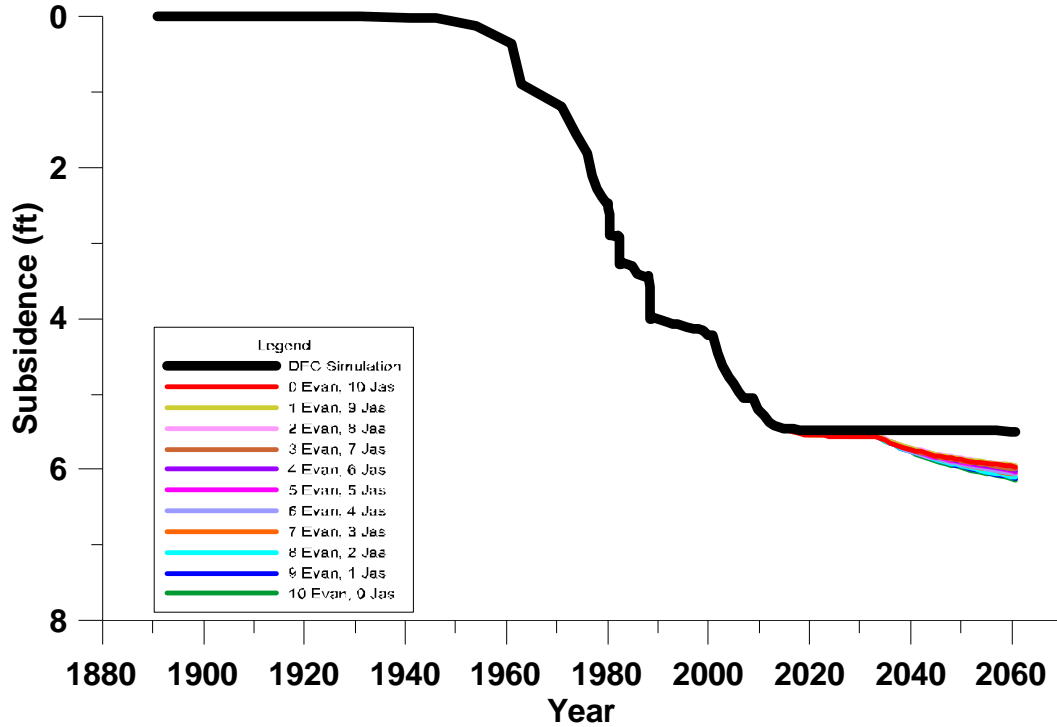


Figure E-54
Waller County - Maximum Subsidence
Electro Purification Pumping - Evangeline/Jasper
HAGM

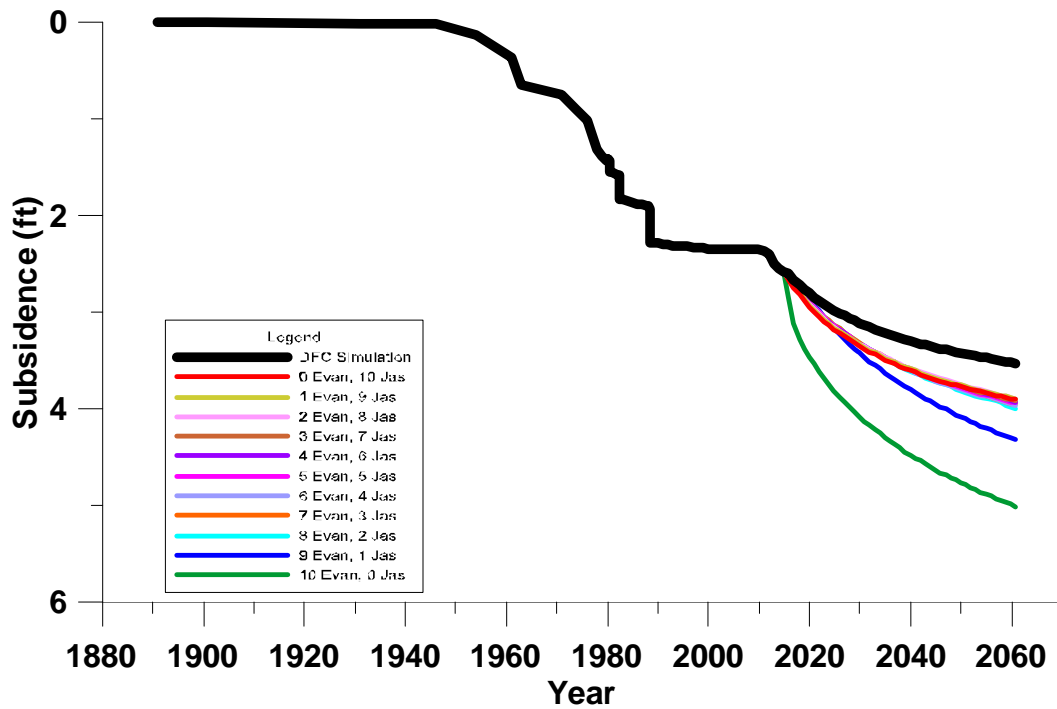


Figure E-55
Project Area - Maximum Subsidence
Electro Purification Pumping - Evangeline/Jasper (GAM)

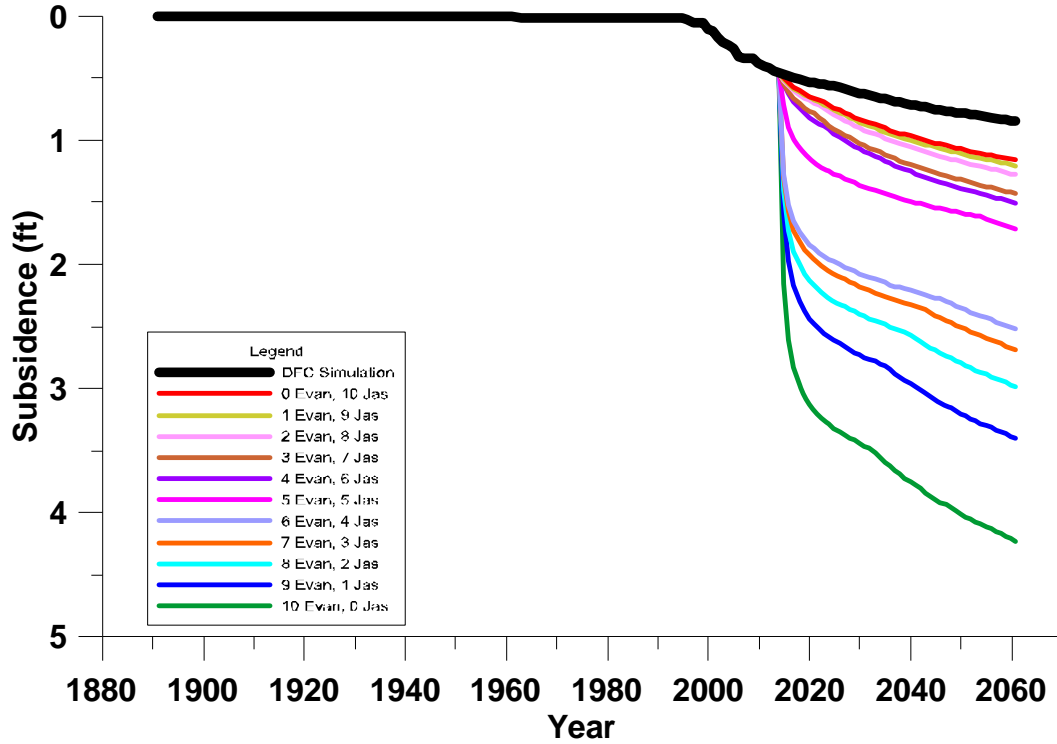
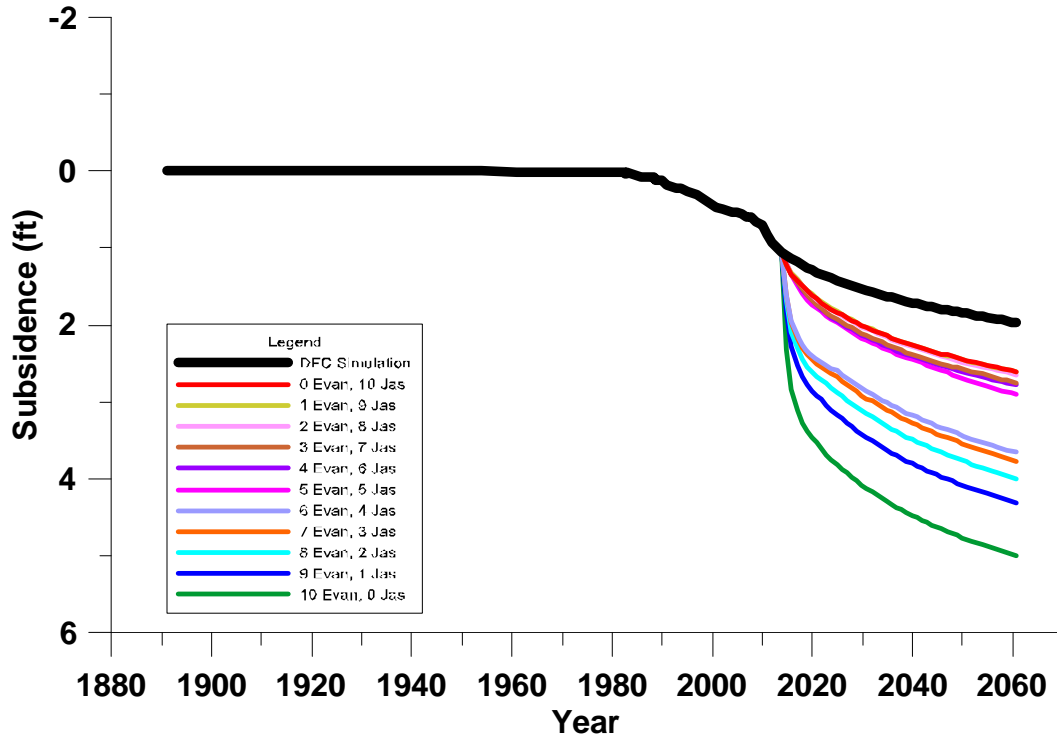


Figure E-56
Project Area - Maximum Subsidence
Electro Purification Pumping - Evangeline/Jasper (HAGM)



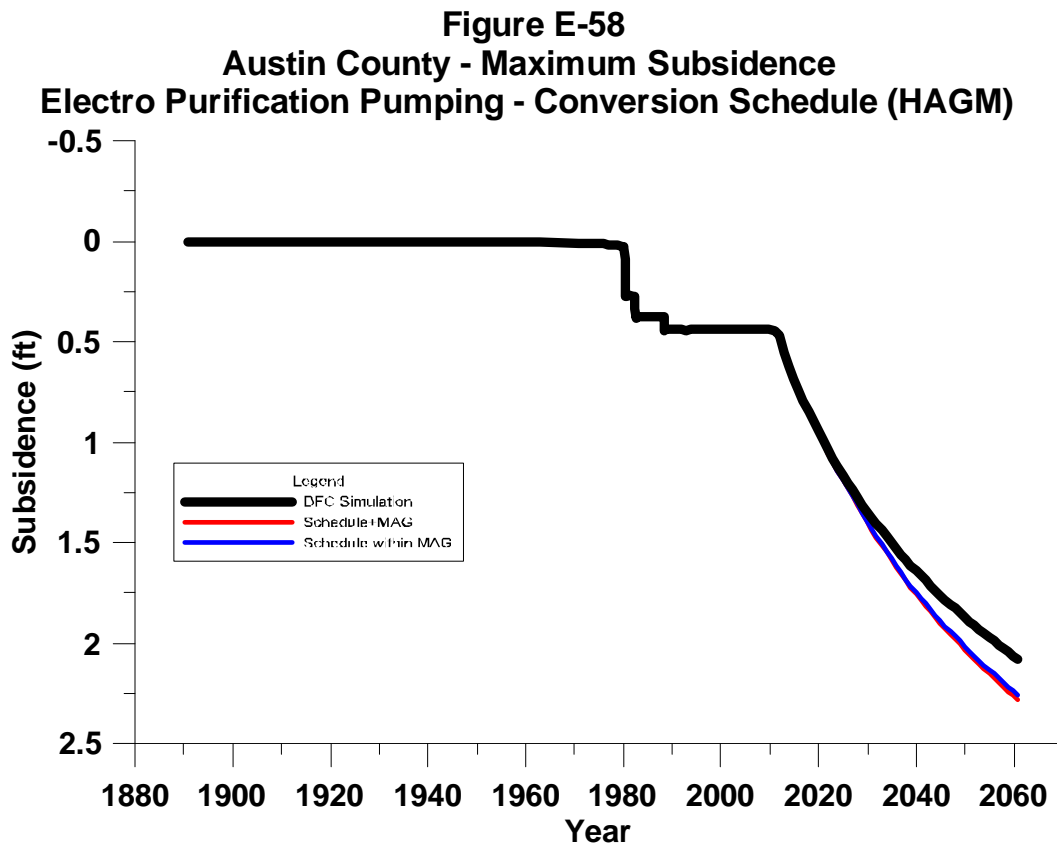
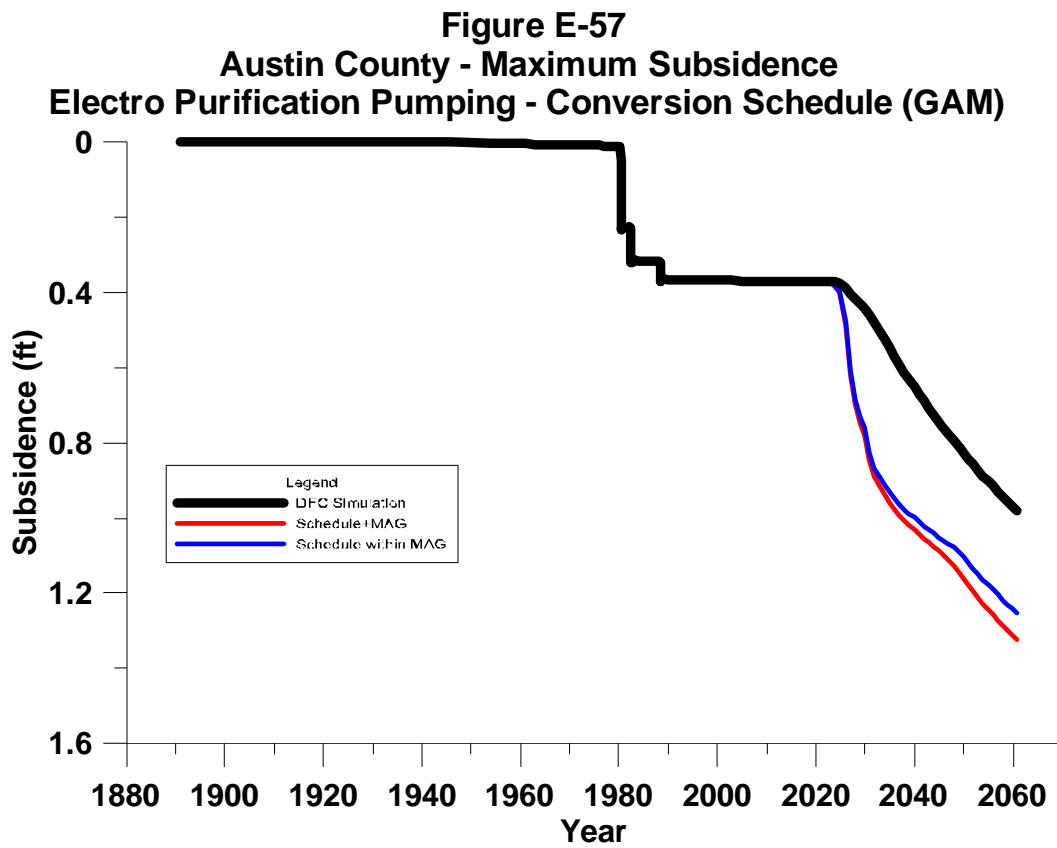


Figure E-59
Fort Bend County - Maximum Subsidence
Electro Purification Pumping - Conversion Schedule (GAM)

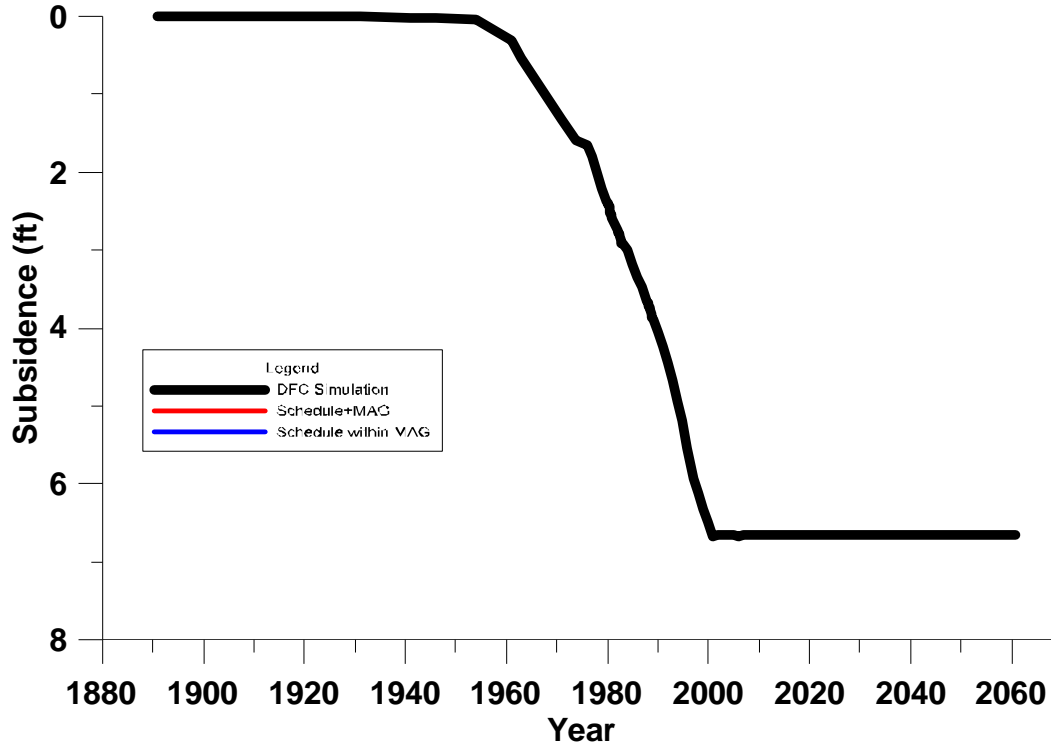


Figure E-60
Fort Bend County - Maximum Subsidence
Electro Purification Pumping - Conversion Schedule (HAGM)

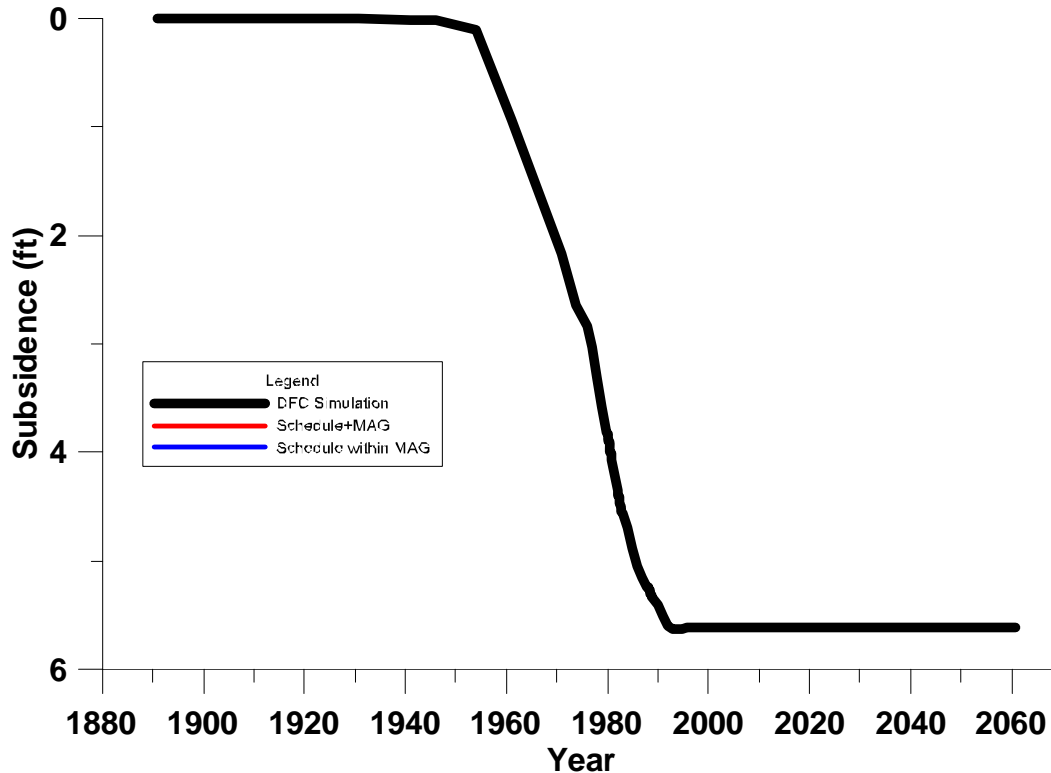


Figure E-61
Waller County - Maximum Subsidence
Electro Purification Pumping - Conversion Schedule (GAM)

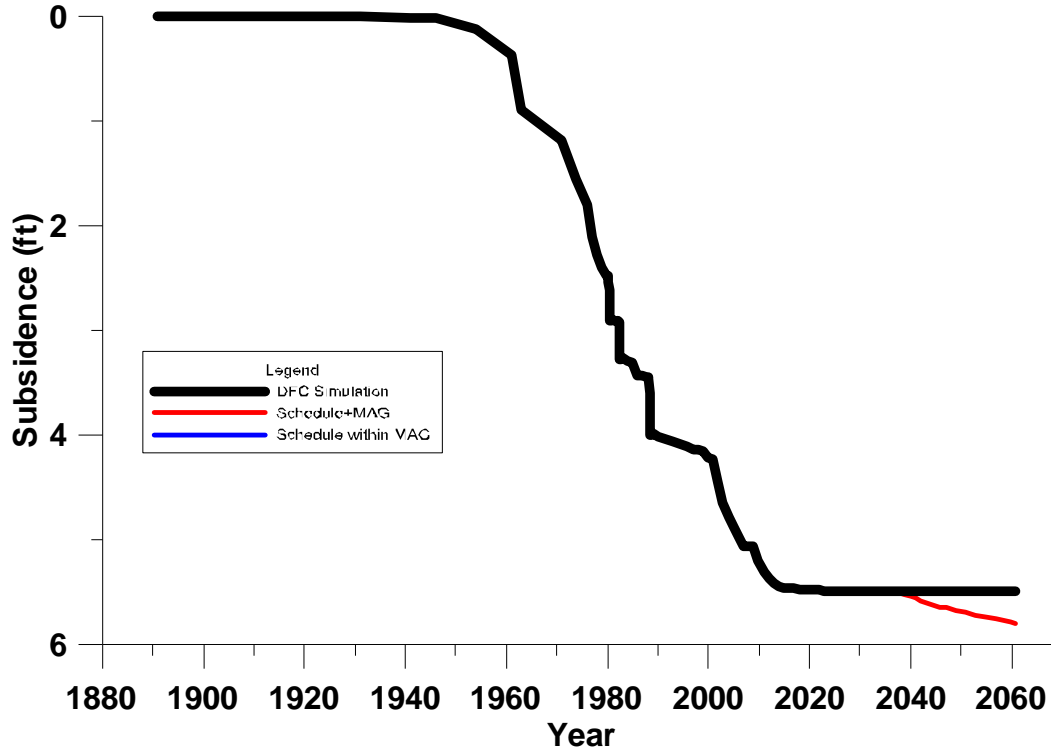
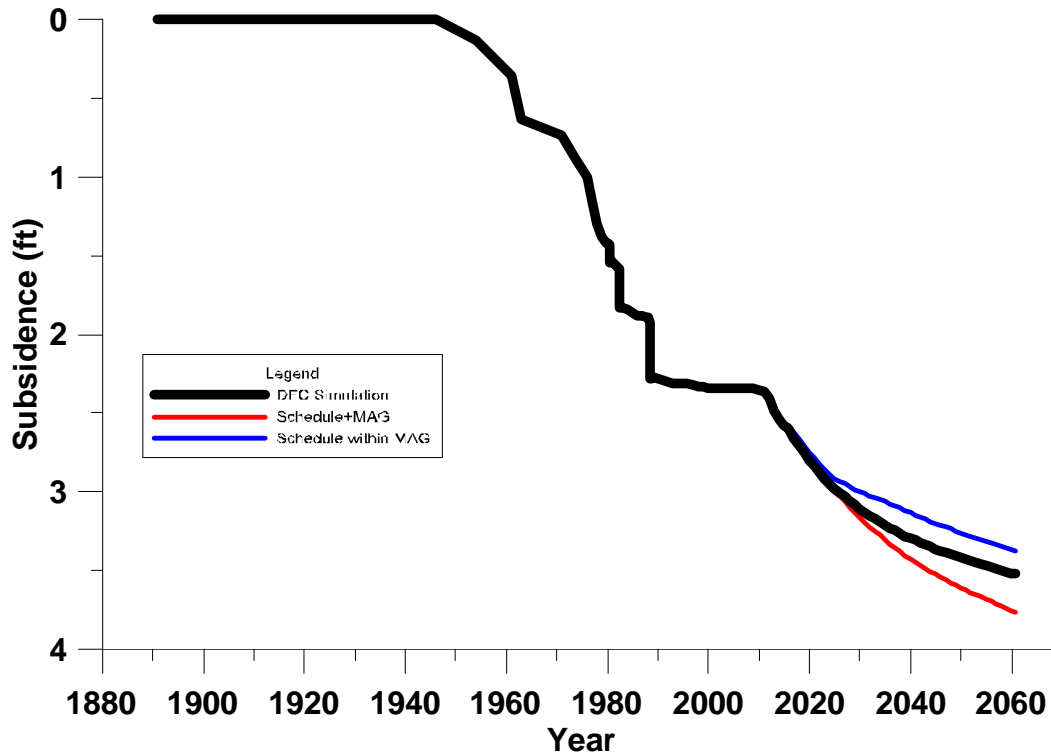


Figure E-62
Waller County - Maximum Subsidence
Electro Purification Pumping - Conversion Schedule (HAGM)



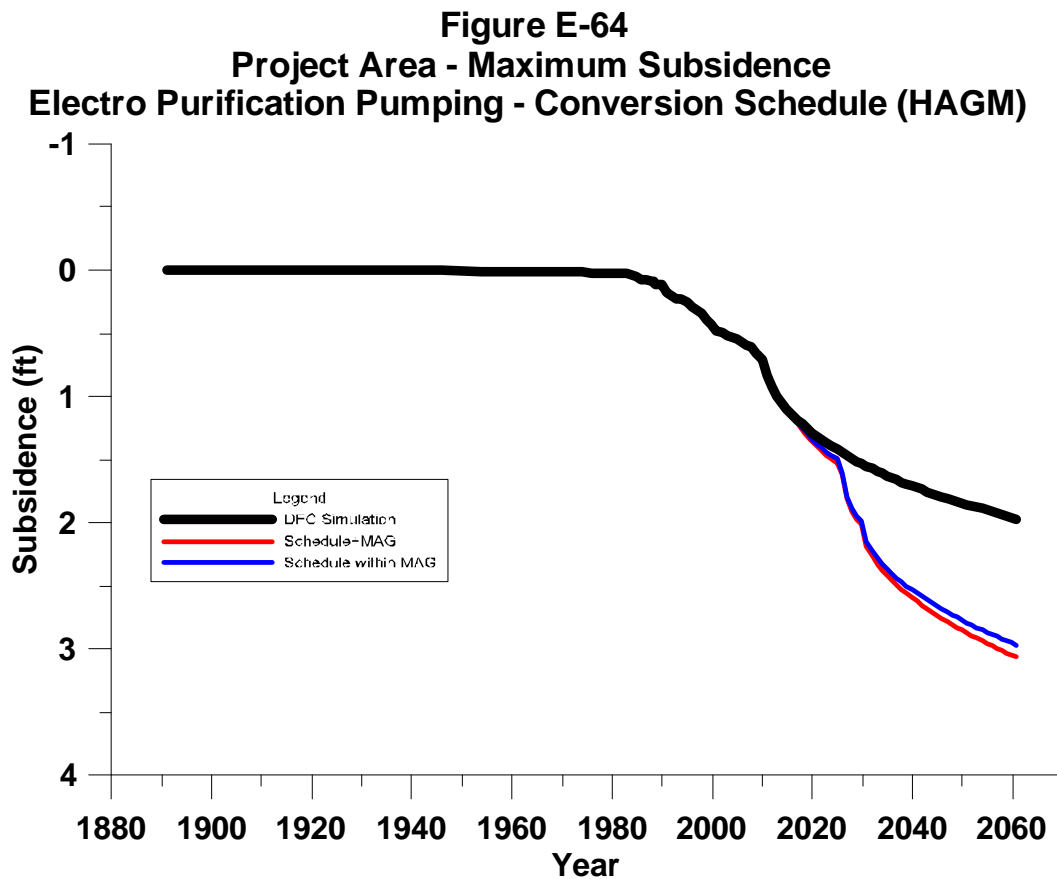
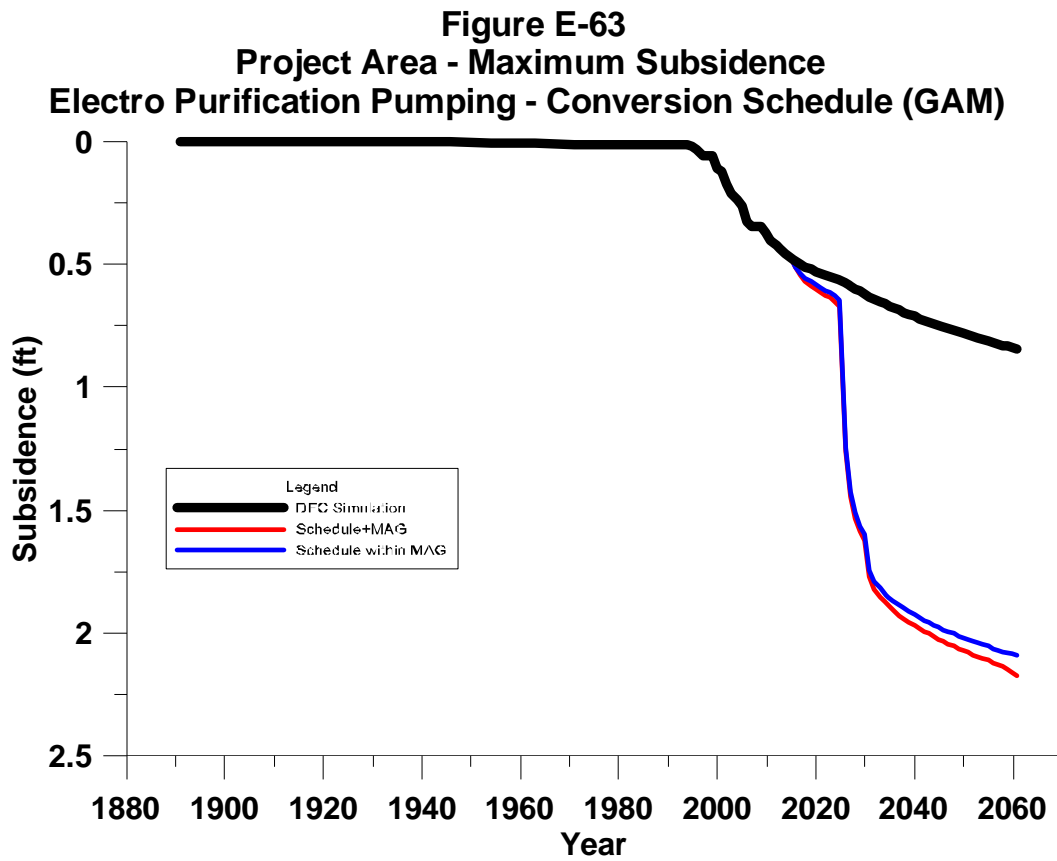


Figure E-65
Simulated Subsidence 1890 to 2060 - GAM
Base Case (DFC/MAG Simulations)

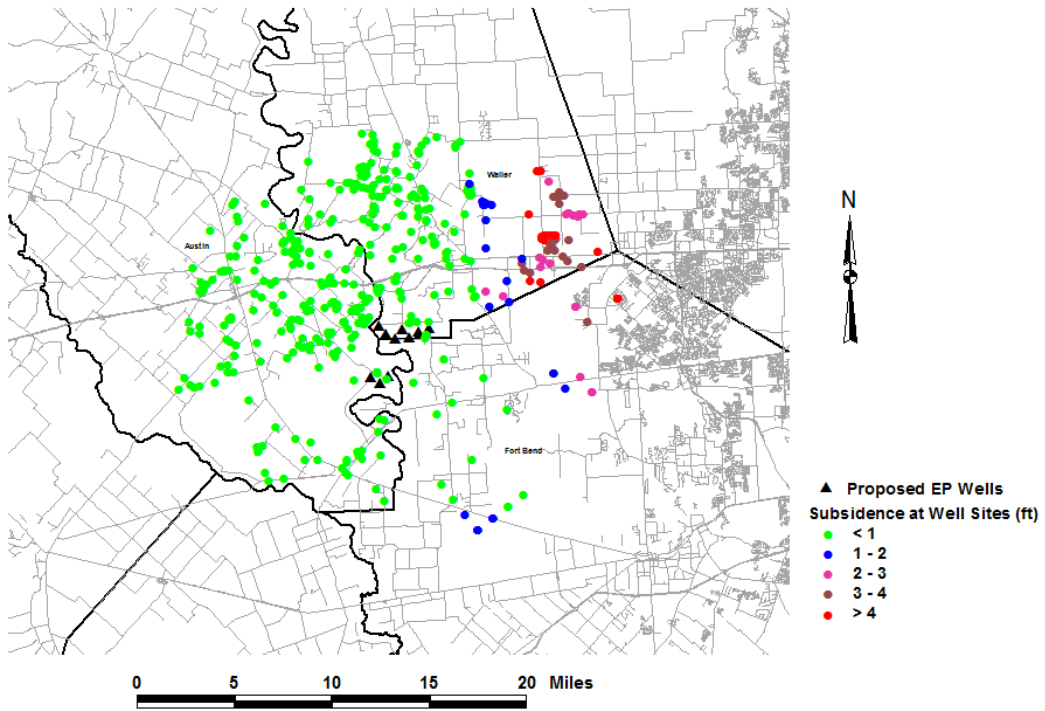


Figure E-66
Simulated Subsidence 1890 to 2060 - HAGM
Base Case (DFC/MAG Simulations)

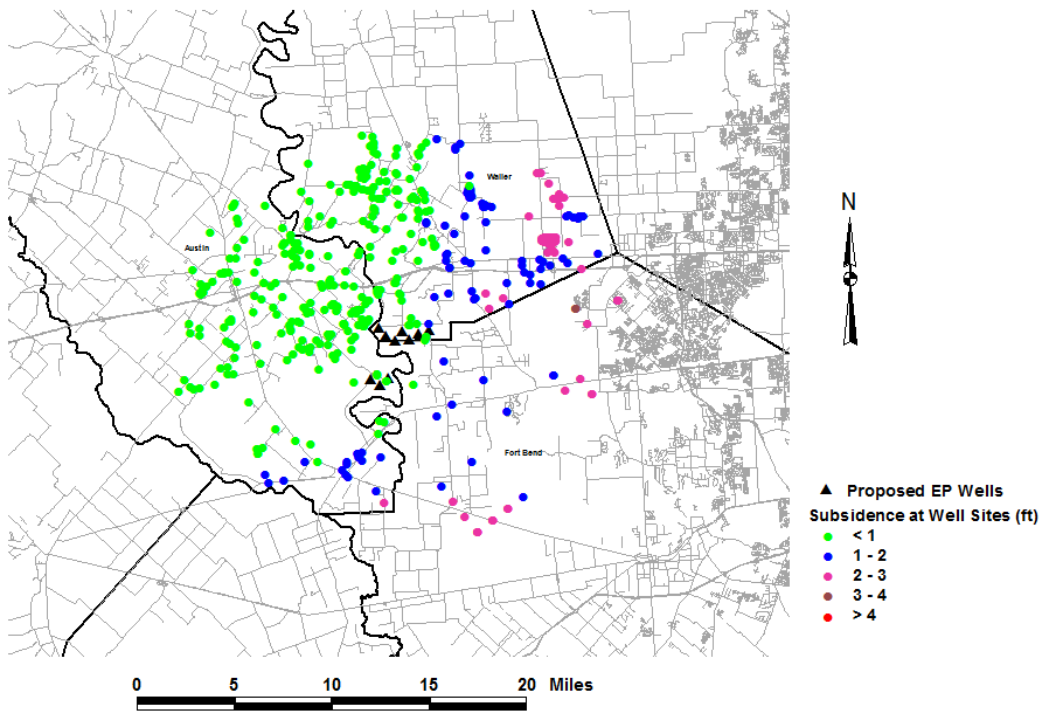


Figure E-67
Simulated Subsidence 1890 to 2060 - GAM
Scenario 3 (EP Pumping = 6 MGD)

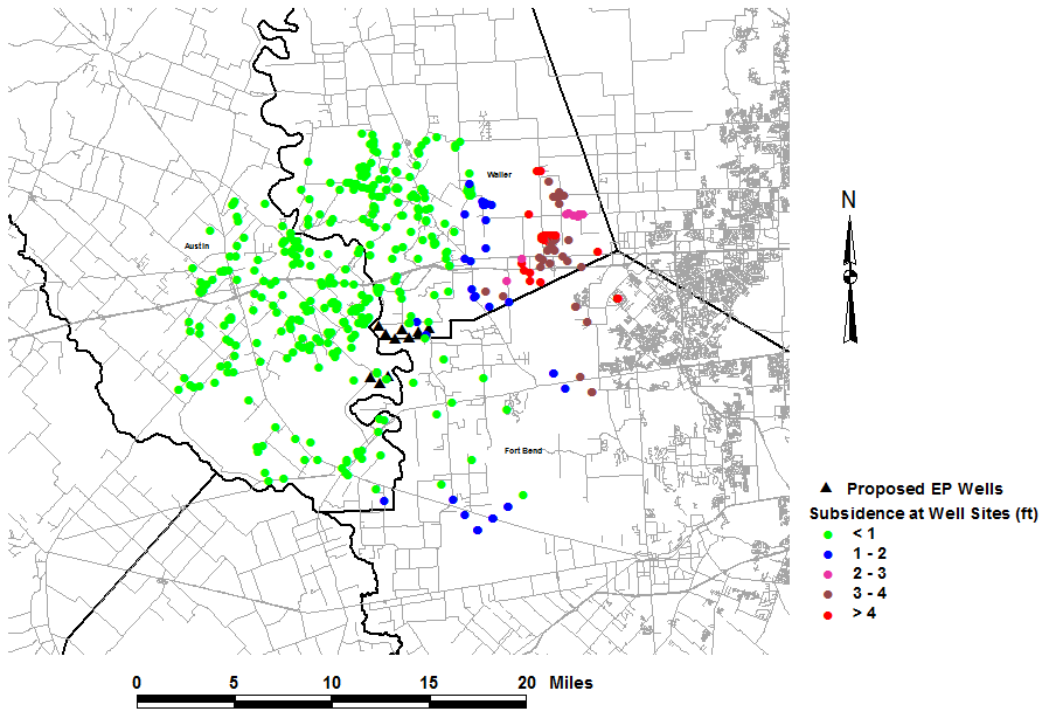


Figure E-68
Simulated Subsidence 1890 to 2060 - HAGM
Scenario 3 (EP Pumping = 6 MGD)

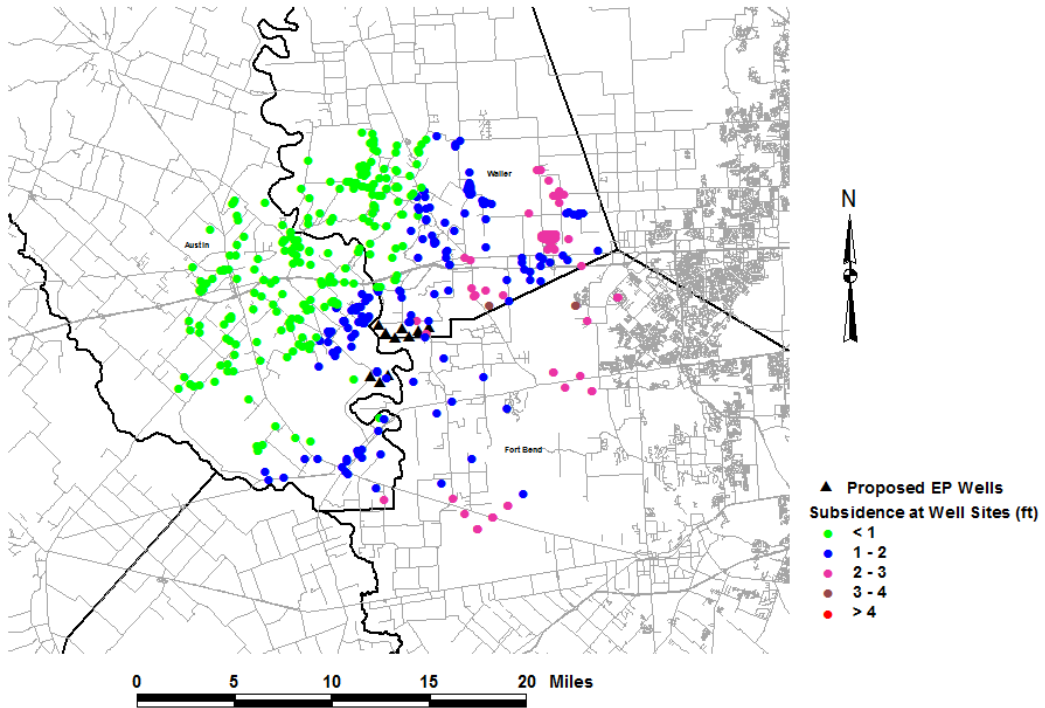


Figure E-69
Simulated Subsidence 1890 to 2060 - GAM
Scenario 10 (EP Pumping = 20 MGD)

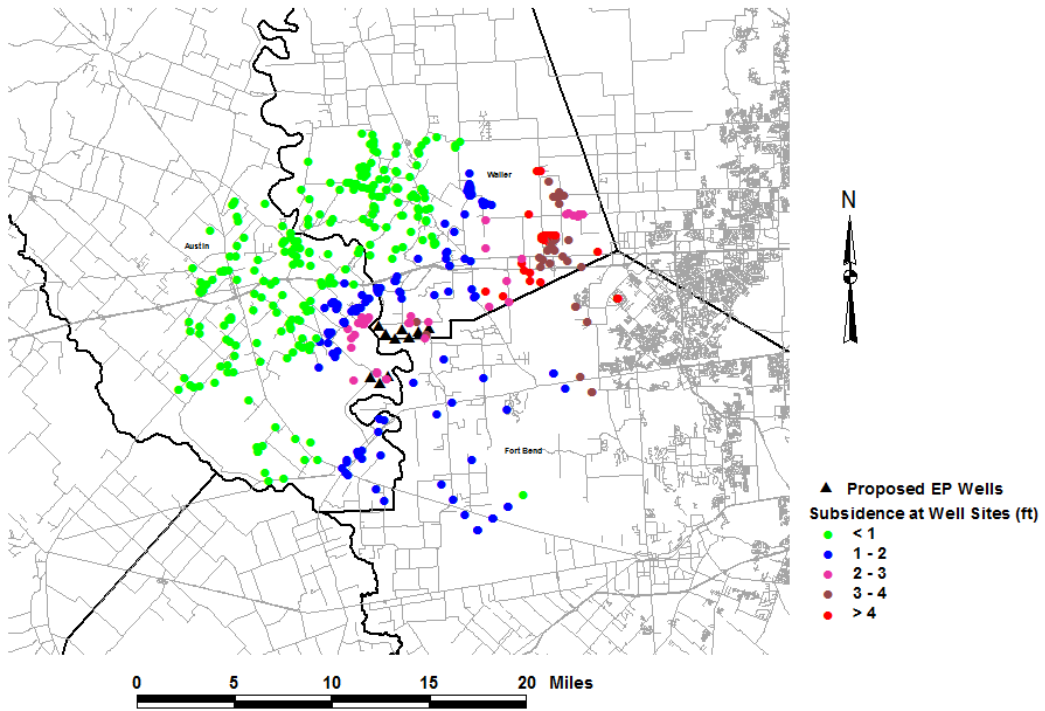


Figure E-70
Simulated Subsidence 1890 to 2060 - HAGM
Scenario 10 (EP Pumping = 20 MGD)

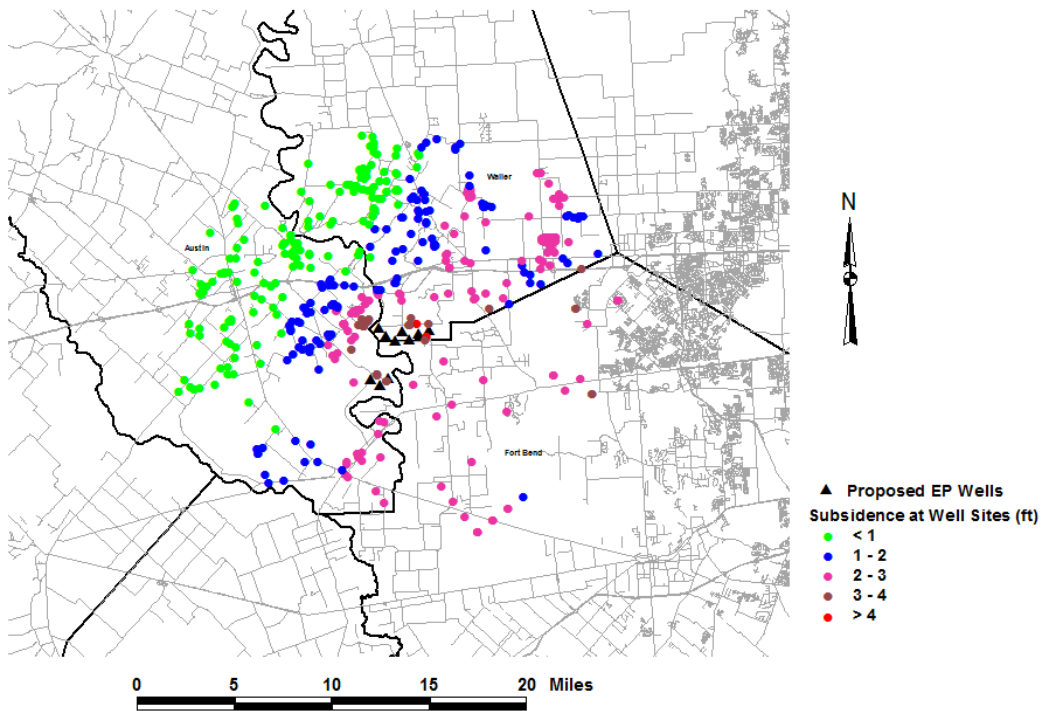


Figure E-71
Simulated Subsidence 1890 to 2060 - GAM
Scenario 31 (EP Pumping = 9.9 MGD)

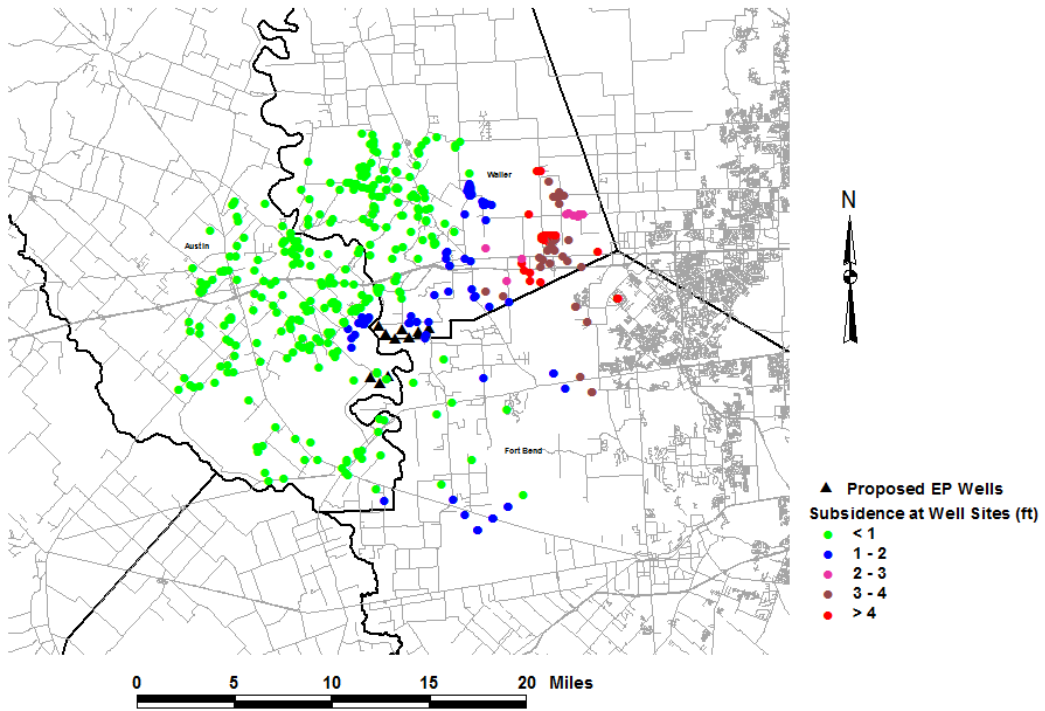


Figure E-72
Simulated Subsidence 1890 to 2060 - HAGM
Scenario 31 (EP Pumping = 9.9 MGD)

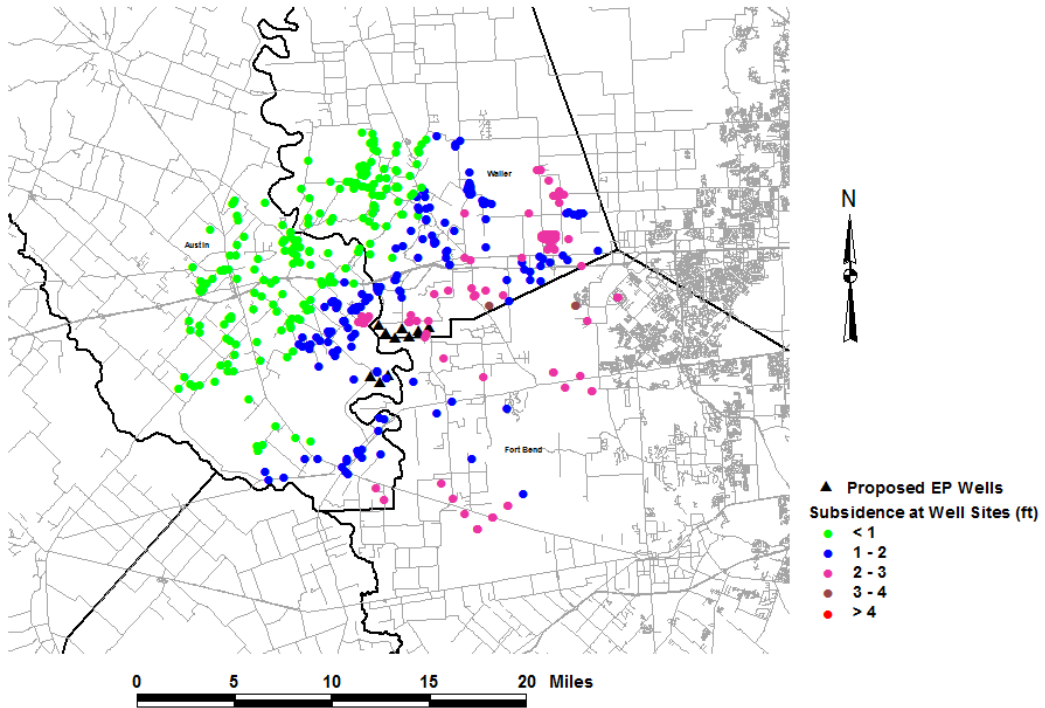


Figure E-73
Simulated Subsidence Attributable to EP Pumping - GAM
Scenario 3 (EP Pumping = 6 MGD)

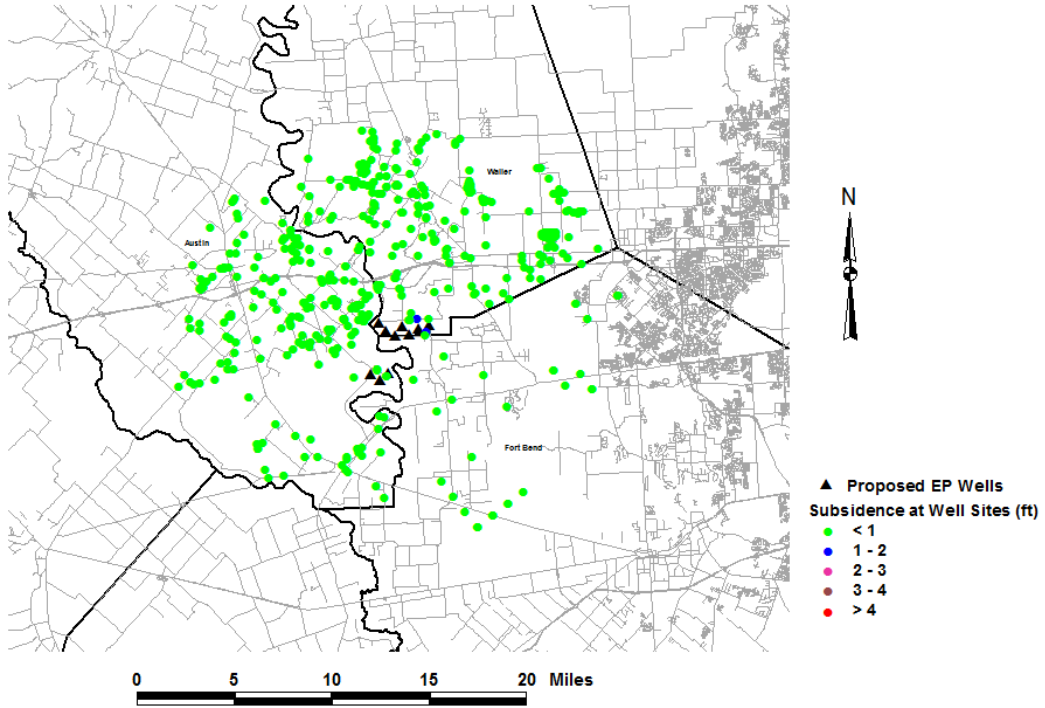


Figure E-74
Simulated Subsidence Attributable to EP Pumping - HAGM
Scenario 3 (EP Pumping = 6 MGD)

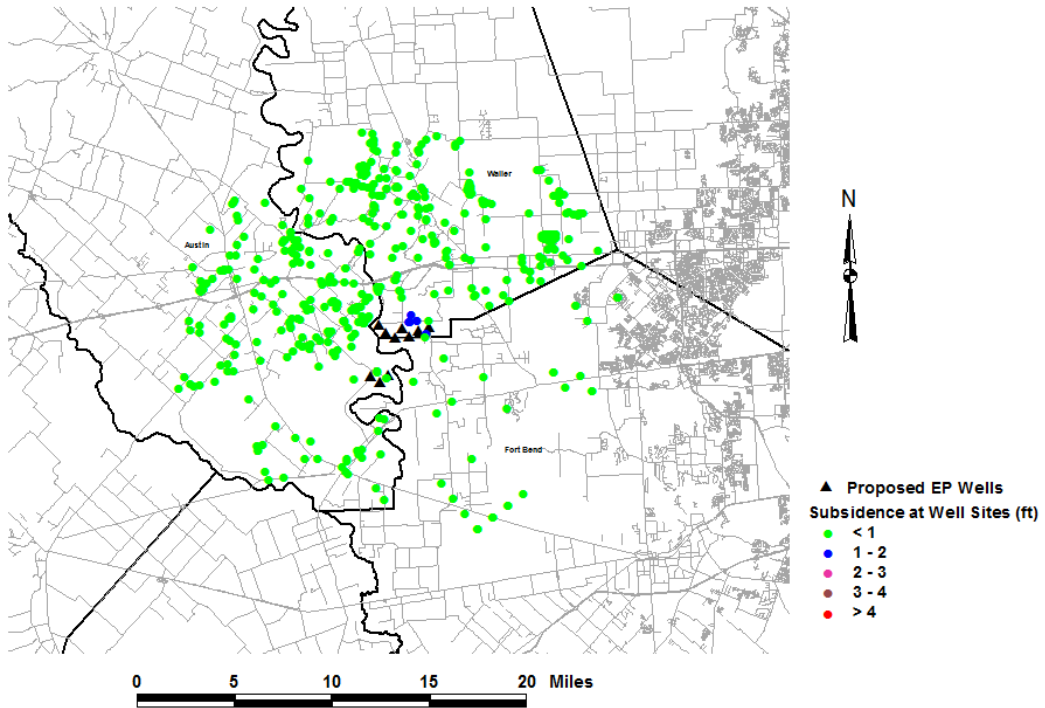


Figure E-75
Simulated Subsidence Attributable to EP Pumping - GAM
Scenario 10 (EP Pumping = 20 MGD)

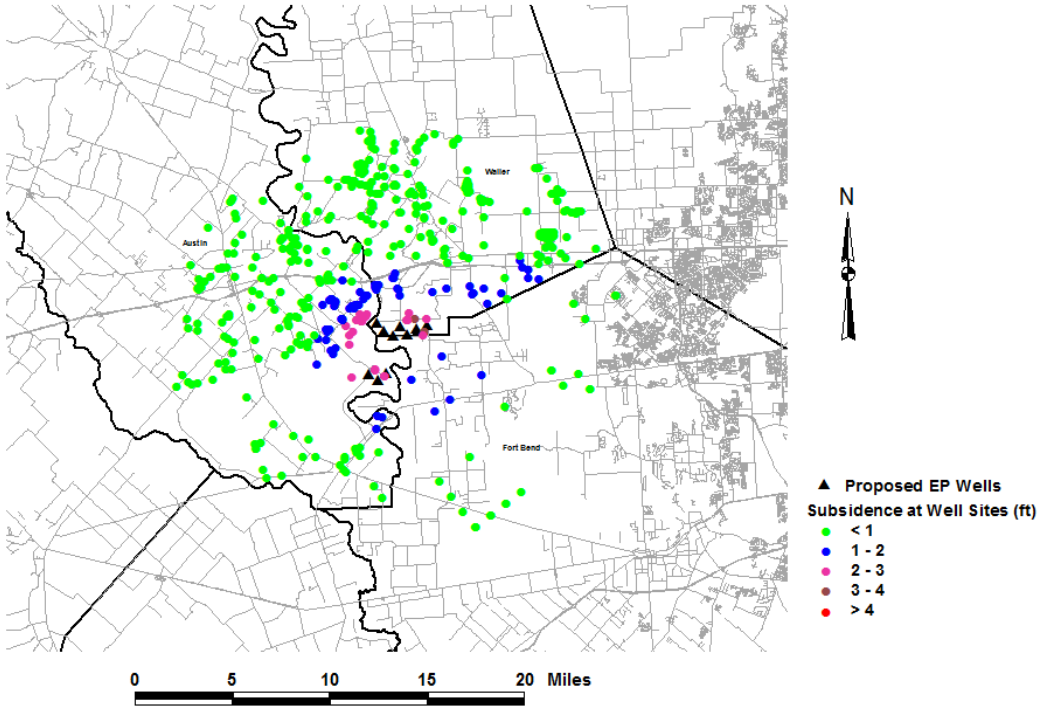


Figure E-76
Simulated Subsidence Attributable to EP Pumping - HAGM
Scenario 10 (EP Pumping = 20 MGD)

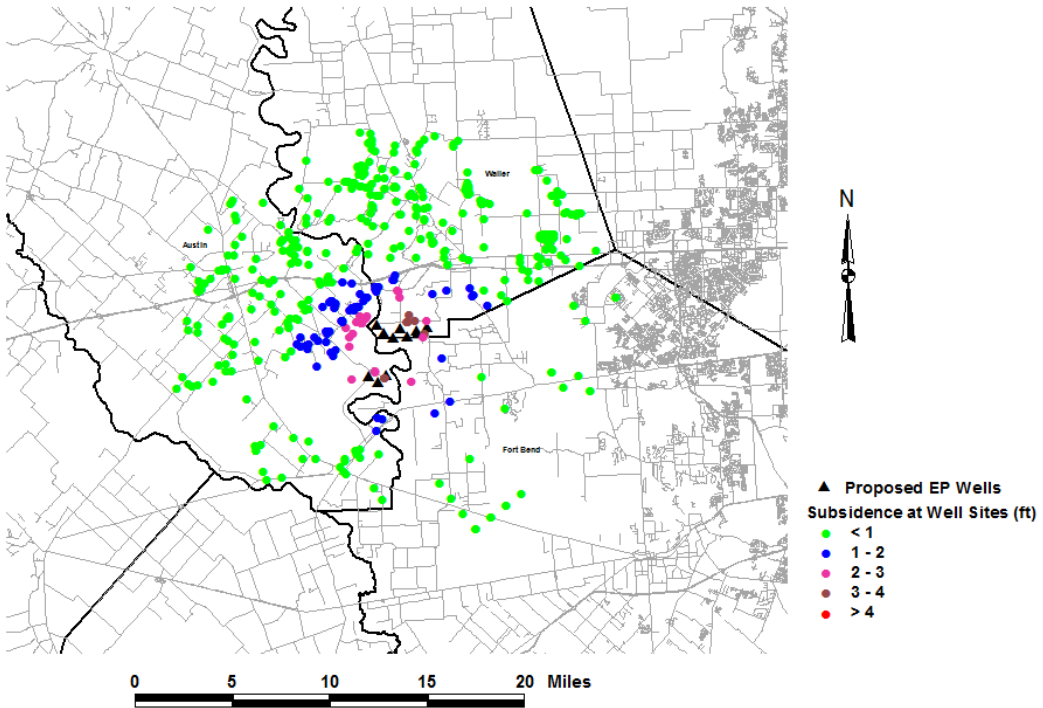


Figure E-77
Simulated Subsidence Attributable to EP Pumping - GAM
Scenario 31 (EP Pumping = 9.9 MGD)

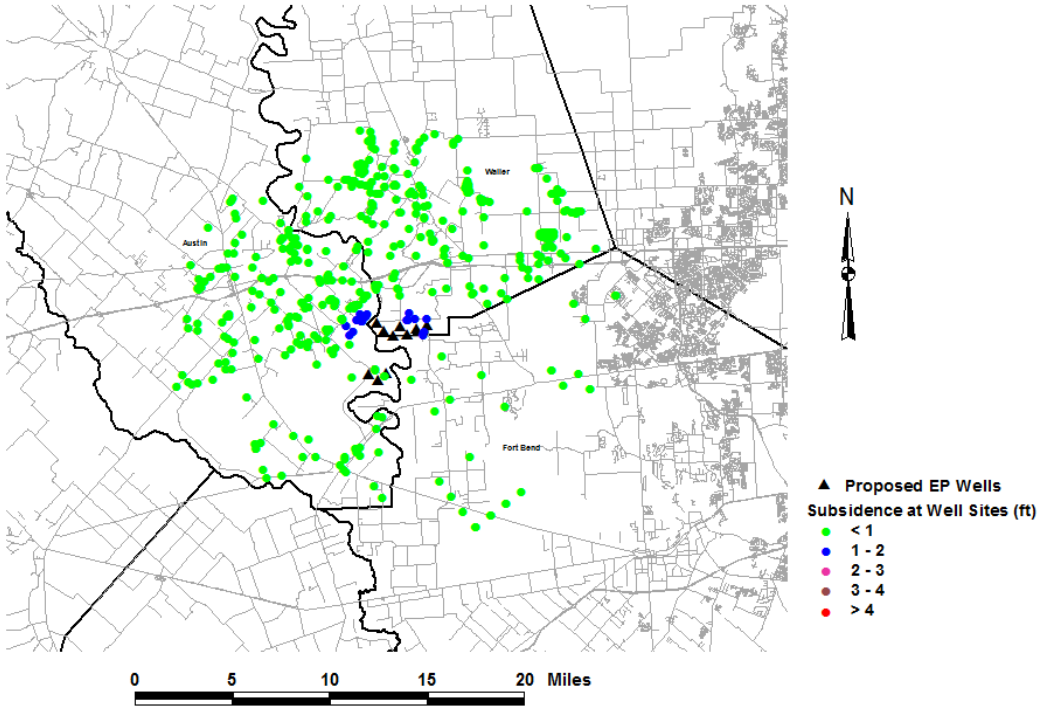
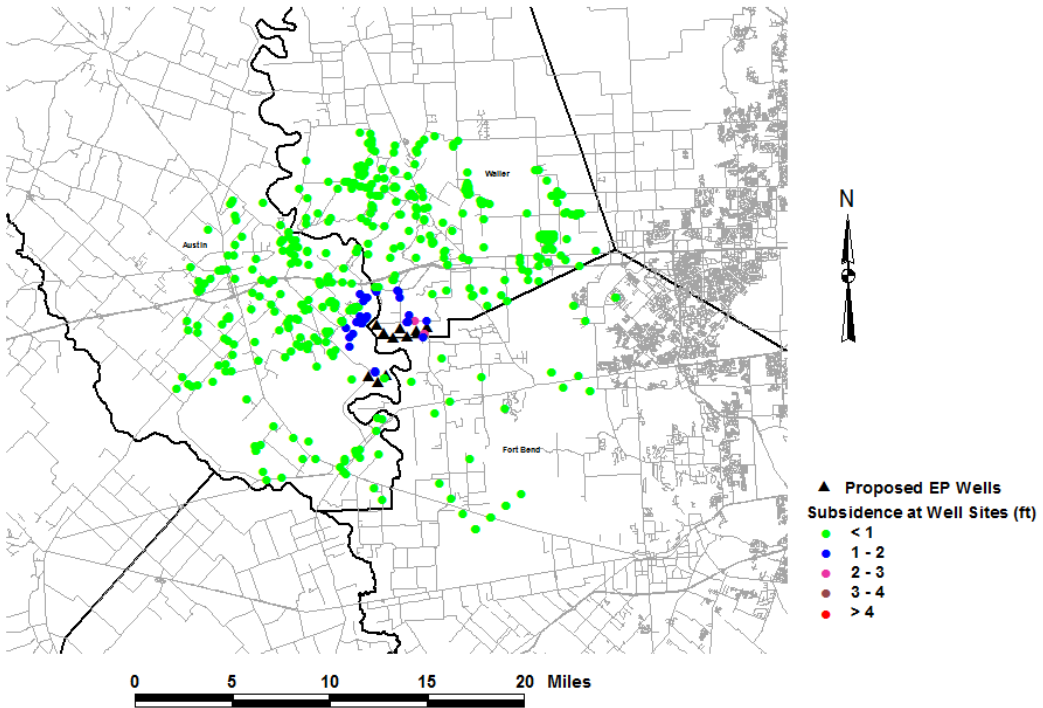


Figure E-78
Simulated Subsidence Attributable to EP Pumping - HAGM
Scenario 31 (EP Pumping = 9.9 MGD)



Appendix F – Salt Domes

Appendix F – Salt Domes

This appendix reviews information related to salt domes in the area of the proposed Electro Purification wells. Several of the parties in the contested case hearing have raised concerns regarding the salt domes that are located in the area of the proposed project, specifically the Brookshire Salt Dome (also known as the San Felipe Salt Dome in the literature).

Hamlin (2006) reviewed the available literature on salt domes in the Gulf Coast Aquifer, and summarized the current understanding of salt dome hydrogeology. As described by Hamlin (2006, pg. 217-218) the salt in salt domes originally formed as bedded evaporate deposits in the ancestral Gulf of Mexico during the Jurassic period. Subsequent deposition has buried the salt with over 20,000 feet of sediments. Due to the low density and ductile quality of the salt, the salt domes occur as a result of salt upwelling into the overlying sediments. This upwelling causes deformation of the overlying sediments, and is characterized by areas of subsidence and downwarping, and can affect surface topography if they rise close enough to the land surface.

Hamlin (2006) included a map (Hamlin, 2006, pg. 221) and cross-section (Hamlin, 2006, pg. 219) that covers the area of the proposed Electro Purification wells. The relevant portion of Hamlin's map (with additional annotations) is presented as Figure F-1, and Hamlin's the cross-section (with additional annotations) is presented as Figure F-2.

Please note that in Figure F-1, the Brookshire Salt Dome (or San Felipe Salt Dome) is not located with a dot on Hamlin's map of shallow salt domes. The depth to the cap rock of the Brookshire Salt Dome (or San Felipe Salt Dome) is reported to be 3,218 feet below ground surface by Beckman and Williamson (1990, pg. 42), and the depth to the salt dome itself is reported to be 4,755 by Beckman and Williamson (1990, pg. 42). For purposes of Hamlin's evaluation and map, this depth did not appear to qualify as a "shallow" salt dome. In contrast, the nearest salt dome that appears on Hamlin's map is the Orchard Salt Dome, with a reported depth to the cap rock of 285 feet and a reported depth to the salt of 369 feet (Beckman and Williamson, 1990, pg. 42).

The cross-section (Figure F-2) includes the Brookshire Salt Dome (or San Felipe Salt Dome) and shows its proximity to the location of the proposed Electro Purification wells. However, given that the proposed Electro Purification wells are expected to be about 1,500 feet deep, the proposed drilling would terminate at a depth about 1,700 feet above the reported depth top of the reported cap rock. Even if the salt dome was directly under one or more of the proposed well sites, there would be no issue with drilling to 1,500 feet.

The cross-section also shows the location of the Orchard Salt Dome. This shallow salt dome is located about 10 miles south of the proposed Electro Purification project area. There are no issues relative to drilling to 1,500 feet with a shallow salt dome located 10 miles away. As described by Hamlin (2006, pg. 228), long term and high pumping can cause migration of poor quality groundwater from salt domes into shallow fresh groundwater aquifers. Long term groundwater quality monitoring is already anticipated to be a condition of the permit, if one is issued, and the issue of potential groundwater quality degradation can be assessed. Any such groundwater quality degradation from the Orchard Salt Dome, however, would affect Fort Bend County and

the proposed project wells (and the immediate vicinity) due to the altered hydraulic gradient caused by the proposed project pumping. Other parts of Waller or Austin counties within the Bluebonnet Groundwater Conservation District would likely be unaffected by salty groundwater induced from the Orchard Salt Dome.

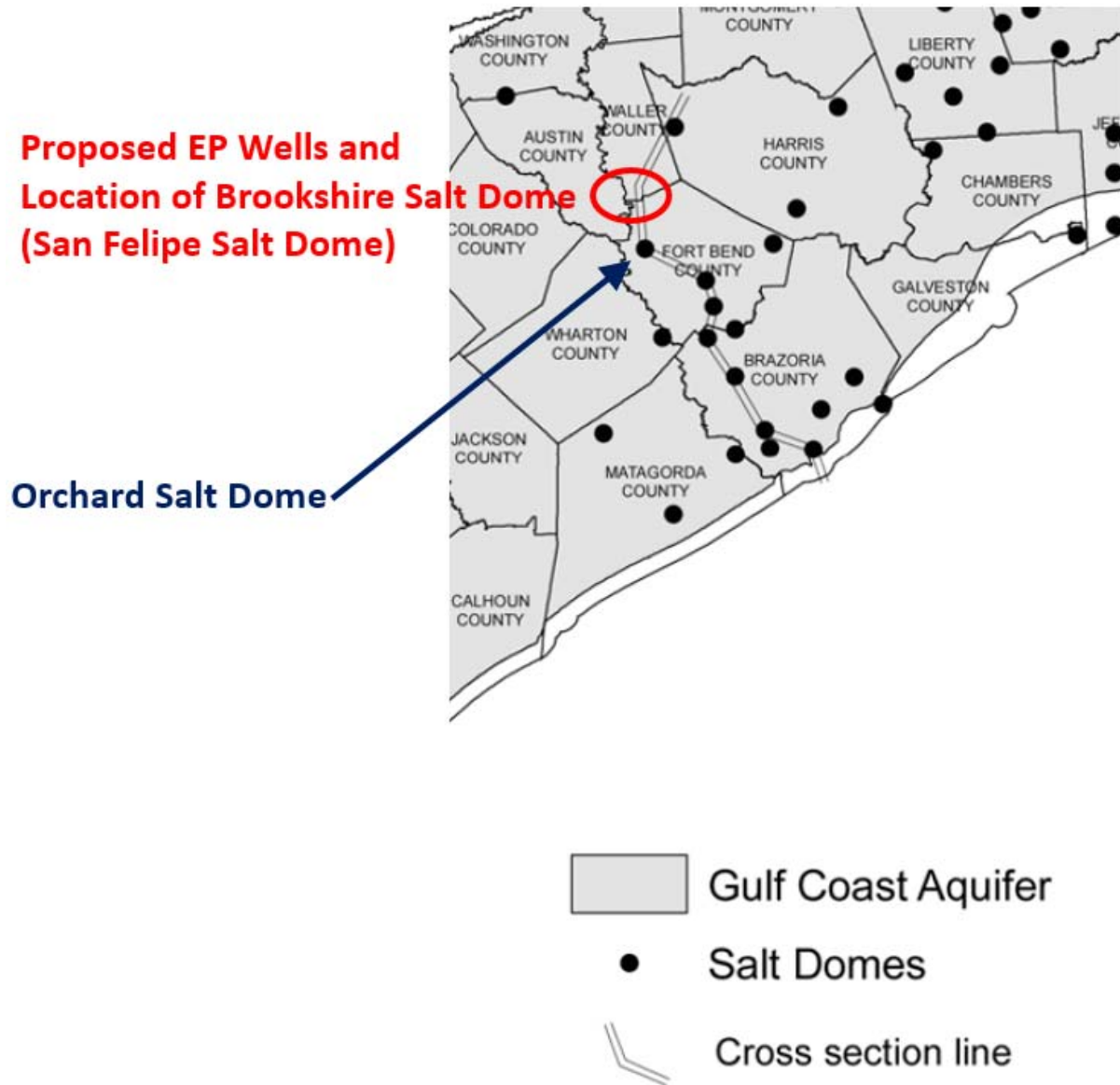


Figure F-1. Map of Shallow Salt Domes in the Texas Gulf Coast Area and Location of Cross-Section Line (from Hamlin, 2006, pg. 221)

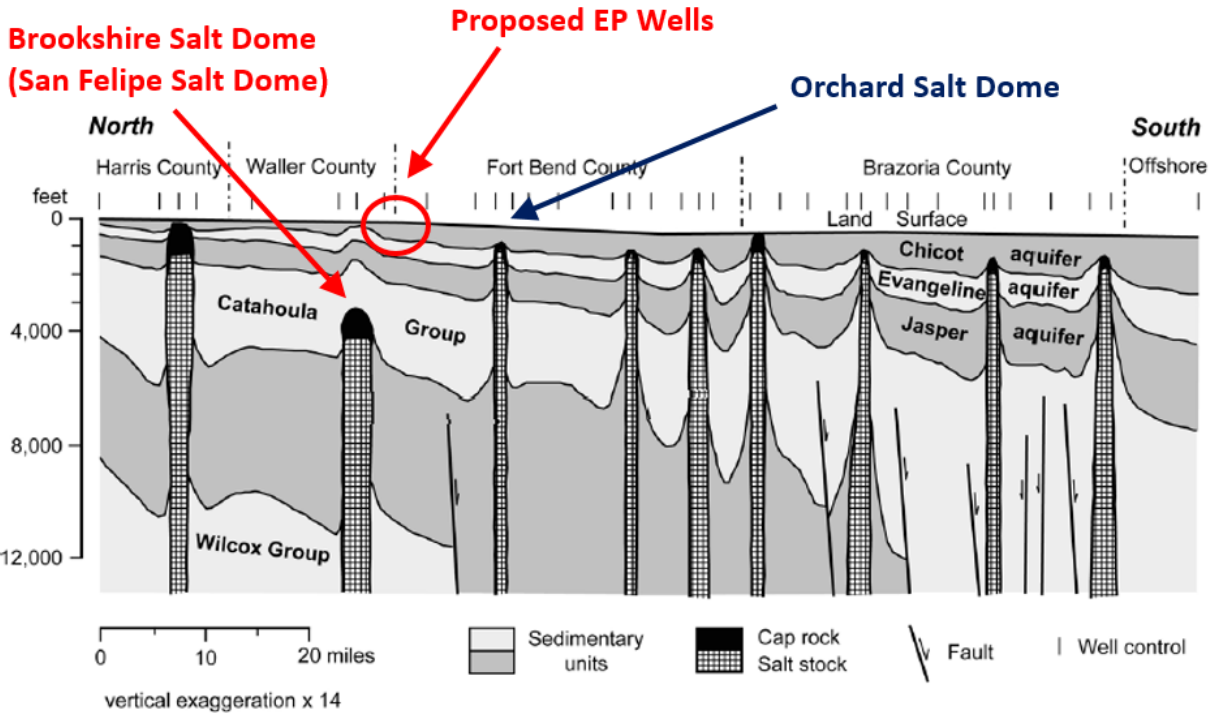


Figure F-2. Cross-Section of Subsurface. Location of Cross Section shown on Figure F-1. (from Hamlin, pg. 219)

References

Beckman, J.D., and Williamson, A.K., 1990. Salt-Dome Locations in the Gulf Coastal Plain, South-Central United States. U.S. Geological Survey Water-Resources Investigation Report 90-4060., 47p.

Hamlin, H.S., Salt Domes in the Gulf Coast Aquifer. Chapter 12 of Mace, R.E., Davidson, S.C., Angle, E.S., and Mullican, W.F., Aquifers of the Gulf Coast of Texas. Texas Water Development Board Report 365, 303p.